# A microseismic study in the western part of the Gulf of Corinth (Greece): implications for large-scale normal faulting mechanisms

A. Rigo,<sup>1,\*</sup> H. Lyon-Caen,<sup>1</sup> R. Armijo,<sup>1</sup> A. Deschamps,<sup>2</sup> D. Hatzfeld,<sup>3</sup> K. Makropoulos,<sup>4</sup> P. Papadimitriou<sup>4</sup> and I. Kassaras<sup>4</sup>

<sup>1</sup> Équipe de Sismotectonique – CNRS URA 195 et 1093 – Institut de Physique du Globe de Paris, 4 Place Jussieu, 75252 Paris Cedex 05, France

<sup>2</sup> Institut de Géodynamique, UMR géosciences Ajur, EP125, CNRS-UNSA, 250 rue A. Einstein, 06560 Valbonne, France

<sup>3</sup> L.G.I.T-I.R.I.G.M., CNRS URA 733, Université Joseph Fourrier, BP 68, 38402 St Martin d'Hères Cedex, France

<sup>4</sup> University of Athens, Department of Geology, Geophysics-Geothermy Division, Panepistimiopolis Ilissia, Athens 157 84, Greece

Accepted 1996 March 19. Received 1996 March 19; in original form 1995 July 17

#### SUMMARY

We present the results of a dense seismological experiment in the western part of the Gulf of Corinth (Psathopyrgos-Aigion area), one of the most active rifts in the Aegean region for which we have precise tectonic information. The network included 51 digital stations that operated during July and August 1991, covering a surface of  $40 \times 40$  km<sup>2</sup>. Among the 5000 recorded events with  $M_{\rm L}$  ranging between 1.0 and 3.0, we precisely located 774 events. We obtained 148 well-constrained focal mechanisms using P-wave first motions. Of these, 60 also have mechanisms obtained by combining the P-wave first motions with the S-wave polarization directions. The observed seismicity is mainly located between 6 and 11 km depth. Most of the fault-plane solutions correspond to E-W-striking normal faulting, in agreement with the geological evidence. Most of the well-determined mechanisms indicate a nodal plane dipping  $10-25^{\circ}$  due north and a steep south-dipping plane. A similar asymmetry is also seen in the seismicity distribution and in the overall geological structure of the Corinth Rift. We discuss this evidence and the inference of a deep detachment zone, a structure where the major faults seen at the surface appear to root. A large part of the microseismic activity appears to cluster in regions near the junctions of the main faults with the proposed detachment zone. This feature of the microseismicity is interpreted in terms of stress transfer and stress concentration in regions of probable nucleation of future large earthquakes.

Key words: fault-plane solutions, Greece, Gulf of Corinth, normal faulting, microseismicity.

#### **1** INTRODUCTION

One important problem in seismotectonics is to characterize the loading process on large active fault systems and to understand the temporal and spatial relationships between small-scale faulting, microseismicity and large destructive earthquakes. How strains accommodate near the base of the seismogenic layer where large earthquakes nucleate is of particular interest in understanding the mechanisms by which stresses build up. In the case of crustal extension, it is commonly accepted that the normal faults capable of generating large earthquakes usually cut the entire seismogenic layer, but how these faults root into the deeper semi-brittle and ductile layers extension (Covington 1983; Arabasz & Julander 1986; Logatchev & Zorin 1987; Maier & Eisbacher 1991; Wenzel et al. 1991). This implies the existence of crustal detachments or large shear zones dipping less than 30°. Studies of large continental normal-faulting earthquakes, however, show that they generally initiate in the upper brittle crust and the faultplane solutions do not exhibit low-angle nodal planes (e.g. Jackson & White 1989), with the possible exception of the Woodlark-D'Entrecasteaux earthquake (Abers 1991). In some large earthquakes, secondary rupture on low-angle normal faults has also been suggested (e.g. Eyidogan & Jackson 1985; Bernard & Zollo 1989a). However, the study of the deeper parts of the faults is hampered by the insufficiency of well-defined seismicity.

remains largely unknown. An asymmetric deep structure is

often inferred from seismic profiles for continental areas under

<sup>\*</sup> Now at: Observatoire Midi-Pyrénées-GRGS-CNRS UMR 5562, 14 Ave. E. Belin, 31400 Toulouse, France.

One possible way to define the fault geometry at depth is to study the deformation in the semi-brittle transition zone by means of its microseismic activity. This can be criticized because fault-plane solutions of microearthquakes do not usually show a simple pattern (e.g. Jackson & White 1989). The main difficulties with this method are (1) to appraise the relationship of the observed microseismic activity (recorded during short periods of time) with the seismic cycle, and (2) to ascribe this activity to the major faults or to the network of fractures surrounding them. A way to overcome these problems is to install very dense networks of portable seismological stations in rapidly deforming areas with high seismicity. However, previous experiments in Greece (Melis et al. 1989; Hatzfeld et al. 1990) and in the Basin and Range (Jones 1987) had no conclusive results about the normal-faulting geometry at depth, possibly because the deployed networks were not dense enough.

The Gulf of Corinth is one of the most prominent active rifts in the Aegean area, with a history of repeated large earthquakes and with a high level of background seismicity (Papazachos & Papazachos 1989; Ambraseys & Jackson 1990). Large earthquakes occurred in 1861 near the city of Aigion  $(M_w = 6.7)$  (Papazachos & Papazachos 1989), producing 13 km long surface breaks (Schmidt 1881), and in 1981 near Corinth, with a sequence of three events  $(M_s = 6.7, 6.4, 6.4)$  (Jackson *et al.* 1982; King, Oppenheimer & Amelung 1985) (Fig. 1). The geological evidence suggests an unusually fast Quaternary slip rate of the order of 1 cm yr<sup>-1</sup> on the major E–W-striking, north-dipping normal faults at the southern edge of the Corinth rift, which appears to be mostly an asymmetric structure (Armijo et al. 1996).

In 1991, we began a multidisciplinary study, which included the tectonics, the geodesy and the microseismicity of the Gulf of Corinth. Detailed accounts of the tectonic results are given elsewhere (Armijo et al. 1996), and a synoptic view of the overall work can be found in Rigo (1994). Here, we present the main results of an experiment in July and August 1991 with a dense network of digital seismological stations installed in the western part of the Gulf. The experiment was designed to cover, at the appropriate scale and with reasonably good hypocentral resolution, an area where the near-surface geometry of the main faults was well constrained. Previous background seismicity proved to be high in the region between the cities of Patras, Aigion and Navpaktos (Galanopoulos 1960, 1961; Melis et al. 1989; Hatzfeld et al. 1990; Amorese 1993). During our six week experiment we recorded a total of about 5000 events, providing us with a consistent data set from which we obtained accurate earthquake locations and well-constrained fault-plane solutions. We use this data together with the tectonic observations to bring constraints on the geometry of the faults and on the mechanism of normal faulting at depth.

#### 2 SEISMOLOGICAL DATA ANALYSIS

#### 2.1 Network and locations

The seismological network, composed of 51 digital portable stations (Fig. 2; Appendix A), covered an area about



Figure 1. Seismotectonic map of the Gulf of Corinth. Active faults are mapped from field observations and SPOT images (Armijo et al. 1996). Elevation contours are in feet. Fault-plane solutions of 1965–92 events with magnitude larger than 5 are from Ambraseys & Jackson (1990), Taymaz, Jackson & McKenzie (1991) and Briole et al. (1993). The epicentre of the 1861/12/26 earthquake (black dot) is from Schmidt (1881). a and b indicate locations of sections in Fig. 12. Do: Doumena; Gxd: Galaxidi; He: Helike; KI: Kalavrita; Ma: Mamousia; MP: Megas Pontias; Na: Navpaktos; Ps: Psathopyrgos; So: Souli. The inset outlines the area studied (Figs 2 and 8).



namo

22

12

Figure 2. Network in operation from 10/07/1991-26/08/1991. Coordinates of the stations are given in Appendix A.

**Digital Stations**  $\triangle$  one-component three-component 15 km

21 48

arak

22' 00'

 $40 \text{ km} \times 40 \text{ km}$ , with an average distance between stations of 3-6 km. The stations were equipped with 1 or 2 Hz seismometers. The 21 one-component stations had a recording frequency of 100 Hz; for the three-component stations, 15 had a recording frequency of 125 Hz, 12 had one of 200 Hz, and 3 had one of 62.5 Hz. Absolute time was given by the DCF time code recorded in parallel with the internal station clock for all three-component stations. For the one-component stations, the internal clock was permanently reset on the DCF time code. Thus the time accuracy is estimated to be better or of the order of the sampling rate. The time-reading precision is estimated to be between 0.005 and 0.06 s for P waves, and between 0.01 and 0.1s for S waves, depending on the recording system.

38' 00

About 5000 events with magnitude  $M_L$  between 1 and 3.0 were recorded during the six weeks of the experiment. Here, we analyse a subset of 850 events recorded by at least five stations during the month of August when the network was completely installed. The hypocentral locations were computed using the Hypo71 code (Lee & Lahr 1975). As no crustal velocity structure is available for the area, we constructed a mean velocity model from our data set. We estimated the  $V_p/V_s$ ratio to be  $1.80 \pm 0.02$  from Wadati diagrams constructed using the three-component records only. This ratio is in agreement with the values ranging between 1.77 and 1.83 obtained in the neighbouring areas (e.g. King et al. 1985; Melis et al. 1989; Hatzfeld et al. 1990; Amorese 1993). We first determined the mean P velocity between 0 and 15 km depth by studying the variation of the mean rms traveltime residual with respect to

this mean velocity (Fig. 3). The mean rms is minimum between 5.4 and 5.7 km s<sup>-1</sup>. Then, taking a velocity of 5.7 km s<sup>-1</sup> as a reference, we computed the number of events for which the rms decreases when using a different velocity. For a value of 5.6 km s<sup>-1</sup>, 90 per cent of the events have their rms reduced. A similar result was obtained with other reference velocities. We thus used a 5.6 km s<sup>-1</sup> mean P velocity between 0 and 15 km (model 1-Table 1). Comparable mean velocities were found in the area (e.g. King et al. 1985; Melis et al. 1989; Amorese 1993). Our data provide no information on the velocity below 15 km depth because of the lack of events at these depths. We thus fixed the velocities there as in the previous studies mentioned above (Table 1). We determined a



Figure 3. Mean location rms for the 850 selected events versus assumed mean P-wave velocities between 0 and 15 km depth. Error bars represent standard deviation.

Table 1. *P*-wave velocity models used for the earthquake locations.  $V_p/V_s = 1.80$ .

	Model 1	Model 2
Depth (km)	Vp (km/s)	Vp (km/s)
0.0 - 4.0		4.8
4.0 - 7.2		5.2
7.2 - 8.2	5.6	5.8
8.2 - 10.4		6.1
10.4 - 15.0		6.3
15.0 - 30.0	6.5	6.5
> 30.0	7.0	7.0

multilayer model (model 2—Table 1), keeping the 5.6 km s<sup>-1</sup> mean P velocity in the upper 15 km, which appears to be the most appropriate for fault-plane solutions (see detailed discussion in Section 2.2). This model was then used to determine both the event locations and the fault-plane solutions.

Owing to the geometry and the density of the network, event locations are very well constrained. We performed two tests to assess the precision of focal depths. First, we compared results obtained using initial depths of 5 and 20 km with Hypo71. Second, we compared results obtained with velocity models 1 and 2. We rejected events for which the focal depth varied by more than 2 km to select a final set of 774 events with a precision of about  $\pm 2$  km for focal depths and  $\pm 1$  km for the epicentral positions (Appendix B). The final mean rms traveltime residual for this final set of events is  $0.11\pm0.04$  s.

#### 2.2 Fault-plane solutions

The fault-plane solutions were determined in two steps. First they were constructed by hand using only the P first motions. Then, when it was possible, they were better constrained using S-wave polarization directions, following the method developed by Zollo & Bernard (1991). In order to guarantee the quality of the determinations, we selected events with at least 10 clear P polarities. This restriction gave us a set of 190 events.

Velocity model 1 did not yield fault-plane solutions for many of these events because the ray's angle of incidence was too small, making it impossible to draw two perpendicular nodal planes. (See, for example, events 398 and 50 in Fig. 4.) The multilayer velocity model 2 was constructed to determine faultplane solutions for a maximum number of events. As a first step, we proceeded by trial and error, using the 190 selected events, to introduce layers between 0 and 15 km in order to transform some direct rays into refracted rays (e.g. event 50, Fig. 4) which are clearly observed on the records. In the resulting model, the depths of the velocity interfaces are mainly constrained by the depth of the events. Clearly model 2 does not correspond to a unique solution, but it is the best layered model that we could find to reduce polarity inconsistencies in the fault-plane solutions. Tests were performed to assess the stability of the fault-plane solutions with respect to the velocities in the layers and the position of the interfaces. Because of the high density of stations in the network, fault-plane solutions are more sensitive to the location of interfaces than to the velocities in each layer. The 3-D smoothly varying velocity model obtained by tomographic inversion with the same set of data (Le Meur 1994) is consistent with model 2. The interfaces of model 2 correspond to the higher gradients of Le Meur's model. Additionally, focal mechanisms determined with model 1 did not significantly change with model 2 (e.g. event



Figure 4. Focal mechanisms of four events (Appendix B) with two different velocity models (models 1 and 2, Table 1). P polarities are plotted on the lower equal-area hemisphere of the focal sphere. Dots represent direct rays, triangles refracted rays. Fault planes are drawn when possible. Note that in model 2 the incidence angles are increased and refracted rays are present.

188, Fig. 4). Finally, we obtained a total of 148 focal mechanisms, of which about 30 are not well constrained (e.g. event 97 in Fig. 4).

As a second step to constrain fault-plane solutions better, we combined P-wave polarities with S-wave horizontal polarization directions to estimate the fault-plane parameters (Zollo & Bernard 1991; de Chabalier et al. 1992). For such a study, the S-wave polarization must be stable in time and linear. This implies the use of incidence angles smaller than 45°. For larger incidences, free-surface effects can be important, inducing the instability of S-wave polarization (Evans 1984; Booth & Crampin 1985; Bernard & Zollo 1989b). To obtain more stable polarizations, the records were bandpass-filtered between 1 and 3 Hz with a zero-phase-shift Butterworth filter. However, few stations show very clear splitting of S waves due to crustal anisotropy (Bouin, Téllez & Bernard 1996) with time delays larger than 0.05 s between the slow and the rapid S arrivals. These data were not used in the inversion. Then, each selected three-component record was examined for S-polarization stability. In Fig. 5 we present an example of the determination of the S-wave polarization direction at station krin for event 447. The initial record (Fig. 5a) is filtered between 1 and 3 Hz (Fig. 5b). We represent the 3-D particle movement vector at a constant time interval on a horizontal stereographic projection for a short temporal window (1 s) for the P wave and the S wave. We can thus check that the P-wave incidence is vertical. If the S-wave polarization is stable and linear with time, the points cluster (each point representing the particle vector at a given time on the stereographic projection) around the direction of the S-wave polarization (west in the example of Fig. 5). The average values of the azimuths and incidence angles of the particle movement vector at the surface define the S-wave mean polarization direction and incidence angle. The nearer to the horizontal the S incidence angle is, the better the datum. The accuracy of the polarization direction depends on the size of the particle movement vector cluster, i.e. on the stability of the S-wave polarization with time. This accuracy is globally estimated to be 10-15°. Thus, for 60 events out of the 190 selected earlier, we were able to add information by including the S-wave polarization directions.

We then performed the inversion for each mechanism by searching for the best fault-plane solution corresponding to the observed P polarities and S-wave polarization directions. Because of the non-linearity of the problem, the inversion is a systematic exploration of the fault-plane parameter space (strike, dip, slip) to find the maximum of a probability density function (Brillinger, Udias & Bolt 1980; Zollo & Bernard 1991). The result of the joint inversion of P polarities and Spolarization directions for event 491 is shown in Fig. 6. The probability density function is represented by the 66, 90 and 99 per cent levels on the entire fault-plane parameter space. The clusters represent the conjugate fault planes (P1 and P2 in Fig. 6). The estimated values for strike, dip and slip are given by the position of the maximum of the density function for each nodal plane. In the example of Fig. 6, the values are: strike =  $211.0^\circ$ , dip =  $70.0^\circ$  and slip =  $-150.4^\circ$ . The uncertainties on these values can be estimated from the area with 66 per cent probability. For a given slip and dip, the uncertainty on the strike is close to 30°; for a given strike, the uncertainties on slip and dip range between 10° and 30°. Because we have to consider the three fault-plane parameters A microseismic study of the Gulf of Corinth 667

## Event 447 - Station krin (krini)



Figure 5. Example of determination of shear-wave direction of polarization. (a) Initial three-component record. (b) Same record filtered between 1 and 3 Hz (top), with particle movement vector on horizontal stereographic projection for P waves (bottom-left) and S waves (bottom-right). The time window used for P and S waves is indicated on the filtered records by horizontal lines. The direction and the dip of the S-wave polarization obtained here are 90.0° and 7.5° ( $\pm$  3.4°), respectively.

together, the overall uncertainty of each of these parameters is about  $\pm 15^{\circ}$ .

The four examples in Fig. 7 illustrate the improvement brought by our method. We compare here the mechanisms obtained with the P first motions only and the mechanisms from the joint inversion of P polarities and S-polarization directions. In general, the addition of S-polarization directions constrains the mechanisms better. In a few cases, however (e.g. event 447, Fig. 5), the fit of S-polarization directions may be slightly worse for the inversion solution than the one obtained



Figure 6. Result of the joint inversion of P polarities and S-wave polarization directions for event 491. Representation of the probability density function in the fault-plane parameter space (strike, dip, slip). The 66, 90 and 99 per cent confidence levels are represented with decreasing symbol sizes. The clusters correspond to the two conjugate fault planes P1 and P2.

by hand. This is related to the shape of the conditional probability density function used in the inversion. Because this function has a finite width around nodal planes, the algorithm naturally tends to favour solutions in which no station is very close to a nodal plane. In any case, variations in strike and dip between the two methods are small and within the uncertainties when both kinds of data (P and S) are well explained. In other cases, such as event 475, the mechanism, which was not well constrained in the manual solution, changes to a N-S- rather than a NW-SE-trending normal fault. Finally, events 92 and 97 (Fig. 5), which were badly constrained by the P polarities alone, are now better resolved.

We determined 148 focal mechanisms (Appendices C and

D). In the interpretation, we always choose the solution from the joint inversion, if it exits.

#### 3 EARTHQUAKE AND FOCAL MECHANISM DISTRIBUTION

The seismicity appears to be located beneath the Gulf and a few kilometres inland on both sides of the Gulf (Fig. 8). More activity is observed on the northern side. In addition to some distributed background seismicity, three main clusters are identified: the cluster near the city of Aigion (Cl1), which was very active during the 2 months of the experiment and should be associated with the  $M_L=4.5$  event that occurred there on



Figure 7. Comparison between focal mechanisms determined with P polarities only (left) and the focal mechanisms determined by joint inversion of P polarities and S-wave polarization directions (right). Thick lines are observed shear-wave polarizations and thun lines are calculated ones.

July 3; cluster Cl2, active during the month of August, with two  $M_L = 2.8-3.0$  events (47 and 677); and the cluster of August 24 (Cl3) with magnitude 2.0-2.8 events. The largest recorded events, both of magnitude  $M_L = 3.0$ , are the August 5 event (156 in Appendix B) and the August 23 event (677 in Appendix B).

The depth distribution of the events (Fig. 9) indicates that the maximum of activity is concentrated at 6-10 km depth. Moreover, 98 per cent of the events have focal depths less than 13-14 km. We deduce that the thickness of the seismogenic layer in the Patras-Aigion area does not exceed 15 km, considering the focal depth uncertainties of  $\pm 2$  km. This is in agreement with the aftershock study of the 1981 Corinth earthquakes by King et al. (1985), who found fewer than five events deeper than 15 km in the Corinth-Perachora region among a set of 133 well-located events. Another aspect of this vertical distribution is the absence of events shallower than 4 km (Fig. 9). We checked that this was not an artefact of our selection criteria for events. This small shallow activity is probably related to the rheological property of the shallow crustal layers, as suggested by King et al. (1994) for the San Andreas fault zone.

The distribution of the seismicity does not outline the geometry of the active faults at depth (Fig. 10). In the western part of the network (a1 and a2 in Fig. 10), the events align along an apparent geometry dipping  $10^{\circ}-20^{\circ}$  north between 7 and 12 km depth, including cluster Cl2. This geometry does not appear clearly in the eastern sections (b and c in Fig. 10), except if we consider that it is outlined by the lower limit of the seismicity. Nevertheless, clusters Cl2 and Cl3 are in the down-dip extension of the Psathopyrgos fault (P in Fig. 10) and the Aigion fault (Ai in Fig. 10), respectively.

The fault-plane solutions yield a consistent N-S direction of extension, in agreement with the large-scale tectonics of this area (Fig. 11). The majority of the mechanisms correspond to E-W-trending normal faulting consistent with the strike of the active faults. Few strike-slip and reverse fault-plane solutions are observed (e.g. 8, 86, 294, 308, and 358 in Appendix C).

Normal-faulting mechanisms with T axes oriented N–S and nodal planes dipping north or south between  $35^{\circ}$  and  $70^{\circ}$  are found in the eastern part of the network (Fig. 11a). The mean T axes for clusters Cl1 and Cl3 are subhorizontal in both cases (Table 2).

Normal-faulting mechanisms with a N–S-oriented T axis plunging approximately 30° are found in the western part of the network (Fig. 11b). They represent normal faulting with an E–W nodal plane dipping  $75^{\circ}-85^{\circ}$  south and the other nodal plane dipping  $10^{\circ}-25^{\circ}$  north. Most of these mechanisms are well constrained by S-wave polarization directions. These peculiar fault-plane solutions are found in cluster Cl2 but also south and northwest of it.

#### **4 DISCUSSION**

To assess the significance of microearthquakes within a volume of crustal rocks with major active faults is a difficult problem.

Table 2. Mean P and T axes for each cluster deduced from faultplane solutions. Uncertainties are  $10^{\circ}$  for the strike and  $5^{\circ}$  for the plunge.

Cluster	Mean	P Axis	Mcan 1	r Axis
	Strike (°)	Plunge (°)	Strike (°)	Plunge (°)
Cli	103.4	78.8	184.9	13.0
Cl2	354.9	66.0	187.5	29.8
CI3	179.7	70.8	341.4	23.8



Figure 8. Locations of the 774 selected events. Segments a1, a2, b and c correspond to the sections shown in Fig. 11. Cl1, Cl2 and Cl3 indicate the three main clusters.



Figure 9. Vertical distribution of the 774 selected events. Uncertainties on focal depths are  $\pm 2$  km. 80 per cent of the activity is located between 6 and 10 km depth.

An event of magnitude smaller than 3 is not necessarily associated with slip on a major fault. Such an event corresponds to a source radius smaller than 300-400 m with only a few millimetres of slip. Thus, microearthquakes may be associated with major fault planes but also with minor faults. The presence of fractures or fracture zones in the upper crust is commonly assumed in active tectonic regions, where they are often observed near fault planes (Chester & Logan 1986; Scholz 1990). During the interseismic period, stress accumulation and elastic deformation of the crust around major fault planes can induce microseismic activity within rock volumes of the order of a few tens of cubic kilometres. Zones where microseismic activity is likely to be concentrated are the process zones near the extremities of major fault planes where stresses accumulate (Cottrell 1964), or highly fractured regions located above ductile shear zones. Microseismicity may also represent internal deformation of blocks bounded by large faults (Fuchs *et al.* 1987; Jackson & White 1989; Echtler, Lüchen & Mayer 1994).

If the occurrence of microevents is controlled by a preexisting network of fractures near major fault planes, where stresses may be locally modified, then some focal mechanisms may not be consistent with those expected from the large-scale tectonics. This is the case for the reverse and the few strikeslip events observed (e.g. events 8, 39, 79, 86, 294; Appendices C and D). All of these events are compatible with minimum horizontal (compressive) stress oriented N–S. However, modification of stresses may also be transient, for instance in response to slip episodes on major faults (e.g. Lyon-Caen *et al.* 

A microseismic study of the Gulf of Corinth 671



Figure 10. Vertical sections of seismicity (see Fig. 8 for location), with no vertical exaggeration. The half-width of projection is 6 km. Active faults observed at the surface have been extrapolated to a depth of 5 km with a dip of  $50^\circ$ . P: Psathopyrgos fault; H: Helike fault, Ai: Aigion fault; M: Mamousia fault.

© 1996 RAS, GJI 126, 663-688



Figure 11. Maps with the 148 calculated fault-plane solutions. The size of the sphere (lower hemisphere) is proportional to magnitude. Grey fault-plane solutions are those within the three main clusters Cl1, Cl2 and Cl3. (a) Focal mechanisms in the western part of the network. (b) Focal mechanisms in the castern part of the network. Numbers refer to events in Appendices B and C.

1988). This may be the case for cluster Cl1, which represents aftershocks of the  $M_L = 4.5$  earthquake of July 3, 1991.

The two sections in Fig. 12 show the observed seismicity and some representative fault-plane solutions, with the geological information. In the western part of the network

(section a, Fig. 12) the distribution of the seismicity with depth increasing towards the north is consistent with the gently north-dipping nodal planes of the focal mechanisms (events 312, 491, 639, 677) and with the mean P and T axes of cluster Cl2. A likely interpretation is that a low-angle normal fault or a detachment zone occurs between 9 and 11 km depth, dipping north at about  $15^{\circ}$ . The seismicity could also be associated with slip on small antithetic faults corresponding to the nodal planes dipping steeply to the south. However, a network of such antithetic faults with the geometry given by the observed seismicity distribution may also accommodate overall strain compatible with the proposed detachment zone. If the dip of the Psathopyrgos fault decreases from 50° as observed at the surface to less steep values at depth, then it would connect with the detachment in the region of cluster Cl2. The intersection of the two fault zones would be a likely place for increased fracturing and thus for generating microseismic activity. The possible upward and downward extensions of the proposed detachment are difficult to define due to the lack of observed microevents. Nevertheless, it seems likely that the detachment extends down-dip to the north, dying out in the ductile lower part of the crust, where it would become aseismic.

The relationship between the spatial event distribution, the focal mechanisms and the surface geology in the eastern part of the network (section b, Fig. 12) appears to be more complex than to the west. The occurrence of a detachment on section b can only be justified by the geometry of the observed seismicity and would correspond to the lower limit of the seismogenic layer. This lower limit appears to dip gently northwards, although no determined fault-plane solution is



Figure 12. Interpretative sections (locations in Fig. 1). Only a few representative fault-plane solutions have been projected on the vertical plane. Insets represent mean P and T axes for clusters Cl2 and Cl3. The active major normal faults documented at the surface connect with the northwarddipping plane (shaded), consistent with the spatial distribution of seismicity and the gently north-dipping nodal planes of the western focal mechanisms.

clearly associated with it. As in section a, the major active normal faults documented at the surface (the Mamousia, Helike and Aigion faults) may connect with the hypothetical detachment at depth. Small antithetic faults probably related to flexure of the hanging wall have been recognized in the field (Fig. 1). Because the total amount of N-S extension is greater in section b than in section a, the hanging wall (northern part of the Gulf) may also be more fractured (Rigo 1994; Armijo et al. 1996). Part of the observed shallow (0-15 km) seismicity in the hanging wall of the Helike-Aigion faults could be associated with such flexure-related antithetic faulting, in agreement with the 60°-65° south-dipping nodal planes of some mechanisms (dashed lines in section b, Fig. 12). Farther north in the hanging wall, cluster Cl3 is located at an average depth of about 10 km. The mean P axis of cluster Cl3 is steeper than those of clusters Cl1 and Cl2 (Figs 12, 10 and 9). Also, unlike the other two clusters, the mean T axis of cluster Cl3 plunges to the north (Table 2; Fig. 12, section b). Cluster Cl3 may thus be associated with gently south-dipping faulting above the detachment. Finally, the Aigion cluster (Cl1, Fig. 9) is located roughly in the region where the downward extension of the Mamousia fault may connect with the proposed detachment (Fig. 12). However, the seismicity associated with this cluster appears to diffuse over almost all of the lower part of the block bounded by the Mamousia and the Helike faults.

#### **5** CONCLUSIONS

Because of the high resolution of the data presented here, we can provide a precise, instantaneous image of the deforming study area. This high resolution enables us to describe precisely the mechanisms of small earthquakes and to draw some inferences about the large-scale geometry and mechanics of extension in the Gulf of Corinth. The data set suggests the existence, beneath the Gulf of Corinth, of a detachment zone that contributes significantly to the overall deformation process. All the large active normal faults mapped appear to connect downwards with the proposed detachment at around 10 km depth. The geometry of the detachment would be that of a normal fault dipping  $15^{\circ} (\pm 10^{\circ})$  northwards, as revealed by the studied seismicity. This is similar to the geometry and mechanism suggested by King *et al.* (1985) for the eastern part of the Corinth Gulf in the Corinth–Perachora region.

Except for cluster Cl2, the observed cluster activity does not exhibit a simple geometry associated with any particular fault. Fault-plane solutions can be quite varied within one cluster, as in the Aigion cluster (Cl1). The cluster microearthquake activity is likely to be mostly located on small structures, antithetic faults or fracture zones located near the extremities of the large faults.

To evaluate roughly the total seismic moment released by the 774 well-located events in the network, we use the formula relating the magnitude  $M_L$  to the seismic moment  $M_0$  established in the Volos region in Central Greece (log  $M_0=1.5$  $M_L+9.0$ ; Makropoulos, personal communication). The total seismic moment released during the 30 day period is of the order of  $0.3-3.0 \times 10^{16}$  N m, which corresponds to an event with an  $M_s$  of 4.3-4.9. This represents quite a high rate of diffuse deformation which is unlikely to be a permanent feature. Previous seismicity experiments in the area indicate activity beneath the Gulf between Patras and Aigion (Melis *et al.* 1989) and on the northern side of the Gulf (Hatzfeld *et al.* 1990).

#### A microseismic study of the Gulf of Corinth 673

Because the resolution of these studies is much poorer than the one presented here, it is difficult to make valid comparisons. However, it appears that the Aigion cluster Cl1 was not active at the time of these experiments (1983-84 and 6 weeks during 1986). Thus, the cluster activity probably changes with time, contributing to the redistribution of stress at some depth. In the Gulf of Corinth, the focal depths of large earthquakes occur near the base of the seismogenic layer at 10-15 km depth, as in other regions under extension throughout the world (Sibson 1982; Meissner & Strehlau 1982; Jackson & White 1989). Therefore, we suggest that the microseismic activity observed corresponds to episodes of stress transfer from the lower semi-brittle zone to the upper brittle zone, through slip on a detachment zone. This process may cause stresses to concentrate in regions near the base of the large steep faults seen at the surface. Such regions are likely places for large normal-faulting earthquakes to initiate their rupture. However, our observations do not tell us if this activity represents to some extent the initiation of a preseismic stage. That the microseismic activity is most probably transient suggests that the stress accumulation near the large faults may operate in cycles with small spatial extent and short duration which may only correspond to discrete episodes during the main seismic cycle.

#### ACKNOWLEDGMENTS

The authors thank all the participants of the summer 1991 field experiment. We also thank Geneviève Patau for reading some of the seismograms, Bertrand Meyer for helpful discussions and Kurt Feigl for a helpful reading of manuscript. The Direction aux Risques Majeurs (DRM) and Institut National des Sciences de l'Univers (INSU) provided financial support. We also benefited from EEC EPOCH Programme support. This is IPGP contribution no. 1427.

#### REFERENCES

- Abers, G., 1991. Possible seismogenic shallow-dipping normal faults in the Woodlark-D'entrecasteaux extensional province, Papua New Guinea, *Geology*, 19, 1205–1208.
- Ambraseys, N.N. & Jackson, J.A., 1990. Seismicity and associated strain of Central Greece between 1890 and 1988, *Geophys. J. Int.*, 101, 663-708.
- Amorese, D., 1993. Sismotectonique et déformation actuelle de la terminaison nord occidentale de l'Arc Égéen (Iles Ioniennes, Acharnanie, Épire, Grèce), Thèse de Doctorat de 3ème cycle, Université Joseph Fourier, Grenoble, France.
- Arabasz, W.J. & Julander, D.R., 1986. Geometry of seismically active faults and crustal deformation within the Basin and Range— Colorado Plateau transition in Utah, Spec. Pap. Geol. Soc. Am., 208, 43-74.
- Armijo, R., Meyer, B., King, G.C.P., Rigo, A. & Papanastassiou, D., 1996. Quaternary evolution of the Corinth Rift and its implications for the Late Cenozoic evolution of the Aegean, *Geophys. J. Int.*, 126, 11-53
- Bernard, P. & Zollo, A., 1989a. The Irpinia (Italy) 1980 earthquake: detailed analysis of a complex normal fault, J. geophys. Res., 94, 1631-1647.
- Bernard, P. & Zollo, A., 1989b. Inversion of near source S polarization for parameters of double couple point sources, Bull. seism. Soc. Am., 79, 1779–1809.
- Booth, D.C. & Crampin, S., 1985. Shear wave polarizations on a

curved wavefront at an isotropic free surface, Geophys. J. R. astr. Soc., 88, 31-45.

- Bouin, M.P., Téllez, J. & Bernard, P., 1996. Seismic anisotropy around the Gulf of Corinth, Greece, deduced from three-component seismograms of local earthquakes and its relationship with crustal strain, J. geophys. Res., 101, 5797-5811.
- Brillinger, D.R., Udias, A. & Bolt, B.A., 1980. A probability model for regional focal mechanism solutions, Bull. seism. Soc. Am., 70, 149-170.
- Briole, P., Deschamps, A., Lyon-Caen, H., Papazissi, K. & Martinod, J., 1993. The Itea ( $M_s = 5.9$ ) earthquake of November 18, 1992. Characteristics of the main shock inferred from body waves and ground displacement analysis, *Proc. 2nd Cong. of the Hellenic Geophys. Un. in Florina*, 1, 297-308.
- Chester, F.M. & Logan, J.M., 1986. Implications for mechanical properties of brittle faults from observations of the Punchbowl fault zone, California, Pageoph., 124, 79-106.
- Cottrell, A.H., 1964. The Mechanical Properties of Materials, John Wiley and Sons, New York, NY.
- Covington, H.R., 1983. Structural evolution of the Raft River Basin, Idaho, Geol. Soc. Am. Memoir, 157, 229-237.
- De Chabalier, J.B., Lyon-Caen, H., Zollo, A., Deschamps, A., Bernard, P. & Hatzfeld, D., 1992. A detailed analysis of microearthquakes in western Crete from digital three-component seismograms, *Geophys. J. Int.*, 110, 347-360.
- Echtler, H.P., Lüschen, E. & Mayer, G., 1994. Lower crustal thinning in the Rhinegraben: Implications for recent rifting, *Tectonics*, 13, 342-353.
- Evans, R., 1984. Effects of the free surface on shear wavetrains, Geophys. J. R. astr. Soc., 76, 165-172.
- Eyidogan, H. & Jackson, J., 1985. A seismological study of normal faulting in the Demirci, Alasehir and Gediz earthquakes of 1969-70 in western Turkey: implications for the nature and geometry of deformation in the continental crust, *Geophys. J R. astr. Soc.*, 81, 569-607.
- Fuchs, K., Bonjer, K.-P., Gajewski, D., Lüschen, E., Prodehl, C., Sandmeier, K.-J., Wenzel, F. & Wilhelm, H., 1987. Crustal evolution of the Rhinegraben area. 1. Exploring the lower crust in the Rhinegraben rift by unified geophysical experiments, *Tectonophysics*. 141, 261-275.
- Galanopoulos, A.G., 1960. Greece, a catalogue of shocks with  $I_0 \ge VI$  or  $M \ge 5$  for the years 1801–1958, Academy of Science, Athens.
- Galanopoulos, A.G., 1961. Greece, a catalogue of shocks with  $I_0 \ge VII$  for the years prior to 1800, Academy of Science, Athens.
- Hatzfeld, D., Pedotti, G., Hatzidimitriou, P. & Makropoulos, K., 1990. The strain pattern in the Western Hellenic Arc deduced from a microearthquake survey, *Geophys. J. Int.*, 101, 181-202.
- Jackson, J.A. & White, N.J., 1989. Normal faulting in the upper continental crust: observations from regions of active extension, J. Struct. Geol., 11, 15-36.
- Jackson, J.A., Gagnepain, J., Houseman, G., King, G.C.P., Papadimitriou, P., Soufleris, C. & Virieux, J., 1982. Seismicity, normal faulting and the geomorphological development of the Gulf of Corinth (Greece): the Corinth earthquakes of February and March 1981, Earth planet. Sci. Lett., 57, 377-397.

- Jones, H.C., 1987. A geophysical and geological investigation of extensional structures, Great Basin, Western United States, *PhD thesis*, Massachusetts Institute of Technology, Cambridge, MA.
- King, G.C.P., Ouyang, Z.X., Papadimitriou, P., Deschamps, A., Gagnepain, J., Houseman, G., Jackson, J.A., Soufleris, C. & Virieux, J., 1985. The evolution of the Gulf of Corinth (Greece): an aftershock study of the 1981 earthquakes, *Geophys. J. R. astr. Soc.*, 80, 677–683.
- King, G.C.P., Oppenheimer, D. & Amelung, F., 1994. Block versus continuum deformation in the western United States, *Earth planet*. *Sci. Lett.*, 128, 55–64.
- Lee, W.H.K. & Lahr, J.C., 1975. HYPO71 (revised): a computer program for determining hypocenter, magnitude and first motion pattern of local earthquakes, US Geol. Survey Open-File report, 75-311, 116 pp.
- Le Meur, H., 1994. Tomographie tridimensionnelle à partir des temps des premières arrivées des ondes P et S, application à la région de Patras, *Thèse de Doctorat de 3ème cycle*, Université Paris 7, France.
- Logatchev, N.A. & Zorin, Y.A., 1987. Evidence and causes of the twostages development of the Baikal rift, *Tectonophysics*, 143, 225-234.
- Lyon-Caen, H., Armijo, R., Drakopoulos, J., Baskoutas, J., Delibassis, N., Gaulon, R., Kouskouna, V., Latoussakis, J., Makropoulos, K., Papadimitriou, P., Papanastassiou, D., Pedotti, G., 1988. The 1986 Kalamata (South Peloponnesus) earthquake: detailed study of a normal fault and tectonic implications, J. geophys. Res., 93, 14 967-15 000.
- Maier, L. & Eisbacher, G.H., 1991. Crustal kinematics and deep structure of the northern Rhine Graben, Germany, *Tectonics*, 10 (3), 621–630.
- Meissner, R. & Strehlau, J., 1982. Limits of stress in continental crust and their relation to the depth-frequency relation of shallow earthquakes, *Tectonics*, 1, 73-89.
- Melis, N.S., Brooks, M. & Pearce, R.G., 1989. A microearthquake study in the Gulf of Patras region, western Greece, and its seismotectonic interpretation, *Geophys. J. R. astr. Soc.*, 98, 515–524.
- Papazachos, B. & Papazachos, K., 1989. The Earthquakes in Greece, Thessaloniki, Ziti Publications, Greece (in Greek).
- Rigo, A., 1994. Étude sismotectonique et géodésique du Golfe de Corinthe (Grèce), *Thèse* de *Doctorat de 3ème cycle*, Université Paris 7, France.
- Schmidt, J.F.J., 1881. Studien über Vulkans und Erdbeben, C. Scholtze, Leipzig (in German).
- Scholz, C.H., 1990. The Mechanics of Earthquakes and Faulting, Cambridge University Press, Cambridge.
- Sibson, R.H., 1982. Fault zone models heat flow and depth distribution of earthquakes in the continental crust of the United States, Bull. seism. Soc. Am., 72, 151-163.
- Taymaz, T., Jackson, J. & McKenzie, D., 1991. Active tectonics of the north and central Aegean Sea, Geophys. J. Int., 106, 433–490.
- Wenzel, F., Brun, J.P. & ECORS-DEKORP working group, 1991. A deep reflection seismic line across the northern Rhine Graben, Earth planet. Sci. Lett., 104, 140-150.
- Zollo, A. & Bernard, P., 1991. Fault mechanisms from near source data: joint inversion of S polarizations and P polarities, *Geophys.* J. Int., 104, 441-451.

Sites	latitude (°N)	longitude (°E)	Sites	latitude (°N)	longitude (°E)
daph	38°25.27'	22°06.21'	marm	38°24.66'	21°49.71'
pyrg	38°24.64'	22°00.99'	pale	38°30.02'	21°50.70'
kout	38°24.04'	22°13.07'	eupa	38°26.13'	21°55.36'
varn	38°27.88'	21°57.58'	iaso	38°13.68'	21°48.94'
trik	38°26.76'	21°54.20'	mira	38°09.31'	21°51.10
triz	38°21.79'	22°04.30'	агта	38°15.96'	21°58.96'
scal	38°25.24'	21°50.48'	piti	38°15.97'	21°53.90'
neok	38°29.30'	21°50.48'	anoz	38°18.76'	21°56.89'
velv	38°23.38'	21°45.98'	arak	38°08.10'	21°57.44'
avor	38°28.04'	22°08.23'	liko	38°13.44'	21°56.60'
rigl	38°28.83'	21°46.05'	mamo	38°09.41'	22°07.92'
rig2	38°28.21'	21°44.84'	taxi	38°10.71'	22°02.42'
thio	38°29.52'	22°00.08'	kefa	38°11.24'	21°49.59'
tolo	38°22.41'	22°11.37'	tran	38°15.74'	21°51.12'
psar	38°19.51'	22°11.07'	kmri	38°13.42'	22°02.23'
limn	38°32.45'	21°58.01'	pant	38°08.48'	22°03.67'
dori	38°30.81'	22°09.61'	ptge	38°11.47'	22°06.22'
pano	38°22.97'	22°16.30'	krin	38°11.54'	21°57.11'
vrai	38°26.99'	22°11.24'	derv	38°10.31'	22°08.24'
poti	38°28.77'	22°04.43'	agge	38°12.97'	22°05.20'
palp	38°28.77'	21°52.70'	rodo	38°15.65'	22°01.71'
pits	38°25.93'	21°44.89'	akas	38°16.62'	21°50.76'
krok	38°31.87'	22°04.27'	dafn	38°12.49'	22°00.30'
mala	38°26.38'	22°15.16'	fter	38°09.36'	22°04.61'
elai	38°23.36'	22°07.08	argi	38°16.96'	21°51.56'
kmro	38°24.70'	21°56.93'	univ	38°17.32'	21°47.33'
klim	38°25.21'	21°58.09'	rodi	38°19.42'	21°53.87'
palr	38°27.78'	21°52.23'	laka	38°14.67'	21°58.76'
sote	38°25.66'	22°10.71'	koul	38°14.33'	22°05.18'
kamb	38°27.20'	22°00.54'	koun	38°11.19'	22°00.72'
kali	38°23.61'	22°08.45'	mal 1	38°22.37'	21°52.68'
serg	38°24.82'	22°03.43'	mal2	38°22.81'	21°54.22'

# APPENDIX A: COORDINATES OF STATIONS DURING THE 1991 EXPERIMENT

APPEND	IX B: EVENI	TLOCATIC	ONS FROM	НУРС	71.						Date	Time	Lat	Long	Depth ER2	. Mag	. RM	S ERX	ER)	n.evt
Time origi	in time (h mn	s); Lat.: lat	itude N (°mn	I); Lon	8:: lo	agitude	E E E	un); d	spth in	km; ERZ:	910802	13 2216.11	38 14.61	22 5.30	7.32 0.4	2.50	0.14	0.5	0.2	8
precision (	on the focal d	epth in Km; n V and ED	Mag.: Magr	litude l	MI; K	MJ: K	001 IV	lean S	quare	or une com-	910807	20.0026 61	38 14 28	6C.C 22	5 20 1 7	2,4		5.0		2 5
puted loca	ation in sec; E	KA anu EN	i i								010800	10.2020 CI	14 11 00	57 4 77 5 4 5 6	7.1 07.6	34 6				3 3
precision (	on the epicent	irai position									010807	10.2 20 21	38 14 77	22 5 21	0.1 U.S. 5					5 2
											010807	14 456 33	38 14 46	22 5 20	0.0 0.0 6 7 0 6 6	100		33	36	3 2
,	i			Tree of		r Mac	Ma	C ED	C ED	/ n evt	010800	15 2126 96	20 14 04	19 19 10	0.0 72.0					R 6
Date	l'ime	1.21 20 70 67	20 12 37	ndba		your ,			12	-	910802	17 5847 76	38 14 28	10.20 12	6.87 0.64	50.4			7.0	ñŸ
102016	11.0001 1	20.02 00	1011 11	PC 8		00.0		5	40		010807	1831052	38 74 74	21 58 13	10 18 03					٩ <b>9</b>
108010	10.05.11	991185	21 49 MR	5.23	20	2.26	0.13	0.6	0.4	. ••	910802	19 5 9 59	38 21.71	22 13.86	11.65 0.4	4.6		5 č	70	68
100016	C7.0010 1	38 27 12	22 12 47	11.21	0.3	2.37	0.0	0.2	0.3	9	910802	19 4122.67	38 18.35	22 10.45	7.50 0.3	2.96	0	3 8	5 2	3 5
100010	41 UC7 7	39 14 71	27 6 40	5 74	80	2.5.2	5	0.4	0.4	7	910802	19 5337.05	38 15.01	22 4 88	637 09					5 5
100010	e 1438 M	38 14 77	22 6.80	104	0.2	2.60	0.10	0.3	0.3	- 00	910802	20 27 8.75	38 14.91	22 4.42	7.14 0.2	2		22	3 8	3 2
100010	10.45.0.37	38 14 00	22 6.23	6.78	03	2.23	0.15	0.3	0.3	6	910802	21 38 2.25	38 11.34	21 48.67	7.18 0.3	2.78	0	5	10	3 2
910801	10 5358 15	38 13.61	22 6.39	1.22	50	2.59	0.16	03	0.4	10	910802	21 4125.64	38 23.21	22 9.61	9.29 0.5	2.39	010	3	04	5 3
910801	13 1226.25	38 33.95	21 54.19	17.61	1.0	2.64	0.0	0.3	0.8	11	910802	21 5714.18	38 14.74	22 5.53	5.61 0.5	2.32	0.13	03	0.2	8 8
010801	13 4610.04	38 14.98	22 4.29	7.76	0.5	2.33	0.13	0.3	0.3	12	910802	22 1722.32	38 14.65	22 6.59	7.44 0.7	2.49	0.14	0.5	04	6
108016	13 4645.20	38 14.87	22 3.97	8.33	0.6	2.54	0.1	0.3	0.3	13	910802	22 2513.36	38 15.36	22 5.45	8.61 1.0	2.20	0.16	0.4	0.5	68
910801	13 48 0.25	38 14.84	22 4.24	8.11	0.5	2.33	0.1	0.3	0.4	14	910802	22 2935.94	38 19.21	22 10.24	5.81 0.3	2.26	0.0	0.4	0.2	69
910801	13 4816.05	38 15.73	22 4.96	60.9	1:1	2.48	0.20	5 0.6	0.6	15	910802	23 29 4.44	38 15.55	22 5.40	9.00 0.5	2.83	0.16	0.2	0.2	20
910801	15 41 37.04	38 14.21	22 5.45	7.31	0.6	2.49	0.11	8 0.4	0.4	16	910802	23 33 5.85	38 15.45	22 5.30	8.33 0.8	2.35	0.14	0.4	0.3	11
910801	15 4534.15	38 22.23	22 0.74	8.03	0.6	2.12	0.1	1 0.5	0.4	17	910803	2 059.76	38 15.79	22 5.30	8.91 0.6	2.40	0.13	0.3	0.3	72
910801	15 52 1.90	38 18.34	22 8.30	8.03	0.5	2.48	0.1	2 0.5	0.8	18	910803	2 1449.37	38 24.38	21 57.68	9.23 0.5	2.45	0.10	0.2	0.2	73
910801	15 5922 99	38 14.72	22 5.03	6.11	0.9	2.09	0.1	5 0.5	0.5	19	910803	2 3534.77	38 14.25	22 4.86	7.31 0.8	2.38	0.17	0.4	0.5	74
910801	16 818.77	38 13.89	22 6.34	7.39	0.7	2.18	0.1	5 0.8	0.0	20	910803	3 2011.57	38 15.90	22 5.14	8.25 1.2	2.46	0.18	0.5	0.6	75
910801	16 1623.79	38 13.80	22 6.75	2.09	0.5	2.4	0.1	2 0.3	0.4	21	910803	4 25 2.84	38 21.15	21 44.38	8.99 0.4	2.86	0.0	0.3	0.1	78
910801	16 2155.67	38 14.55	22 5.36	6.48	0.3	2.45	0.1	3 0.2	0.2	22	910803	4 5838.55	38 14.13	22 7.37	6.18 0.5	2.47	0.15	0.3	0.2	79
108016	16 2231.80	38 14.64	22 5.60	6.98	0.3	2.42	0.1	5 0.3	0.3	23	910803	7 636.62	38 22.26	22 12.40	11.24 0.3	2.45	0.0	0.3	0.3	80
910801	16 53 0.12	38 14.56	22 5.80	5.77	0.6	2.36	0.1	3 0.4	0.3	24	910803	7 1344.71	38 18.17	21 48.52	8.28 0.7	2.51	0.10	0.6	0.3	81
108016	19 137.72	38 14.42	22 5.65	7.16	0.3	2.50	0.0	5 0.3	0.3	25	910803	8 325.60	38 15.01	22 4.84	8.14 0.5	2.41	0.10	0.3	0.3	82
108016	19 4915.54	38 17.19	22 2.57	8.50	1.6	2.41	0.1	7 0.6	0.6	27	910803	8 551.52	38 14.98	22 4.74	7.91 1.0	2.01	0.14	0.0	0.7	83
910801	20 624.16	38 14.74	22 4.24	8.10	0.5	2.33	0.1	3 0.3	0.3	28	910803	8 3121.36	38 14.25	22 7.24	6.73 0.4	2.37	0.15	0.7	0.5	8
108016	21 53 4.85	38 18.75	22 10.94	71.17	0.2	2.51	0.0	8 0.4	0.5	30	910803	8 5428.27	38 14.06	22 8.12	8.11 0.9	2.58	0.13	0.8	0.6	85
910801	21 5728.87	38 17.84	22 10.20	8.47	1.6	2.55	0.1	6 0.6	0.8	31	910803	9 458.56	38 13.90	22 7.52	7.34 0.3	2.78	0.15	0.2	0.2	86
910801	22 732.61	38 11.63	21 48.76	6.78	0.4	2.21	0.1	2 0.5	0.4	32	910803	10 056.76	38 19.31	22 6.18	9.64 0.5	2.42	0.0	0.2	0.3	87
108016	22 5956.04	38 18.77	22 4.25	8.70	0.6	2.68	8 0.1	2 0.2	0.2	33	910803	11 5149.59	38 14.02	22 7.36	6.82 0.3	2.47	0.13	0.3	0.2	88
910801	23 8 4.59	38 24.28	21 50.94	9.79	0.4	2.62	0.1	0.2	0.2	\$	910803	11 5332.80	38 22.20	22 11.78	9.19 0.2	2.24	0.0	0.2	0.2	68
910801	23 4460.00	38 13.75	22 6.43	7.64	0.3	2.77	0.1	4 0.2	0.2	35	910803	11 5634.55	38 22.27	22 11.65	9.10 0.2	2.21	0.0	0.2	0.2	8
910802	0 1724.67	38 20.74	21 46.57	9.07	0.5	2.93	9.1	5 0.3	0.2	36	910803	12 2457.48	38 17.55	21 56.12	7.96 0.4	2.23	0.13	0.4	0.3	91
910802	0 3640.40	38 24.03	21 47.94	60.6	0.6	2.93	9.2	0.5	0.4	37	910803	12 3454.06	38 25.04	22 12.26	13.81 0.2	2.46	0.0	0.2	0.2	92
910802	0 3640.48	38 23.99	21 48.10	9.29	0.8	2.86	S 0.0	5 0.4	0.2	38	910803	12 4716.16	38 18.14	21 47.74	7.92 0.5	2.26	0.0	0.6	0.4	93
910802	0 5235.45	38 14.33	22 5.65	7.54	0.4	2.43	3 0.1	3 0.2	0.2	39	910803	12 5720.68	38 23.76	22 3.33	10.17 0.4	2.37	0.0	0.2	0.4	<b>5</b>
910802	1 1128.11	38 24.12	21 48.17	8.24	0.3	2.47	0.0	8 0.3	0.2	4	910803	14 1023.49	38 14.35	21 58.28	6.76 0.3	2.57	0.11	0.2	0.2	95
910802	2 3918.92	38 22.64	22 12.09	9.61	0.2	2.39	0.1	0 0.2	0.2	41	910803	14 2333.03	38 18.47	22 9.70	4.05 0.5	2.02	0.0	0.5	0.2	96
910802	2 40 6.52	38 11.57	21 48.86	7.15	0.3	2.64	4 0.1	3 0.5	0.4	42	910803	16 1931.41	38 22.38	22 11.74	9.70 0.3	2.37	0.0	0.2	0.2	76
910802	4 4255.96	38 18.14	22 9.02	4.17	0.6	2.11	0.0	5 0.6	0.5	43	910803	18 1418.27	38 24.82	21 57.92	9.59 0.5	2.66	0.0	0.1	0.2	98
910802	5 710.42	38 21.60	22 11.47	8.95	0.4	243	2 0.1	3 0.4	0.2	4	910803	19 33 8.51	38 19.13	22 9.53	6.07 0.5	2.46	0.13	0.4	0.3	8
910802	7 1936.83	38 14.86	22 4.46	7.66	0.4	2.35	8 0.1	3 0.2	0.2	45	910803	19 749.47	38 18.89	21 49.73	7.72 1.4	2.37	0.23	0.8	0.5	10
910802	7 2444.15	38 20.56	22 4.30	9.80	0.9	2.63	0.2	0.3	0.3	46	910803	19 33 8.49	38 19.18	22 9.61	6.43 0.4	2.46	0.13	0.4	0.2	101
910802	9 21 8.71	38 25.34	21 56.21	9.84	0.2	2.91	0.1	0 0.1	0.1	47	910803	20 2149.26	38 22.08	21 49.62	7.07 0.2	2.30	0.0	0.2	0.1	102
910802	9 5651.16	38 25.46	21 55.84	8.86	0.3	2.52	0.0	5 0.1	0.7	48	910803	20 4447.74	38 14.10	22 5.60	7.72 0.3	2.73	0.13	0.2	0.2	103
910802	11 4324.26	38 11.87	21 48.69	6,46	0.5	2.70	0.1	20.6	0.4	49	910803	22 5 2.92	38 18.74	21 48.35	6.99 0.2	2.36	0.0	0.3	0.1	5

n.evt	25	174	175	176	178	179	180	101	3 28	185	186	8 6	161	193	194	261	198	61	200	30 I	3 2	204	207	208	211	213	214	216	217	218	220	ន	222	223	224	226	228	62		53	233 234
ERY	0.7	0 1 1 1 1 1	0.2	0.1	3 2	0.2	0.4	1.0	0.5	0.1	0.4	7 6	0.2	0.2	0.3	0.1	07	0.2	0.3	03	52	0.1	0.7	7.0	0.2	0.3	50	0.2	0.7	0.3	0.6	0.6	0.9	0.2	0.5	0.3	0.4	0.7	- ~ ~	62	0.2
ERX	0.7	50	0.2	0.1	0.7	0.2	0.3	7.0	0.4	0.2	0.4	7 0	0.3	0.3	0.2	0.1	0.1	0.2	0.3	0.4 6	10	0.3	0.6	0.5 0.5	0.2	0.3	7.0	0.1	1.1	0.3	0.7	60	0.5	0.4	0.7	0.2	0.6	0.4		02	0.3
RMS	0.13	0.12	0.15	0.10	0.11	0.08	0.0	100	0.12	0.10	0.08	7170	0.12	0.12	0.14	0.07	CI 70	0.13	0.15	0.08	0.11	0.09	0.13	0.14	0.0	0.13	0.14	0.08	0.25	0.14	0.23	0.15	0.09	0.14	0.07	0.10	0.05	80.0	51.0 11.0	0.10	0.05
Mag.	2.47	2.63	2.73	2.82	2.50	2.43	2.52	10.7 2 73	2.32	2.53	2.03	47 7 8 7 8	2.49	2.32	2.56	2.47	00.0	2.70	2.67	2.78 2.53	2.49	2.70	2.25	2.42	0.0	2.82	CC 7	2.19	0.0	2.40 2.40	2.45	0.0	2.03	2.36	2.14	2.74	2.28	8.8	0.00 2.46	2.38	2.14 2.03
ERZ	1.3	0.2	0.7	0.3	5.0	0.4	0.9	0.0	57	0.5	0.7	2 C	0.4	0.6	0.5	6.0 0	0.2	0.4	0.4	0.5	0.3	0.2	1.5	0.7	0.4	0.2	5.0	0.3	2.9	0.6	1.6	13	0.5	0.4	0.4	6.0	4.0	0.8	9.0	0.4	0.3
Depth	13.46	4.07 1090	8.75	9.43 e 7e	2.90	8.69	4.66	70'NI	4.71	8.32	66.1	C/ 0	8.03	7.69	8.10	8.31	e.e. 8.52	7.39	8.15	14.22 7 81	7.89	7.18	7.55	1.0.1	8.07	7.06	07.7 8	8.45	6.62	8.29	8.23 8.23	8.21	7.84	11.13	6.21	10.56	13.33	8.31	8.10	9.43	6.96 8.35
	~ 1	- 3	. 6	<b>7</b> ,	10	5	<u></u> .	4 6	. ~		æ (	2 2		0	80	<u>ج</u> م	8 22	0	5	6 <u>-</u>	. 10	÷.	c 5	6 X	yo,	2 '	0.50	ŝ	~		- 4	· 0	4	\$	<u>ت</u>	2	2 2	25	З ж	• 8	8 7
Long	22 5.4	22 4.7 21 48.6	22 5.3	21 54.5	27 6.8 27	21 57.6	21 49.1	8.4 77 20 4 3	27.12	22 6.8	22 7.0	4.C 22	22 5.2	22 4.9	22 5.0	22 1.0	21 56.7	22 7.5	22 4.8	22 4.1 22 50	1 2 2 4 9 4	21 49.4	22 5.0	21 4/	22 0.2	21 49.1	22 2.1	22 3.9	22 5.2	22 5.4	22 6.1	22 1.0	22 0.7	22 12.4	22 10.3	21 53.	22 16.1	21 25	22 1.5	21 58.0	22 11.8
	99	2 2	20	<u>ت</u> ۲	8 12	5	ლი 1	2 0	: 9	2	3	ž ž	: 3	5	2	88	2 8	12	12	52	5 25	2	£ 9	2 23	ន	ę :	2 C	: 65	<del>8</del>	6	<u>.</u>	8	8	<b>ç</b>	8	<u>ຕ</u> ່	5	5.	t 2	1 8	88
Lat	38 17.1	38 20.8 38 20.8	38 15.5	38 24.8	38 14.5	38 24.0	38 20.4	38 185	38 14.4	38 18.	38 18.5	38 14	38 15.6	38 15.8	38 15.7	38 22.0	38 24.	38 14.	38 14.	38 12.3	38 14.	38 20.	38 14.	38 23.	38 23.	38 11.	38 14.	38 21.	38 15.	38 15.	38 15	38 22.0	38 23.(	38 22.	38 18.	38 8.7	38 23.	38 24	38 15.1	38 24	38 20. 38 22.6
	7.47	56.0 66.0 66.0	5.95	96.1	<del>1</del> 43	8	8	2 %	3 6	.29	5	۲, ۵	1.62	4.02	8.86	5.50	007.2	8.96	5.00	0.63	12.06	1.26	6.47	3.31	11.10	4.15	10.07	8	5	3 2	9 9	33	.67	.10	8	8.39	0.79	2.0I	8.20	3.71	11.32 5.40
Time	20 155	21 473 21 57 6	22 41:	22 59 4	0 4646	0 52 5.	1 5710	1967.2	6 3940	7 3724	8 416.	10 0.6	10 15	11 313	11 413	12 101	13 272	14 165	15 27	15 27	15 284	15412	18 55	21 C 12	22 123	23 74	01000	0 2740	0 5241	1 628	1 4321	3 3943	4 48 5	7 2253	9 734	11 131	12 43	13 522 51	15 454	15 503	19 334 21 583
					- 10		<u>.</u>	~ ~		Ś	<u>,</u>	<u> </u>		<b>5</b>	\$	<b>~</b> ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	0 10		<u>s</u>	vo vo			<u>vo</u> v	0 10		vo 1	0 -	. ~	-	~ '		. ~	2	~	~	~	~ •	~ -		. ~	~ ~
Date	910805	910802	91080	910805	910806	910806	910806	9108019	910806	91080	91080	9108019	910800	08016	910800	91080	9108019	91080	91080	91080	91080	91080	91080	91080	91080	91080	91080	91080	91080	91080	91080	91080	91080	08016	91080	08016	91080	09010	9108016	91080	910807
n.evt	<u>10</u>	<u>8</u> 5	108	<u>60</u>	112	113	114	116	117	120	121	123	125	126	127	2 2	3 5	132	133	135	136	137	138	9	14]	142	5 4	145	<u>1</u>	147	149	152	153	2	155	<u>s</u> :		3 5	162	163	<u>3</u> 8
ERY n.evt	0.3 105	1.0	0.3 108	0.4 109 0.2 110	0.2 112	0.3 113	0.2 114	0.1 116	0.2 117	0.4 120	0.3 121	0.3 123	0.1 125	0.9 126	0.2 127	0.2 129	0.5 131	0.5 132	0.4 133	0.4 135	0.2 136	0.3 137	0.2 138	0.4 140	0.4 141	0.1 142	0.3 144	0.2 145	0.2 146	0.1 147	0.5 149	0.2 152	0.4 153	0.1 154	0.2 155	001 1.0	151 0.0 0.51 5.0		0.4 162	0.3 163	0.2 164 0.4 169
ERX ERY n.evt	0.3 0.3 105	0.8 1.0 107	0.7 0.3 108	0.4 0.4 109 0.2 0.2 110	0.3 0.2 112	0.3 0.3 113	0.2 0.2 114	0.2 0.1 116	0.1 0.2 117	0.3 0.4 120	0.2 0.3 121	0.2 0.3 123	0.1 0.1 125	1.0 0.9 126	0.2 0.2 127	0.2 0.2 129	0.9 0.5 131	0.5 0.5 132	0.4 0.4 133	0.3 0.4 135	0.2 0.2 136	0.3 0.3 137	0.2 0.2 138	0.3 0.4 140	0.4 0.4 141	0.1 0.1 142	0.3 0.3 144	0.2 0.2 145	0.2 0.2 146	0.1 0.1 147	0.6 0.5 149	0.2 0.2 152	0.4 0.4 153	0.2 0.1 154	0.1 0.2 155	0CI I.0 Z.0	1.51 0.0 8.0 0.31 5.0 5.0		0.4 0.4 162	0.2 0.3 163	0.2 0.2 164 0.2 0.4 169
RMS ERX ERY n.evt	0.09 0.3 0.3 105	0.22 0.8 1.0 107	0.17 0.7 0.3 108	0.12 0.4 0.4 109 0.06 0.2 0.2 110	0.11 0.3 0.2 112	0.09 0.3 0.3 113	0.04 0.2 0.2 114	0.08 0.2 0.1 116	0.09 0.1 0.2 117	0.09 0.3 0.4 120	0.12 0.2 0.3 121	0.08 0.2 0.3 123	0.10 0.1 0.1 125	0.12 1.0 0.9 126	0.11 0.2 0.2 127	0.08 0.2 0.2 129	0.23 0.9 0.5 131	0.12 0.5 0.5 132	0.16 0.4 0.4 133	0.11 0.3 0.4 135	0.11 0.2 0.2 136	0.09 0.3 0.3 137	0.11 0.2 0.2 138	0.17 0.3 0.4 140	0.15 0.4 0.4 141	0.10 0.1 0.1 142	0.10 0.3 0.3 144	0.13 0.2 0.2 145	0.12 0.2 0.2 146	0.03 0.1 0.1 147	0.22 0.6 0.5 149	0.05 0.2 0.2 152	0.07 0.4 0.4 153	0.08 0.2 0.1 154	0.09 0.1 0.2 155		1/21 0.0 8.0 9.0 0.04 0.2 0.4 140		0.10 0.4 0.4 162	0.12 0.2 0.3 163	0.12 0.2 0.2 164 0.11 0.2 0.4 169
Mag. RMS ERX ERY n.evt	2.40 0.09 0.3 0.3 105 2.67 0.11 0.1 0.1 106	2.31 0.22 0.8 1.0 107	2.51 0.17 0.7 0.3 108	2.42 0.12 0.4 0.4 109 2.58 0.06 0.2 0.2 110	2.44 0.11 0.3 0.2 112	2.35 0.09 0.3 0.3 113	2.16 0.04 0.2 0.2 114 2.34 0.07 0.7 0.1 115	2.60 0.08 0.2 0.1 116	2.66 0.09 0.1 0.2 117	2.10 0.09 0.3 0.4 120	2.21 0.12 0.2 0.3 121 2.11 0.08 0.5 0.5 123	2.58 0.08 0.2 0.3 123	2.73 0.10 0.1 0.1 125	2.47 0.12 1.0 0.9 126		2.38 0.08 0.2 0.2 129 2.37 0.14 0.4 0.4 130	2.38 0.23 0.9 0.5 131	2.38 0.12 0.5 0.5 132	243 0.16 0.4 0.4 133	2.37 0.11 0.3 0.4 135	2.61 0.11 0.2 0.2 136	2.58 0.09 0.3 0.3 137	2.49 0.11 0.2 0.2 138 7.60 0.13 0.4 0.7 130	2.38 0.17 0.3 0.4 140	2.34 0.15 0.4 0.4 141	2.63 0.10 0.1 0.1 142	2.28 0.10 0.3 0.3 144	2.54 0.13 0.2 0.2 145	2.55 0.12 0.2 0.2 146	2.04 0.03 0.1 0.1 147	2.35 0.22 0.6 0.5 149	2.23 0.05 0.2 0.2 152	2.30 0.07 0.4 0.4 153	2.94 0.08 0.2 0.1 154	2.49 0.09 0.1 0.2 155		2.19 U.19 U.8 U.6 13/ 2.00 0.05 0.3 0.5 150		2.23 0.10 0.4 0.4 162	2.51 0.12 0.2 0.3 163	2.90 0.12 0.2 0.2 164 2.31 0.11 0.2 0.4 169
LERZ Mag. RMS ERX ERY n.evt	0.6 2.40 0.09 0.3 0.3 105 0.3 2.67 0.11 0.1 0.6	1.4 2.31 0.22 0.8 1.0 107	0.7 2.51 0.17 0.7 0.3 108	0.4 2.42 0.12 0.4 0.4 109 0.6 2.58 0.06 0.2 0.2 110	0.6 2.44 0.11 0.3 0.2 112	0.4 2.35 0.09 0.3 0.3 113	0.3 2.16 0.04 0.2 0.2 114 0.1 2.34 0.07 0.2 0.1 115	0.3 2.60 0.08 0.2 0.1 116	0.3 2.66 0.09 0.1 0.2 117	0.6 2.10 0.09 0.3 0.4 120	0.5 2.21 0.12 0.2 0.3 121 0.5 2.11 0.08 0.5 0.5 122	0.3 2.58 0.08 0.2 0.3 123	0.3 2.73 0.10 0.1 0.1 125	1.0 2.47 0.12 1.0 0.9 126	0.4 2.42 0.11 0.2 0.2 127	0.3 2.38 0.08 0.2 0.2 129 12 2.37 0.14 0.4 0.4 130	1.5 2.38 0.23 0.9 0.5 131	0.7 2.38 0.12 0.5 0.5 132	0.5 243 0.16 0.4 0.4 133	2.3 2.03 0.20 0.6 1.4 134 0.5 2.37 0.11 0.3 0.4 135	0.4 2.61 0.11 0.2 0.2 136	0.5 2.58 0.09 0.3 0.3 137	0.4 2.49 0.11 0.2 0.2 138 0.6 7.60 0.13 0.4 0.2 130	0.3 2.38 0.17 0.3 0.4 140	0.7 2.34 0.15 0.4 0.4 141	0.3 2.63 0.10 0.1 0.1 142	0.3 2.28 0.10 0.3 0.3 144	0.3 2.54 0.13 0.2 0.2 145	0.3 2.55 0.12 0.2 0.2 146	0.2 2.04 0.03 0.1 0.1 147 03 735 0.07 0.2 0.2 148	0.6 2.35 0.22 0.6 0.5 149	0.2 2.23 0.05 0.2 0.2 152	0.4 2.30 0.07 0.4 0.4 153	0.3 2.94 0.08 0.2 0.1 154	0.4 2.49 0.09 0.1 0.2 155		2.3 2.19 U.19 U.8 U.0 13/ 0.5 2.00 0.05 0.3 0.5 160		0.5 2.23 0.10 0.4 0.4 162	0.5 2.51 0.12 0.2 0.3 163	0.6 2.90 0.12 0.2 0.2 164 0.6 2.31 0.11 0.2 0.4 169
Depth ERZ Mag. RMS ERX ERY n.evt	10.33 0.6 2.40 0.09 0.3 0.3 105 0.00 0.3 2.67 0.11 0.1 0.1 106	8.77 1.4 2.31 0.22 0.8 1.0 107	6.14 0.7 2.51 0.17 0.7 0.3 108	7.00 0.4 2.42 0.12 0.4 0.4 109 9.47 0.6 2.58 0.06 0.2 0.2 110	9.43 0.6 2.44 0.11 0.3 0.2 112	9.69 0.4 2.35 0.09 0.3 0.3 113	8.25 0.3 2.16 0.04 0.2 0.2 114 8.57 0.1 2.34 0.07 0.7 0.1 115	7.71 0.3 2.60 0.08 0.2 0.1 116	10.51 0.3 2.66 0.09 0.1 0.2 117	8.16 0.6 2.10 0.09 0.3 0.4 120	6.81 0.5 2.21 0.12 0.2 0.3 121 5 25 0 5 2.11 0.08 0 5 0 5 122	17.88 0.3 2.58 0.08 0.2 0.3 123	9.90 0.3 2.73 0.10 0.1 0.1 125	19.56 1.0 2.47 0.12 1.0 0.9 126	7.29 0.4 2.42 0.11 0.2 0.2 127	10./8 0.3 2.38 0.08 0.2 0.2 129 673 17 277 014 04 04 130	7.27 1.5 2.38 0.23 0.9 0.5 131	7.56 0.7 2.38 0.12 0.5 0.5 132	7.42 0.5 243 0.16 0.4 0.4 133	0.89 2.3 2.03 0.20 0.6 1.4 1.34 5.65 0.5 2.37 0.11 0.3 0.4 135	5.51 0.4 2.61 0.11 0.2 0.2 136	6.54 0.5 2.58 0.09 0.3 0.3 137	7.86 0.4 2.49 0.11 0.2 0.2 138 0.25 0.6 2.60 0.13 0.4 0.2 130	7.18 0.3 2.38 0.17 0.3 0.4 140	7.91 0.7 2.34 0.15 0.4 0.4 141	10.00 0.3 2.63 0.10 0.1 0.1 142 711 0.5 2.22 0.14 0.2 0.5 142	6.72 0.3 2.28 0.10 0.3 0.3 144	6.78 0.3 2.54 0.13 0.2 0.2 145	7.50 0.3 2.55 0.12 0.2 0.2 146	4.75 0.2 2.04 0.03 0.1 0.1 147 0.14 0.3 2.25 0.07 0.2 0.2 148		6.55 0.2 2.23 0.05 0.2 0.2 152	10.52 0.4 2.30 0.07 0.4 0.4 153	9.31 0.3 2.94 0.08 0.2 0.1 154	9.28 0.4 2.49 0.09 0.1 0.2 155	0CI I'O 7.0 0.10 7.15 0.10 0.2 0.1 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	0.00 2.3 2.19 0.19 0.8 0.0 13/ 8.60 0.6 3.00 0.06 0.3 0.6 160	8.49 0.4 7.53 0.05 0.7 0.7 161	5.63 0.5 2.23 0.10 0.4 0.4 162	7.84 0.5 2.51 0.12 0.2 0.3 163	8.38 0.6 2.90 0.12 0.2 0.2 164 7.77 0.6 2.31 0.11 0.2 0.4 169
Depth ERZ Mag. RMS ERX ERY n.cvt	36 10.33 0.6 2.40 0.09 0.3 0.3 105 38 0.20 0.3 2.67 0.11 0.1 0.1 106	94 8.77 1.4 2.31 0.22 0.8 1.0 107	<b>63 6.14 0.7 2.51 0.17 0.7 0.3 108</b>	.45 7.00 0.4 2.42 0.12 0.4 0.4 109 76 9.47 0.6 2.58 0.06 0.2 0.2 110	44 9.43 0.6 2.44 0.11 0.3 0.2 112	.90 9.69 0.4 2.35 0.09 0.3 0.3 113	05 8.25 0.3 2.16 0.04 0.2 0.2 114 47 8.57 0.1 2.34 0.07 0.2 0.1 115	.63 7.71 0.3 2.60 0.08 0.2 0.1 116	52 10.51 0.3 2.66 0.09 0.1 0.2 117	.00 8.16 0.6 2.10 0.09 0.3 0.4 120	56 6.81 0.5 2.21 0.12 0.2 0.3 121 46 6.36 0.6 3.11 0.08 0.6 0.6 133	87 17.88 0.3 2.58 0.08 0.2 0.3 123	.69 9.90 0.3 2.73 0.10 0.1 0.1 125	.43 19.56 1.0 2.47 0.12 1.0 0.9 126	58 7.29 0.4 2.42 0.11 0.2 0.2 127	.31 10./8 0.3 2.38 0.08 0.2 0.2 129 13 6.73 1.3 2.77 0.14 0.4 0.4 130	.09 7.27 1.5 2.38 0.23 0.9 0.5 131	82 7.56 0.7 2.38 0.12 0.5 0.5 132	90 7.42 0.5 2.43 0.16 0.4 0.4 133	.19 0.69 2.3 2.03 0.20 0.0 1.4 1.34 71 5.65 0.5 2.37 0.11 0.3 0.4 135	.98 5.51 0.4 2.61 0.11 0.2 0.2 136	.47 6.54 0.5 2.58 0.09 0.3 0.3 137	20 7.86 0.4 2.49 0.11 0.2 0.2 138 00 0.75 0.5 7.50 0.13 0.4 0.2 130	94 7.18 0.3 2.38 0.17 0.3 0.4 140	31 7.91 0.7 2.34 0.15 0.4 0.4 141	.47 10.00 0.3 2.63 0.10 0.1 0.1 142	44 6.72 0.3 2.28 0.10 0.3 0.3 144	42 6.78 0.3 2.54 0.13 0.2 0.2 145	50 7.50 0.3 2.55 0.12 0.2 0.2 146	62 4.75 0.2 2.04 0.03 0.1 0.1 147 53 0.14 0.3 2.25 0.07 0.2 0.2 148	.16 6.20 0.6 2.35 0.22 0.6 0.5 149	19 6.55 0.2 2.23 0.05 0.2 0.2 152	76 10.52 0.4 2.30 0.07 0.4 0.4 153	.01 9.31 0.3 2.94 0.08 0.2 0.1 154	.57 9.28 0.4 2.49 0.09 0.1 0.2 155	0C1 1.0 7.0 01.0 7.1 5.1 0.2 0.1 0.2 0.1 0.2 0.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	09 0.00 2.3 2.19 0.19 0.8 0.0 13/ 76 8.60 0.6 2.00 0.06 0.3 0.6 160	01 570 570 770 770 770 100 100 100 100 100 100 1	71 5.63 0.5 2.23 0.10 0.4 0.4 162	88 7.84 0.5 2.51 0.12 0.2 0.3 163	89 8.38 0.6 2.90 0.12 0.2 0.2 164 66 7.77 0.6 2.31 0.11 0.2 0.4 169
Long Depth ERZ Mag. RMS ERX ERY n.evt	22 6.36 10.33 0.6 2.40 0.09 0.3 0.3 105 22 0.28 0.20 0.3 2.67 0.11 0.1 0.1 106	22 5.94 8.77 1.4 2.31 0.22 0.8 1.0 107	22 9.63 6.14 0.7 2.51 0.17 0.7 0.3 108	21 48.45 7.00 0.4 2.42 0.12 0.4 0.4 109 22 1.76 9.47 0.6 2.58 0.06 0.2 0.2 110	22 9.44 9.43 0.6 2.44 0.11 0.3 0.2 112	22 11.90 9.69 0.4 2.35 0.09 0.3 0.3 113	22 2.05 8.25 0.3 2.16 0.04 0.2 0.2 114 21 44 47 8 57 0 1 2 34 0 00 0 7 0 1 115	21 47,63 7.71 0.3 2.60 0.08 0.2 0.1 116	21 54.52 10.51 0.3 2.66 0.09 0.1 0.2 117	21 51.00 8.16 0.6 2.10 0.09 0.3 0.4 120	22 4.56 6.81 0.5 2.21 0.12 0.2 0.3 121 22 8.46 5.26 0.5 2.11 0.06 0.5 0.5 122	21 53.87 17.88 0.3 2.58 0.08 0.2 0.3 123	21 57.69 9.90 0.3 2.73 0.10 0.1 0.1 125	21 43.43 19.56 1.0 2.47 0.12 1.0 0.9 126	22 3.58 7.29 0.4 2.42 0.11 0.2 0.2 127	2149.31 10.78 0.3 2.38 0.08 0.2 0.2 129 215312 573 12 227 014 04 04 130	21 49:09 7.27 1.5 2.38 0.23 0.9 0.5 131	22 6.82 7.56 0.7 2.38 0.12 0.5 0.5 132	22 4.90 7.42 0.5 243 0.16 0.4 0.4 133	21 2/1 2/1 2/28 2.3 2.03 0.20 0.0 1.4 134 22 9.71 5.65 0.5 2.37 0.11 0.3 0.4 135	21 57.98 5.51 0.4 2.61 0.11 0.2 0.2 136	21 49.47 6.54 0.5 2.58 0.09 0.3 0.3 137	22 7.20 7.86 0.4 2.49 0.11 0.2 0.2 138 21 45 00 0.25 0.6 2.60 0.13 0.4 0.2 130	22 5.94 7.18 0.3 2.38 0.17 0.3 0.4 140	22 7.31 7.91 0.7 2.34 0.15 0.4 0.4 141	21 55.47 10.00 0.3 2.63 0.10 0.1 0.1 142	22 9.44 6.72 0.3 2.28 0.10 0.3 0.3 144	22 9.42 6.78 0.3 2.54 0.13 0.2 0.2 145	22 7.50 7.50 0.3 2.55 0.12 0.2 0.2 146	22 9.62 4.75 0.2 2.04 0.03 0.1 0.1 147 22 8.53 0.14 0.3 2.25 0.07 0.2 0.2 148	22 11.16 6.20 0.6 2.35 0.22 0.6 0.5 149	22 9.19 6.55 0.2 2.23 0.05 0.2 0.2 152	22 14.76 10.52 0.4 2.30 0.07 0.4 0.4 153	21 48.01 9.31 0.3 2.94 0.08 0.2 0.1 154	21 56.57 9.28 0.4 2.49 0.09 0.1 0.2 155	0C1 1.0 7.0 0.10 7.15 0.10 0.27 0.10 0.2 0.1 10 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.	70 20 20 20 20 20 20 20 20 20 20 20 20 20	101 CO CO 000 007 000 000 070 070 070 070 070 07	22 9.71 5.63 0.5 2.23 0.10 0.4 0.4 162	22 4.88 7.84 0.5 2.51 0.12 0.2 0.3 163	22 4.89 8.38 0.6 2.90 0.12 0.2 164 22 4.66 7.77 0.6 2.31 0.11 0.2 0.4 169
Long Depth ERZ Mag. RMS ERX ERY n.evt	161 22 6.36 10.33 0.6 2.40 0.09 0.3 0.3 105 72 72 0.2 0.2 0.2 0.2 7 0.1 0.1 0.1 0.6		.14 22 9.63 6.14 0.7 2.51 0.17 0.7 0.3 108	.30 2148.45 7.00 0.4 2.42 0.12 0.4 0.4 109 1.72 22 1.76 9.47 0.6 2.58 0.06 0.2 0.2 110	<b>159 22 9.44 9.43 0.6 2.44 0.11 0.3 0.2 112</b>	.47 22 11.90 9.69 0.4 2.35 0.09 0.3 0.3 113	.96 22 2.05 8.25 0.3 2.16 0.04 0.2 0.2 114 86 21 44 47 8 57 0 1 2 34 0 07 0 2 0 1 115	.43 21 47.63 7.71 0.3 2.60 0.08 0.2 0.1 116	24 21 54.52 10.51 0.3 2.66 0.09 0.1 0.2 117	20 21 51.00 8.16 0.6 2.10 0.09 0.3 0.4 120		21 22 649 J.J. 00 00 211 000 02 03 122 122 129 21 53.87 17.88 0.3 2.58 0.08 0.2 0.3 123	.72 21 57.69 9.90 0.3 2.73 0.10 0.1 0.1 125	.47 21 43.43 19.56 1.0 2.47 0.12 1.0 0.9 126	.62 22 3.58 7.29 0.4 2.42 0.11 0.2 0.2 127	29 21 49.31 10.78 0.3 2.38 0.08 0.2 0.2 129 27 21 53 12 673 12 227 014 04 04 130	.76 21 49.09 7.27 1.5 2.38 0.23 0.9 0.5 131	.17 22 6.82 7.56 0.7 2.38 0.12 0.5 0.5 132	28 22 4.90 7.42 0.5 2 43 0.16 0.4 0.4 133	4/ 21 2/.19 0.89 2.3 2.00 0.20 0.0 1.4 134 02 22 9.71 5.65 0.5 2.37 0.11 0.3 0.4 135	44 21 57.98 5.51 0.4 2.61 0.11 0.2 0.2 136	00 21 49.47 6.54 0.5 2.58 0.09 0.3 0.3 137	.43 22.7.20 7.86 0.4 2.49 0.11 0.2 0.2 138 26 21.45.00 0.25 0.5 2.60 0.13 0.4 0.2 130	. 26 22 5.94 7.18 0.3 2.38 0.17 0.3 0.4 140	81 22 7.31 7.91 0.7 2.34 0.15 0.4 0.4 141	.97 21 55.47 10.00 0.3 2.63 0.10 0.1 0.1 142	45 22 9.44 6.72 0.3 2.28 0.10 0.3 0.3 14	.71 22 9.42 6.78 0.3 2.54 0.13 0.2 0.2 145	.07 22 7.50 7.50 0.3 2.55 0.12 0.2 0.2 146	.69 22 9.62 4.75 0.2 2.04 0.03 0.1 0.1 147 13 22 8.53 0.14 0.3 2.25 0.07 0.3 0.2 148	.25 22 11.16 6.20 0.6 2.35 0.22 0.6 0.5 149	28 22 9.19 6.55 0.2 2.23 0.05 0.2 0.2 152	.62 22 14.76 10.52 0.4 2.30 0.07 0.4 0.4 153	34 21 48.01 9.31 0.3 2.94 0.08 0.2 0.1 154	.76 21 56.57 9.28 0.4 2.49 0.09 0.1 0.2 155	0<1 1.0 7.7 0.12 0.40 0.57 0.4 0.10 0.7 0.1 0.2 0.1 1.2 0.1 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	.14 22 3.09 0.00 2.3 2.19 0.19 0.8 0.0 13/ 06 22 0.76 8.60 0.6 2.00 0.06 0.3 0.6 160	001 C70 C70 0070 0077 070 0079 077 77 007 43 215461 840 04 254 0000 077 02	<i>57</i> 22 9.71 5.63 0.5 2.23 0.10 0.4 0.4 162	41 22 4.88 7.84 0.5 2.51 0.12 0.2 0.3 163	.21 22 4.89 8.38 0.6 2.90 0.12 0.2 0.2 164 .39 22 4.66 7.77 0.6 2.31 0.11 0.2 0.4 169
Lat Long Depth ERZ Mag. RMS ERX ERY n.evt	38 16.61 22 6.36 10.33 0.6 2.40 0.09 0.3 0.3 105 38 32 37 32 32 37 31 0.5	38 14.41 22 5.94 8.77 1.4 2.31 0.22 0.8 1.0 107	38 18.14 22 9.63 6.14 0.7 2.51 0.17 0.7 0.3 108	38 11.30 21 48.45 7.00 0.4 2.42 0.12 0.4 0.4 109 38 2072 22 1.76 9.47 0.6 2.58 0.06 0.2 0.2 110	38 19.59 22 9.44 9.43 0.6 2.44 0.11 0.3 0.2 112	38 22.47 22 11.90 9.69 0.4 2.35 0.09 0.3 0.3 113	38 21.96 22 2.05 8.25 0.3 2.16 0.04 0.2 0.2 114 38 21 86 21 44 47 8 57 0 1 2 34 0 107 0 2 0 1 115	38 18.43 21 47.63 7.71 0.3 2.60 0.08 0.2 0.1 116	38 27.24 21 54.52 10.51 0.3 2.66 0.09 0.1 0.2 117	38 25.20 21 51.00 8.16 0.6 2.10 0.09 0.3 0.4 120	38 14.59 22 4.56 6.81 0.5 2.21 0.12 0.2 0.3 121 38 19 27 22 8.45 6.24 0.4 2.11 0.08 0.5 0.5 122	38 18.27 22 6.43 2.29 0.0 2.1 0.08 0.2 0.3 122 38 33.19 21 53.87 17.88 0.3 2.58 0.08 0.2 0.3 123	38 24.72 21 57.69 9.90 0.3 2.73 0.10 0.1 0.1 125	38 30.47 21 43.43 19.56 1.0 2.47 0.12 1.0 0.9 126	38 15.62 22 3.58 7.29 0.4 2.42 0.11 0.2 0.2 127	38 2/.59 21 49.51 10.78 0.3 2.38 0.08 0.2 0.2 129 38 27 27 21 54 12 673 12 227 014 04 04 130	38 20.76 21 49.09 7.27 1.5 2.38 0.23 0.9 0.5 131	38 14.17 22 6.82 7.56 0.7 2.38 0.12 0.5 0.5 132	38 14.28 22 4.90 7.42 0.5 2 43 0.16 0.4 0.4 133	38 0.4/ 21 37.19 0.89 2.3 2.05 0.20 0.0 1.4 134 38 19.02 22 9.71 5.65 0.5 2.37 0.11 0.3 0.4 135	38 16.44 21 57.98 5.51 0.4 2.61 0.11 0.2 0.2 136	38 20.00 21 49.47 6.54 0.5 2.58 0.09 0.3 0.3 137	38 14.43 22 7.20 7.86 0.4 2.49 0.11 0.2 0.2 138 38 21 28 21 45 00 0.25 0.5 2.60 0.13 0.4 0.2 130	38 13.96 22 5.94 7.18 0.3 2.38 0.17 0.3 0.4 140	38 13.81 22 7.31 7.91 0.7 2.34 0.15 0.4 0.4 141	38 25.97 21 55.47 10.00 0.3 2.63 0.10 0.1 0.1 142	38 20.45 22 9.44 6.72 0.3 2.28 0.10 0.3 0.3 144	38 20.71 22 9.42 6.78 0.3 2.54 0.13 0.2 0.2 145	38 14.07 22 7.50 7.50 0.3 2.55 0.12 0.2 0.2 146	38 20.69 22 9.62 4.75 0.2 2.04 0.03 0.1 0.1 147 38 21 12 22 8 53 0.14 0.3 225 0.07 0.2 148	38 18.25 22 11.16 6.20 0.6 2.35 0.22 0.6 0.5 149	38 20.28 22 9.19 6.55 0.2 2.23 0.05 0.2 0.2 152	38 19.62 22 14.76 10.52 0.4 2.30 0.07 0.4 0.4 153	38 24.34 21 48.01 9.31 0.3 2.94 0.08 0.2 0.1 154	38 24.76 21 56.57 9.28 0.4 2.49 0.09 0.1 0.2 155		38 19.14 22 3.09 0.00 2.3 2.19 0.19 0.8 0.0 13/ 38 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	001 570 57 00 000 77 000 000 77 00 000 000	38 18.57 22 9.71 5.63 0.5 2.23 0.10 0.4 0.4 162	38 14.41 22 4.88 7.84 0.5 2.51 0.12 0.2 0.3 163	3814.21 22 4.89 8.38 0.6 2.90 0.12 0.2 0.2 164 3814.39 22 4.66 7.77 0.6 2.31 0.11 0.2 0.4 169
Lat Long Depth ERZ Mag. RMS ERX ERY n.evt	147.65 38 16.61 22 6.36 10.33 0.6 2.40 0.09 0.3 0.3 105	16.24 38 14.41 22 5.94 8.77 1.4 2.31 0.22 0.8 1.0 107	<b>25.11 38 18.14 22 9.63 6.14 0.7 2.51 0.17 0.7 0.3 108</b>	9.15 3811.30 2148.45 7.00 0.4 2.42 0.12 0.4 0.4 109 13.44 38.20.72 22.1.76 9.47 0.6 2.58 0.06 0.2 0.2 110	22.04 38 19.59 22 9.44 9.43 0.6 2.44 0.11 0.3 0.2 112	13.92 38.22.47 22.11.90 9.69 0.4 2.35 0.09 0.3 0.3 113	[3.17 38.21.96 22 2.05 8.25 0.3 2.16 0.04 0.2 0.2 114 11 77 38 21 86 21 44 47 8 57 0.1 2 34 0.07 0.2 0.1 115	0.36 38 18.43 21 47.63 7.71 0.3 2.60 0.08 0.2 0.1 116	11.25 38 27.24 21 54.52 10.51 0.3 2.66 0.09 0.1 0.2 117	45.82 38 25.20 21 51.00 8.16 0.6 2.10 0.09 0.3 0.4 120	119.88 38 14.59 22 4.56 6.81 0.5 2.21 0.12 0.2 0.3 121 21 55 25 19 27 22 8.45 5 25 0 5 2 11 0.09 0 5 0 5 122	53.81 38 33.19 21 53.87 17.88 0.3 2.58 0.08 0.2 0.3 123	.3.98 38 24.72 21 57.69 9.90 0.3 2.73 0.10 0.1 0.1 125	0.44 38 30.47 21 43.43 19.56 1.0 2.47 0.12 1.0 0.9 126	142.97 38 15.62 22 3.58 7.29 0.4 2.42 0.11 0.2 0.2 127	24.19 38.27.29 21.49.31 10.78 0.3 2.38 0.08 0.2 0.2 129 30.80 38.27.77 71.51.7 5.73 1.7 7.77 0.14 0.4 0.4 130	37.49 38 20.76 21 49.09 7.27 1.5 2.38 0.23 0.9 0.5 131	25.47 38 14.17 22 6.82 7.56 0.7 2.38 0.12 0.5 0.5 132	19.35 38 14.28 22 4.90 7.42 0.5 243 0.16 0.4 0.4 133   0.000 <td< td=""><td>39./3 38 0.4/ 21 3/.19 0.59 2.3 2.00 0.20 0.0 1.4 1.34 48.97 38 19.02 22 9.71 5.65 0.5 2.37 0.11 0.3 0.4 135</td><td>53.89 38 16.44 21 57.98 5.51 0.4 2.61 0.11 0.2 0.2 136</td><td>9.19 38 20.00 21 49.47 6.54 0.5 2.58 0.09 0.3 0.3 137</td><td>4.59 38 14.43 22 7.20 7.86 0.4 2.49 0.11 0.2 0.2 138 324 28 21 28 21 45 00 0.25 0.5 7.50 0.13 0.4 0.2 130</td><td>7.11 38 13.96 22 5.94 7.18 0.3 2.38 0.17 0.3 0.4 140</td><td>2.85 38 13.81 22 7.31 7.91 0.7 2.34 0.15 0.4 0.4 141</td><td>4.52 38 25.97 21 55.47 10.00 0.3 2.63 0.10 0.1 0.1 142</td><td>241 38 20 47 22 9.44 6.72 0.3 2.28 0.10 0.3 0.3 14 247 38 20,45 22 9,44 6.72 0.3 2.28 0.10 0.3 0.3 14</td><td>0.11 38 20.71 22 9.42 6.78 0.3 2.54 0.13 0.2 0.2 145</td><td>1.78 38 14.07 22 7.50 7.50 0.3 2.55 0.12 0.2 0.2 146</td><td>2.81 38 20.69 22 9.62 4.75 0.2 2.04 0.03 0.1 0.1 147 8.26 38.31 12 22 8.53 0.14 0.3 7.25 0.07 0.2 0.2 148</td><td>3.96 38 18.25 22 11.16 6.20 0.6 2.35 0.22 0.6 0.5 149</td><td>45.48 38 20.28 22 9.19 6.55 0.2 2.23 0.05 0.2 0.2 152</td><td>2.98 38 19.62 22 14.76 10.52 0.4 2.30 0.07 0.4 0.4 153</td><td>35.11 38 24.34 21 48.01 9.31 0.3 2.94 0.08 0.2 0.1 154</td><td>57.17 38 24.76 21 56.57 9.28 0.4 2.49 0.09 0.1 0.2 155</td><td></td><td>8.4/ 38 19.14 22 3.09 0.00 2.3 2.19 0.19 0.8 0.0 13/ 13.61 38 27 0.6 27 0.7 76 8.60 0.6 7.00 0.76 0.3 0.5 160</td><td>001 570 570 007 007 007 000 007 127 0020 001 120 007 38 26 00 07 12 120 000 007 18 12 12 12 12 12 12 12 12 12 12</td><td>7.23 38 18.57 22 9.71 5.63 0.5 2.23 0.10 0.4 0.4 162</td><td>19.25 38 14.41 22 4.88 7.84 0.5 2.51 0.12 0.2 0.3 163</td><td>21.84 38 14.21 22 4.89 8.38 0.6 2.90 0.12 0.2 0.2 164 44.23 38 14.39 22 4.66 7.77 0.6 2.31 0.11 0.2 0.4 169</td></td<>	39./3 38 0.4/ 21 3/.19 0.59 2.3 2.00 0.20 0.0 1.4 1.34 48.97 38 19.02 22 9.71 5.65 0.5 2.37 0.11 0.3 0.4 135	53.89 38 16.44 21 57.98 5.51 0.4 2.61 0.11 0.2 0.2 136	9.19 38 20.00 21 49.47 6.54 0.5 2.58 0.09 0.3 0.3 137	4.59 38 14.43 22 7.20 7.86 0.4 2.49 0.11 0.2 0.2 138 324 28 21 28 21 45 00 0.25 0.5 7.50 0.13 0.4 0.2 130	7.11 38 13.96 22 5.94 7.18 0.3 2.38 0.17 0.3 0.4 140	2.85 38 13.81 22 7.31 7.91 0.7 2.34 0.15 0.4 0.4 141	4.52 38 25.97 21 55.47 10.00 0.3 2.63 0.10 0.1 0.1 142	241 38 20 47 22 9.44 6.72 0.3 2.28 0.10 0.3 0.3 14 247 38 20,45 22 9,44 6.72 0.3 2.28 0.10 0.3 0.3 14	0.11 38 20.71 22 9.42 6.78 0.3 2.54 0.13 0.2 0.2 145	1.78 38 14.07 22 7.50 7.50 0.3 2.55 0.12 0.2 0.2 146	2.81 38 20.69 22 9.62 4.75 0.2 2.04 0.03 0.1 0.1 147 8.26 38.31 12 22 8.53 0.14 0.3 7.25 0.07 0.2 0.2 148	3.96 38 18.25 22 11.16 6.20 0.6 2.35 0.22 0.6 0.5 149	45.48 38 20.28 22 9.19 6.55 0.2 2.23 0.05 0.2 0.2 152	2.98 38 19.62 22 14.76 10.52 0.4 2.30 0.07 0.4 0.4 153	35.11 38 24.34 21 48.01 9.31 0.3 2.94 0.08 0.2 0.1 154	57.17 38 24.76 21 56.57 9.28 0.4 2.49 0.09 0.1 0.2 155		8.4/ 38 19.14 22 3.09 0.00 2.3 2.19 0.19 0.8 0.0 13/ 13.61 38 27 0.6 27 0.7 76 8.60 0.6 7.00 0.76 0.3 0.5 160	001 570 570 007 007 007 000 007 127 0020 001 120 007 38 26 00 07 12 120 000 007 18 12 12 12 12 12 12 12 12 12 12	7.23 38 18.57 22 9.71 5.63 0.5 2.23 0.10 0.4 0.4 162	19.25 38 14.41 22 4.88 7.84 0.5 2.51 0.12 0.2 0.3 163	21.84 38 14.21 22 4.89 8.38 0.6 2.90 0.12 0.2 0.2 164 44.23 38 14.39 22 4.66 7.77 0.6 2.31 0.11 0.2 0.4 169
Time Lat Long Depth ERZ Mag. RMS ERX ERY n.ew	23 1747.65 38 16.61 22 6.36 10.33 0.6 2.40 0.09 0.3 0.3 105 23 1917 09 29 27 27 27 27 21 20	23 3916.24 38 14.41 22 5.94 8.77 1.4 2.31 0.22 0.8 1.0 107	23 4025.11 38 18.14 22 9.63 6.14 0.7 2.51 0.17 0.7 0.3 108	0579.15 38 11.30 21 48.45 7.00 0.4 2.42 0.12 0.4 0.4 109 1 4713.44 38 20.72 22 1.76 9.47 0.6 2.58 0.06 0.2 0.2 110	2 3222.04 38 19.59 22 9.44 9.43 0.6 2.44 0.11 0.3 0.2 112	3 1333.92 38 22.47 22 11.90 9.69 0.4 2.35 0.09 0.3 0.3 113	33613.17 3821.96 222.05 8.25 0.3 2.16 0.04 0.2 0.2 114 3562177 3821.86 2144.47 857 0.1 234 002 0.2 0.1 115	8 4326.36 38 18.43 21 47.63 7.71 0.3 2.60 0.08 0.2 0.1 116	9 5721.25 38 27.24 21 54.52 10.51 0.3 2.66 0.09 0.1 0.2 117	11 1345.82 38 25.20 21 51.00 8.16 0.6 2.10 0.09 0.3 0.4 120	112319.88 3814.59 224.56 6.81 0.5 2.21 0.12 0.2 0.3 121	12 122100 36 16.37 22 6.49 3.50 0.0 2.11 0.06 0.2 0.3 122 14 053.81 38 33.19 21 53.87 17.88 0.3 2.58 0.08 0.2 0.3 123	16 17 3.98 38 24.72 21 57.69 9.90 0.3 2.73 0.10 0.1 0.1 125	16 38 0.44 38 30.47 21 43.43 19.56 1.0 2.47 0.12 1.0 0.9 126	17 1542.97 38 15.62 22 3.58 7.29 0.4 2.42 0.11 0.2 0.2 127	18 5254.19 38 27.59 21 49.51 10.78 0.5 2.58 0.08 0.2 0.2 129 10 3030 80 38 27 77 71 51 57 57 17 77 71 6 0.4 0.4 130	20 1637.49 38 20.76 21 49.09 7.27 1.5 2.38 0.23 0.9 0.5 131	20 3925.47 38 14.17 22 6.82 7.56 0.7 2.38 0.12 0.5 0.5 132	20 5419.35 38 14.28 22 4.90 7.42 0.5 2 43 0.16 0.4 0.4 133	214139.13 38 0.47 21 31.19 0.89 2.5 2.05 0.20 0.0 1.4 134 22 5748.97 38 19.02 22 9.71 5.65 0.5 2.37 0.11 0.3 0.4 135	23 2253 89 38 16.44 21 57.98 5.51 0.4 2.61 0.11 0.2 0.2 136	0 219.19 38 20.00 21 49.47 6.54 0.5 2.58 0.09 0.3 0.3 137	0 2534.59 38 14.43 22 7.20 7.86 0.4 2.49 0.11 0.2 0.2 138 0 26 24 28 71 28 71 28 71 45 00 0 25 0 6 7 50 0 13 0 4 0 2 130	05127.11 38 13.96 22 5.94 7.18 0.3 2.38 0.17 0.3 0.4 140	2 852.85 38 13.81 22 7.31 7.91 0.7 2.34 0.15 0.4 0.4 141	2 4654.52 38 25.97 21 55.47 10.00 0.3 2.63 0.10 0.1 0.1 142 3 10100 2014 10 21 52.0 711 0.5 2.42 0.14 0.3 0.5 142	3 123247 38 14.18 22 9.44 6.72 0.3 2.28 0.10 0.3 0.3 144	3 20 0.11 38 20.71 22 9.42 6.78 0.3 2.54 0.13 0.2 0.2 145	3511.78 3814.07 22 7.50 7.50 0.3 2.55 0.12 0.2 0.2 146	4 1512.81 38 20.69 22 9.62 4.75 0.2 2.04 0.03 0.1 0.1 147 5 7738 75 38 31 17 22 8 53 0 14 0 3 7 25 0 27 0 2 148	5 4753.96 38 18.25 22 11.16 6.20 0.6 2.35 0.22 0.6 0.5 149	10 1145.48 38 20.28 22 9.19 6.55 0.2 2.23 0.05 0.2 0.2 152	11 16 2.98 38 19.62 22 14.76 10.52 0.4 2.30 0.07 0.4 0.4 153	12 2135.11 38 24.34 21 48.01 9.31 0.3 2.94 0.08 0.2 0.1 154	13 657.17 38 24.76 21 56.57 9.28 0.4 2.49 0.09 0.1 0.2 155	14 313.6/ 38 19.04 22 7.03 9.35 0.4 3.12 0.10 0.2 0.1 135 142 142 142 142 142 142 142 142 142 142	14.2/8.4/ 38.19.14 24.2.09 0.00 2.3 2.19 0.19 0.8 0.0 15/ 11.1513.61 38.17.06 27.0.76 8.60 0.6 7.00 0.06 0.5 16	001 C.0 C.0 0000 007 000 0000 070 77 0077 0C 10/CICC/I		20 119.25 38 14.41 22 4.88 7.84 0.5 2.51 0.12 0.2 0.3 163	20 521.84 38 14.21 22 4.89 8.38 0.6 2.90 0.12 0.2 0.2 164 20 1544.23 38 14.39 22 4.66 7.77 0.6 2.31 0.11 0.2 0.4 169
Time Lat Long Depth ERZ Mag. RMS ERX ERY n.ew	03 231747.65 3816.61 22 6.36 10.33 0.6 2.40 0.09 0.3 0.3 105 03 231947.65 38372 22 0.36 0.00 0.3 2.57 0.11 0.1 0.6	20 23 3916.24 38 14.41 22 5.94 8.77 1.4 2.31 0.22 0.8 1.0 107	03 23 4025.11 38 18.14 22 9.63 6.14 0.7 2.51 0.17 0.7 0.3 108	04 0579.15 3811.30 2148.45 7.00 0.4 2.42 0.12 0.4 0.4 109 04 14713.44 38.2072 22.1.76 9.47 0.6 2.58 0.06 0.2 0.2 110	04 2 3222.04 38 19.59 22 9.44 9.43 0.6 2.44 0.11 0.3 0.2 112	04 3 1333.92 38 22.47 22 11.90 9.69 0.4 2.35 0.09 0.3 0.3 113	04 3 3613.17 38 21.96 22 2.05 8.25 0.3 2.16 0.04 0.2 0.2 114 04 3 569177 38 21 86 21 44 47 8 57 0.1 2 34 0.07 0.2 0.1 115	04 8 4326.36 38 18.43 21 47.63 7.71 0.3 2.60 0.08 0.2 0.1 116	04 95721.25 38 27.24 21 54.52 10.51 0.3 2.66 0.09 0.1 0.2 117	04 11 1345.82 38 25.20 21 51.00 8.16 0.6 2.10 0.09 0.3 0.4 120	04 112319.88 3814.59 22 4.56 6.81 0.5 2.21 0.12 0.2 0.3 121 04 121201.55 2018.27 22 8.45 5.25 0.5 2.11 0.08 0.5 0.5 122	04 14 053.81 38 33.19 21 53.87 17.88 0.3 2.58 0.08 0.2 0.3 123	04 16 17 3.98 38 24.72 21 57.69 9.90 0.3 2.73 0.10 0.1 0.1 125	04 16 38 0.44 38 30.47 21 43.43 19.56 1.0 2.47 0.12 1.0 0.9 126	04 17 1542.97 38 15.62 22 3.58 7.29 0.4 2.42 0.11 0.2 0.2 127	04 18 2234.19 38 2/.39 21 49.31 10.78 0.3 2.38 0.08 0.2 0.2 129 24 10 3030 80 38 27 37 31 53 13 573 13 2.37 014 0.4 0.4 130	04 201637,49 38 20.76 21 49.09 7.27 1.5 2.38 0.23 0.9 0.5 131	04 20 3925.47 38 14.17 22 6.82 7.56 0.7 2.38 0.12 0.5 0.5 132	04 20 5419.35 38 14.28 22 4.90 7.42 0.5 2 43 0.16 0.4 0.4 133	04 214139./3 38 0.4/ 21 3/.19 0.89 2.3 2.09 0.20 0.0 1.4 134 04 22 5748.97 38 19.02 22 9.71 5.65 0.5 2.37 0.11 0.3 0.4 135	04 23 2253 89 38 16.44 21 57.98 5.51 0.4 2.61 0.11 0.2 0.2 136	05 0 219.19 38 20.00 21 49.47 6.54 0.5 2.58 0.09 0.3 0.3 137	05 02534.59 38 14.43 22 7.20 7.86 0.4 2.49 0.11 0.2 0.2 138 35 0.56.54 38 11.38 21 46.00 0.75 0.6 7.60 0.13 0.4 0.7 130	05 05127.11 3813.96 22 5.94 7.18 0.3 2.38 0.17 0.3 0.4 140	05 2 852.85 38 13.81 22 7.31 7.91 0.7 2.34 0.15 0.4 0.4 141	05 2 4654.52 38 25.97 21 55.47 10.00 0.3 2.63 0.10 0.1 0.1 142	05 3123247 38 20,45 22 9,44 6,72 0.3 2.28 0.10 0.3 0.3 144	05 3 20 0.11 38 20.71 22 9.42 6.78 0.3 2.54 0.13 0.2 0.2 145	05 3511.78 3814.07 22.7.50 7.50 0.3 2.55 0.12 0.2 0.2 146	05 4 1512.81 38 20.69 22 9.62 4.75 0.2 2.04 0.03 0.1 0.1 147 36 5 2 2 3 2 2 1 2 2 5 5 6 1 6 2 2 2 6 7 6 7 7 6 7 7 7 7 2 1 4	05 54753.96 3818.25 2211.16 6.20 0.6 2.35 0.22 0.6 0.5 149	05 10 1145.48 38 20.28 22 9.19 6.55 0.2 2.23 0.05 0.2 0.2 152	05 11 16 2.98 38 19.62 22 14.76 10.52 0.4 2.30 0.07 0.4 0.4 153	05 12 2135.11 38 24.34 21 48.01 9.31 0.3 2.94 0.08 0.2 0.1 154	05 13 657.17 38 24.76 21 56.57 9.28 0.4 2.49 0.09 0.1 0.2 155	0C1 1.0 7.0 01.0 7.1 6.7 0.2 7.0 1.0 0.1 7.0 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0	03 14.2/8.4/ 38 19.14 24 3.09 0.00 2.3 2.19 0.19 0.8 0.0 13/ 34 17 3513 61 38 37 36 37 076 37 0.6 3700 0.76 0.5 160	001 C/0 C/0 00/0 00/2 0/0 00/0 0/0 77 00/27 00/01/2/1 0/0 10/1 12 12/01/27 00/20 0/20 12/01/20 12/01/20 12/01/2	35 19 11 7.2 33 18 57 22 9.71 5.63 0.5 2.23 0.10 0.4 0.4 162	35 20 119.25 38 14.41 22 4.88 7.84 0.5 2.51 0.12 0.2 0.3 163	05 20 521.84 38 14.21 22 4.89 8.38 0.6 2.90 0.12 0.2 0.2 164 )5 20 1544.23 38 14.39 22 4.66 7.77 0.6 2.31 0.11 0.2 0.4 169

A microseismic study of the Gulf of Corinth 677

APPENDIX	B (Continued.	(																		
Date 010807	Time 22 2017 05	Lat 38 22 50	Long 22.11.64	Depth 10.32	ERZ 0.2	Mag. 2.30	RMS 0.07	ERX 0.2	ERY 0.2	Levt 235	Date 910810	Time 5 2515.48	Lat 38 14.08	Long 22 5 75	Depth EF	Z Wa		AS ER	XER	Y n.ev
910807	23 5913.23	38 13.89	22 7.22	8.26	0.6	2.39	0.16	0.4	4	236	910810	5 5042.11	38 19.27	22 9.48	5.10 1.5	25	100	200	5 6	38
910808	2 2512.14	38 16.12	22 10.38	7.27	0.9	2.25	0.08	0.9	4.0	237	910810	6 4039.00	38 11.60	21 48.78	6.95 0.2	2.7	9 0.1	0.4	0.2	297
910808	2 5757.85	38 20.81	22 2.88	8.41	0.5	2.32	0.0	0.2	0.2	238	910810	6 4927.92	38 14.20	22 5.77	7.16 1.0	52	10.2	00 00	0.5	298
910808 010608	4 753.43 4 11 0 73	38 24.24	21.99.15	9.12 8.45	0.4 1 4	235	0.07	5.0		65 07	018016	8 2941 75	38 9.04	22 5.86	6.73 0. 11 23 0.	2 7 2 7 2 7	00 00	0.0	000	56 2 2 6
910808	4 1435.76	38 14.65	22 5.18	9.71	0.7	2.63	0.18	0.3	5	141	910810	9413.20	38 20.70	22 9.49	6.64 0.	10.14	000		50	
910808	4 1558.69	38 14.59	22 5.28	9.45	0.5	2.70	0.14	0.2	0.2	242	910810	9 5515.09	38 20.91	22 9.16	5.98 0.5	5 2.2	9 0.1	0.0	0.	33
910808	10 5926.80	38 37.16	22 9.81	17.08	1.6	2.48	0.10	0.8	12	243	910810	10 740.83	38 24.87	21 57.10	8.67 0.4	1 2.1	2 0.0	5 0.2	0.3	304
910808	13 5147.83	38 14.60	22 6.20	8.17	0.7	0.0	0.08	0.3	0.5	946	910810	10 1535.73	38 23.94	21 54.15 20 2 2 2	8.98 0.1	5.5	6 0.1	2	0.2	305
910808	13 5935.04	38 14.43	22 4.97	7.85	0.3	2.61	0.11	0.2	2.5	947	010810	10 4227.95	38 13.91	22 7.37	7.04	1 2.6	1.0.1	0.0	0	308
910808	14 2649.75	38 17.11	22 7.85	8.34	0.8	5.8	0.14	0.4	2. 2	148	910810	0C.6C26.21	96.11 86	90.0 22	8.36	80 G	5 0.1	1 0.2	23	6 9 9
910808	16 1545.86 16 5074 95	38 20.40	22 1.60	9.45 6 7 5	0.4	2.54	0.10	0.7		240 250	910810	01.020 CI	38 14 48	41./C 12	8.00 9.53 9.53	51 6	1 0 0 0 0	0.2	5.5	310
910808	18 31 8.67	38 22 57	21 55.42	8.46	0.6	2.46	0.12	52	22	212	910810	14 40 3.30	38 29.50	21 52.45	12.34 0.6	12	8 0.1	5 0 5 0		312
910808	19 22 3.69	38 21.38	22 14.38	10.76	0.3	2.80	0.12	0.3	2	22	910810	15 1951.41	38 20.68	21 57.31	9.46 0.9	2.7	7 0.2	4 0.5	0	313
910808	20 319.46	38 19.05	22 2.27	8.95	0.4	2.78	0.09	0.2	0.1	233	910810	15 2247.60	38 21.26	21 44.46	10.64 0.7	1 2.7	9 0.1	6 0.5	0.7	314
910808	20 5814.07	38 14.88	22 5.99	8.05	0.3	0.0	0.07	0.2	50	54	910810	17 4426.29	38 14.08	22 7.44	7.52 0.4	1 2.6	2 0.1	3 0.3	0.3	315
910808	20 5827.4	38 14.91	22 6.08	8.15	0.3	2.73	0.11	0.2	50	255	910810	18 3917.03	38 14.74	22 5.06	5.64 0.6	5 2.3	6 0.1	1 0.3	0.2	316
910808	21 1227.67	38 24.58	21 48.84	8.38	0.2	2.31	0.05	0.2	0.2	121	910810	21 5039.64	38 14.38	22 6.11	7.06 0.3	1 2.3	7 0.1	3 0.3	0.3	318
910808	21 55 0.92	38 14.29	22 4.89	7.14	0.4	2.45	0.15	0.3	6.9	28	910810	22 26 0.27	38 19.41	22 9.79	7.15 0.7	0.0	0.0	8.0.8	0.8	320
610809	1 36 6.45	38 24.15	22 12.46	9.46	0.9	2.22	0.13	0.6	8. 1	53	910810	22 3742.65	38 14.64	22 4.99	7.33 0.5	2.5	1.0	7 0.3	0.3	321
910809	2 533.32	38 14.25	22 6.08	9.93 00.0	0.1	8.8	0.10	4.0	2.2	8	018010	22 4/30.30	38 22.71	22 1.47	9.00 0.4	5.7	9 1.0 2	6 G	2.5	322
910809	2 1941.23	58 14.00	22.0.22	5.5	0.1	8.6	80.0		* *	107	010010	CC-17CC C7	38 10 00	CI C 77	4.0.4 2.0 2.0	1 v 1 c		2 4		
910809	2 48 9.35	38 18.4/ 20 15 10	22 10.03	57.0	<u>.</u>	2.41	11.0	4 0	25	707	110019	0.407100	20.71.00	20./C 12	0.07 0.1 11 00 0 4			4 Q	56	324
910809	20.1000 C	38 21 68	27 2 01	5 0 8 7 8 7 8 7 8 7	70	6 F		3 6	3 -	503	910811	2 31 29.49	38 21.73	22 4.02	9.09 0.4	000			32	326
610809	7 1124.61	38 23.67	22 0.63	8.17	0.2	2.47	50.0	0.2	4	990	910811	2 50 1.43	38 20.88	21 47.04	8.08 0.6	2.7	5 0.1	5 0.5		327
608016	10 3 9.46	38 25.89	21 48.66	9.45	07	2.46	0.05	0.1	50	201	910811	4 729.23	38 20.55	22 12.22	8.30 0.4	24	0.0	4.0	0.5	328
608016	10 23 7.89	38 18.60	22 9.75	4.66	0.6	1.92	0.08	0.4	50	268	910811	4 2129.34	38 13.87	22 6.10	7.19 0.4	2.4	1 0.1	1 0.5	0.4	329
910809	11 56 5.24	38 18.77	22 8.50	7.13	0.2	2.71	0.12	0.2	0.1	569	910811	4 4018.90	38 14.48	22 4.86	6.42 0.7	22	3 0.1	20.4	0.3	330
608016	12 031.26	38 24.96	21 53.54	9.06	1.0	0.0	0.11	0.6	0.5	012	910811	4 4923.28	38 14.09	22 6.13	8.16 0.5	2.5	2 0.1	4.0.4	0.4	331
910809	12 623.41	38 24.71	21 53.92	8.90	0.7	0.0	0.11	0.4	4.0	112	910811	10 5031.72	38 9.37	22 2.42	7.27 0.4	2.4	2	7 0.3	9.	332
910809	13 2120.48	38 21.50	21 59.85	7.72	0.2	0.0	0.02	0.1	0.2	223	118019	14 42 6.34	38 27.65 20 20 20	22 1.77	8.52 0.4	6.1	000	0.2	<del>0</del> .0	333
910809	14 930.15	38 27.43	21 54.55	10.24	6.9	2.54	0.10	0.2		513	910811	15 5248 44	38 10 07	CC.6C 12	8.12 0.2	20 4 Clic				334
910809	16 1911 88	38 24 01	7C'0 77	VC./	+ 0		11.0		7 0	4/2	910811	15 5711 40	38 19.16	21 55.29	0.0 00.7			- 9	55	32,53
910809	16 3322.08	38 24.26	21 50.94	8.27	0.5	2.65	60.0	0.2	5	16	910811	16 218.06	38 22.24	21 59.60	7.96 0.2	2.7	3 0.1	5 0.1	0.1	337
910809	16 3514.21	38 24.25	21 51.06	7.28	0.3	2.16	0.05	0.1	0.3	Ш	910811	16 546.52	38 22.43	21 59.74	8.09 0.2	2.4	3 0.0	9 0.1	0.1	338
910809	17 1646.53	38 14.83	22 6.01	9.18	0.6	2.68	0.15	0.3	5.0	:78	910811	16 1017.00	38 20.49	22 9.63	5.66 0.3	1.9	2 0.0	4 0.2	0.1	339
910809	17 2653.04	38 14.69	22 6.18	9.79	0.5	2.59	0.11	0.2	0.2	6L:	118016	16 2329.71	38 22.54	21 59.95	7.71 0.7	2.3	3 0.1	0.2	0.3	340
910809	18 2738.05	38 19.24	21 46.94	8.74	0.9	2.54	0.14	0.5	53	80	910811	16 4434.18	38 20.53	22 9.53	5.38 0.3	6.1	00	4 0.1	0.1	341
608016	18 3428.40	38 25.03	21 57.29	9.6	0.4	2.44	0.09	0.2	0.2	82	118019	17 345.18	38 22.38	21 59.64	7.58 0.7	23	0.0	9 0.2	0.7	342
010809	20 1914.51	38 14.24	22 4.85	7.64	0.6	2.35	0.17	0.4	4	83	118019	17 1733.50	38 22.33 28 20 27	21 59.54	7.44 0.5	5.0	0.10		0.2	343
910800	CI-4CI 12	38 20.01 20 20 77	6C.1 22	16.11		8.6	0.12	4.0	2	22	110016	64.14C1 61	10.02.00	22 8.94 71 50 73	2.0 CI.0		500	0 c	5.5	<del>.</del>
910809	10:0C1 12	38 20 10	22 1.00 27 6 18	77.0	0 0 0	2 4 0 2 4 0	c1.0	3 2	12	00	910811	20 26 1.44	38 22.35	21 59.72	1.00 0.1 7 69 0.3	4			32	£ 97
910809	22 4659.30	38 24.17	21 58.04	9.48	0.7	2.24	0.12	18	1 2	8 <del>5</del>	910811	22 2135.96	38 29.46	21 58.27	12.76 0.6	4.7	80.10	5 02	. 4	350
910809	22 55 3.47	38 14.50	22 4.66	7.13	0.4	2.52	0.18	5	4	16	910811	23 3815.47	38 22.32	21 59.75	8.10 0.5	2.7	6 0.1	8 0.3	0.2	351
910809	23 1135.51	38 24.87	21 57.05	8.56	0.4	2.13	0.06	0.3	2	92	910812	0 1343.36	38 22.32	21 59.68	7.27 0.7	2.2	0.0	7 0.2	0.2	352
910809	23 5022.63	38 21.54	21 51.02	7.12	0.2	1.02	0.07	0.3	0.2	<b>93</b>	910812	0 2723.25	38 24.46	21 57.90	9.49 0.3	2.6	7 0.1	1 0.1	0.1	353
910810	2 31 4.86	38 18.59	22 11.57	6.95	0.3	2.67	0.15	4.0	22	94	910812	0 3258.21	38 22.30	21 59.85	7.85 0.5	0.0	0.1-0	4 0.2	0.4	354

5		. <u>.</u>		<u> </u>	. <i>~</i>	~		. ~	<b>_</b>				~	~			-				_							_	<u>.</u> .	-	_				~	~ -		
1.e. 403 409 410	14		415	416	418	420	<b>5</b>	14	424	425	426	428	429	430	431 64 62	433	43	436	437	439	4	<b>4</b> 5	1	45	4	4	447 450	451	452	453	4 <u>5</u> 4	455	45	451	458	455 46C	4 19	462
ER) 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	0.10	0.2	0.1	0.2	0.4	0.2	0.0	0.0	0.3	0.5	0.3	5 C	0.2	0.3		007	0.2	0.7	0.1	0.6	0.2	6.0	3	0.2	0.2	0.3	0.5	0.5	0.5	0.2	0.3	0.5	0.1	0.2	0.7	0.3	0.2	0.2
ERX 0.4 0.5 0.5	0.1	0.1	0.1	0.2	4 C	0.3	0.0	3 3	0.2	0.3	0.7	5 5	0.1	0.5	0.1	0.0	0.3	0.4	0.7	5 <b>5</b>	0.1	0.7	0.7	0.2	0.2	0.2	7 0	0.3	0.3	0.3	0.3	0.4	0.2	0.3	0.7	6.0 0	0.25	0.3
RMS 0.10 0.07 0.15	6.0	8 8 8	0.04	0.07	C 00	0.06	0.07	0.06	0.07	0.12	0.11	0.14	0.07	0.07	80 C	0.15	0.05	0.04	0.10	0.12	0.10	0.12	0.0	0.04	0.05	0.14	0.12	0.13	0.12	0.15	0.12	0.16	60.0	0.08	0.15	0.13	0.0	0.11
Mag. 2.31 2.58 2.56	2.61	0.0	0.0	0.0	5 6	0.0	2.27	2 <del>1</del> 0	0.00	0.0	800	5 6 7	2.30	2.02	2.03	241	2.11	1.92	2.5 <del>4</del>	88	2.12	2.33	88	2.41	1.79	2.53	2.74	2.12	2.62	2.58	2.37	2.32	2.52	0.0	2.32	2.48	2.13	2.57
ERZ 0.4 0.4 0.4	7 O O		38	0.6	0. <del>4</del>	0.5	0.5	50	0.3	0.5	0.4 0	0.3	0.3	0.5		0.5	0.2	0.3	0.3	0.5	0.3	- 0.0	10	0.3	0.4	40	20	0.7	0.6	0.3	5.0	0.7	<b>0.4</b>	0.9	0.1	0.0	4.0	0.4
Depth 7.78 7.54 5.05	69.6	12.5	121	2.20	8,8	8.0	5.38	.13	69.1	7.82	1.51	Q 19	9.43	52	202	88	5.86	6	8.21	57	8.27	10.23	i g	66:5	6	6.9	9.42	13.76	13.18	5.96	22	£83	22	2.62	2.92	- 22 22 22 22	2.29	11.04
						~				•			<u> </u>	~	~ .			•			~			•.					-	Ū	• ·	Ŭ		•,	•	~ ~		
000 2 5.28 1 59.74 2 11.27	1 58.23	1 59.29	1 59.73	1 56.25	c/.c 2 2 9.82	1 59.78	2 4.52	1 48.14	1 51.07	2 0.28	2 0.24	2 5.68	1 58.74	2 10.95	1.55.1	2 8.77	2 13.20	2 11.29	28.28	2 0.71	2 0.07	1 58.27	2 9.45	2 9.43	2 8.76	2 2.32	27.90 I 24.06	2 4.16	2 4.23	2 4.34	2 4.49	2 4.65	2 3.79	2 8.51	2 3.40	2 1.84 2 6 15	1 55.55	1 47.17
14444	101	100	10	00	1 11	7		1 (1	7	2	~ ~	4 74	6	61 0	2 10	1 11	2	6		1 11	6	0 r	1 11	6	2	. 10	2 4	ы	2	2	61	~	N	2	~ ~	2 10	1 14	7
ut 8 14.30 8 22.53 8 18.24 8 18.24	123.59 123.59	8 22.46 8 22.46	3 22.51	3 22.66	8 13.89 8 20.39	3 22.48	3 13.36	20.46	3 24.35	\$ 22.53	3 22.26	c/.cl (	8 25.19	3 22.03	5 25.34 M M M	8 19.57	3 20.83	3 22.02	3 20.13 2 22 45	3 23.07	3 22.62	5 24.91 2 22 05	3 20.56	3 20.55	3 21.58	3 12.79	333.70	34.09	333.85	3 14.66	3 13.96	3 14.22	3 21.07	3 18.80	3 16.36	5 21.36 8 14 42	3 25.36	8 23.27
****	ñ 77 7	* ** *	" <del>ന</del>	8 3	8 8 8 0	5 3	4 6	3 8 - 0	38	33	ж ж о ч	7 7 7 12	8 8	ж - 9	8 8 2 9	n m n Q	7 30	₩ -	۳ ۳ 	i m	÷ ۳	ri ri	i m	ñ	ñ	ة ة :	ল লাল	е ЭЭ	32	ю Э	8	7	ଳ । ଜୁନ	я У	ਲ ਹ ਕ	ñ ř	۲ آ	ŝ
ne 553.75 2 3.56 158.36	134.79	810.12 810.12	524.45	4325.2	039.1	5727.4	5245.3	3233.1	3647.3	5744.3	53 9.0	5238.3	4755.3	68.44	7754	4954.0	509.9	618.84	245.27	822.46	923.08	2 3.71 457 56	414.41	414.40	437.81	4 3.17	1639.9	1937.8	1946.(	1343.5	4957.9	14 7.2	1410.	3313.0	5134.5	026.89 342.47	2 6.06	731.25
		- 60 6	5 M	9 :	12	12	13	1 7	14	14	11	20	21	ដ	3 8	າ ຕ	23	-	 	10	6	m r	- 00	80	00	6	15	15	15	16	19	11	<u>61</u> (	61	ສ :			25
813 813 813	813 813	813 813	813	813	813	813	813	813	813	813	813	613 813	813	813	813	813	813	814	814	814	814	814	814	814	814	814	814	814	814	814	814	814	814	814	814	815	815	815
910 910 910	010	010	010	910	016 016	910	910	910	910	910	910	910	910	910	010	910	910	910	910	910	016	016	910	910	910	910	910	910	910	910	96	910	016	96	916	910	016	016
۲.																																						
355 356 357	359	361 361	363	364	36 36	367	368 360	370	371	372	373	375	376	377	378 270	380	381	382	383	385	386	387	88 88	390	391	392	565 <b>1</b> 05	395	396	397	398	399	400	401	<b>5</b> 4 24 29	403 404	405	406
ERY n.evt 0.2 355 0.1 356 0.2 357 0.1 358	0.2 359	0.6 361 0.6 361 0.7 367	0.3 363	0.2 364	0.1 305 0.2 366	0.2 367	0.4 368 0.5 368	0.2 370	0.3 371	0.1 372	0.2 373	0.5 375	0.2 376	0.2 377	0.4 378	0.2 380	0.6 381	0.2 382	0.1 383	0.1 385	0.5 386	0.3 387	0.5 389	0.2 390	0.1 391	0.2 392	0.3 393	0.3 395	0.3 396	0.9 397	0.2 398	0.3 399	0.3 400	1.1 401	0.4 402	0.1 403	0.3 405	0.3 406
ERX ERY n.evt 0.2 0.2 355 0.1 0.1 356 0.3 0.2 357 0.1 0.1 356	0.2 0.2 359 0.2 0.2 359 0.1 0.1 350	005 1.0 1.0 166 3.0 3.0 7.0 2.5	0.3 0.3 363	0.3 0.2 364	0.2 0.2 366	0.2 0.2 367	0.6 0.4 368	0.2 0.2 370	0.4 0.3 371	0.2 0.1 372	0.2 0.2 373	0.4 0.5 375	0.2 0.2 376	0.2 0.2 377	0.3 0.4 378	0.3 0.2 380	0.3 0.6 381	0.2 0.2 382	0.1 0.1 383	0.1 0.1 385	0.6 0.5 386	0.4 0.3 387	0.9 0.5 389	0.2 0.2 390	0.2 0.1 391	0.3 0.2 392	0.2 0.3 393 0.3 0.2 394	0.3 0.3 395	0.3 0.3 396	0.4 0.9 397	0.2 0.2 398	0.3 0.3 399	0.3 0.3 400	0.5 1.1 401	0.2 0.4 402	0.2 0.1 403 0.3 0.4 404	0.2 0.3 405	0.3 0.3 406
RMS ERX ERY n.evt 0.10 0.2 0.2 355 0.11 0.1 0.1 356 0.08 0.3 0.1 357 0.00 0.1 0.1 357	0.11 0.2 0.2 359 0.11 0.2 0.2 359 0.11 0.1 0.1 250	0.11 0.1 0.1 500 0.23 0.6 0.6 361 0.10 0.3 0.3 363	0.16 0.3 0.3 363	0.15 0.3 0.2 364	0.11 0.2 0.2 366	0.10 0.2 0.2 367	0.17 0.6 0.4 368	0.13 0.2 0.2 370	0.17 0.4 0.3 371	0.08 0.2 0.1 372	0.04 0.2 0.2 373	0.12 0.4 0.5 375	0.08 0.2 0.2 376	0.09 0.2 0.2 377	0.09 0.3 0.4 378 0.06 0.3 0.7 378	0.11 0.3 0.2 380	0.05 0.3 0.6 381	0.12 0.2 0.2 382	0.09 0.1 0.1 383	0.08 0.1 0.1 385	0.10 0.6 0.5 386	0.15 0.4 0.3 387	0.14 0.9 0.5 389	0.06 0.2 0.2 390	0.04 0.2 0.1 391	0.09 0.3 0.2 392	0.13 0.3 0.2 393	0.12 0.3 0.3 395	0.11 0.3 0.3 396	0.12 0.4 0.9 397	0.08 0.2 0.2 398	0.12 0.3 0.3 399	0.09 0.3 0.3 400	0.05 0.5 1.1 401	0.11 0.2 0.4 402	0.14 0.2 0.1 403 0.14 0.3 0.4 404	0.08 0.2 0.3 405	0.09 0.3 0.3 406
Mag. RMS ERX ERY n.evt 2.44 0.10 0.2 0.2 355 2.59 0.11 0.1 0.1 356 2.57 0.10 0.1 0.2 357 2.57 0.10 0.1 0.1 356	2.42 0.11 0.2 0.2 359 2.43 0.11 0.2 0.2 359 2.44 0.11 0.1 0.1 250	2.04 0.11 0.1 0.1 500 2.65 0.23 0.6 0.6 361 2.40 0.10 0.7 0.7 367	2.54 0.16 0.3 0.3 363	2.40 0.15 0.3 0.2 364	2.83 0.11 0.2 0.2 366	2.37 0.10 0.2 0.2 367	2.52 0.17 0.6 0.4 368 2.38 0.14 0.4 0.5 360	2.37 0.13 0.2 0.2 370	2.46 0.17 0.4 0.3 371	2.42 0.08 0.2 0.1 372	2.20 0.04 0.2 0.2 373	2.40 0.13 0.4 0.5 374 0.00 0.12 0.4 0.5 375	0.00 0.08 0.2 0.2 376	2.32 0.09 0.2 0.2 377	2.14 0.09 0.3 0.4 378 0.00 0.08 0.3 0.2 370	2.52 0.11 0.3 0.2 380	2.20 0.05 0.3 0.6 381	2.69 0.12 0.2 0.2 382	2.69 0.09 0.1 0.1 383 2.65 0.10 0.2 0.2 384	2.57 0.08 0.1 0.1 385	2.35 0.10 0.6 0.5 386	2.39 0.15 0.4 0.3 387 2.57 0.17 0.3 0.2 288	2.22 0.14 0.9 0.5 389	2.20 0.06 0.2 0.2 390	0.00 0.04 0.2 0.1 391	2.20 0.09 0.3 0.2 392	2.60 0.13 0.3 0.2 395	2.31 0.12 0.3 0.3 395	2.28 0.11 0.3 0.3 396	2.50 0.12 0.4 0.9 397	2.37 0.08 0.2 0.2 398	2.34 0.12 0.3 0.3 399	2.29 0.09 0.3 0.3 400	2.11 0.05 0.5 1.1 401	2.57 0.11 0.2 0.4 402	2.84 0.14 0.2 0.1 403 2.44 0.14 0.3 0.4 404	0.00 0.08 0.2 0.3 405	2.38 0.09 0.3 0.3 406
ERZ Mag. RMS ERX ERY n.evt 0.4 2.44 0.10 0.2 0.2 355 0.3 2.59 0.11 0.1 0.1 356 0.4 2.37 0.10 0.1 0.1 357 0.4 2.37 0.10 0.1 0.1 357	0.4 2.42 0.11 0.2 0.2 359 0.4 2.42 0.11 0.2 0.2 359 0.2 2.44 0.11 0.1 0.1 2.50	0.2 2.04 0.11 0.1 0.1 500 1.4 2.65 0.23 0.6 0.6 361 0.4 7.40 0.10 0.7 0.7 363	0.6 2.54 0.16 0.3 0.3 363	0.5 2.40 0.15 0.3 0.2 364	0.3 2.83 0.11 0.2 0.2 366	0.4 2.37 0.10 0.2 0.2 367	0.5 2.52 0.17 0.6 0.4 368	0.3 2.37 0.13 0.2 0.2 370	0.9 2.46 0.17 0.4 0.3 371	0.3 2.42 0.08 0.2 0.1 372	0.5 2.20 0.04 0.2 0.2 373	0.9 0.00 0.12 0.4 0.5 374	0.5 0.00 0.08 0.2 0.2 376	0.3 2.32 0.09 0.2 0.2 377	0.5 2.14 0.09 0.3 0.4 378 0.4 0.00 0.08 0.3 0.2 370	0.4 0.00 0.00 0.5 0.2 379 0.5 2.52 0.11 0.3 0.2 380	0.9 2.20 0.05 0.3 0.6 381	0.4 2.69 0.12 0.2 0.2 382	0.3 2.69 0.09 0.1 0.1 383 0.3 2.65 0.10 0.2 0.2 384	0.3 2.57 0.08 0.1 0.1 385	0.5 2.35 0.10 0.6 0.5 386	0.5 2.39 0.15 0.4 0.3 387	0.7 2.22 0.14 0.9 0.5 389	0.3 2.20 0.06 0.2 0.2 390	0.4 0.00 0.04 0.2 0.1 391	0.7 2.20 0.09 0.3 0.2 392	0.3 2.20 0.08 0.2 0.3 393 0.2 2.60 0.13 0.3 0.2 394	0.4 2.31 0.12 0.3 0.3 395	0.4 2.28 0.11 0.3 0.3 396	0.7 2.50 0.12 0.4 0.9 397	0.3 2.37 0.08 0.2 0.2 398	0.5 2.34 0.12 0.3 0.3 399	0.3 2.29 0.09 0.3 0.3 400	0.4 2.11 0.05 0.5 1.1 401	0.7 2.57 0.11 0.2 0.4 402	0.4 2.84 0.14 0.2 0.1 403 0.7 2.44 0.14 0.3 0.4 404	0.6 0.00 0.08 0.2 0.3 405	0.2 2.38 0.09 0.3 0.3 406
Depth ERZ Mag. RMS ERX ERY n.evt 7.56 0.4 2.44 0.10 0.2 0.2 355 8.55 0.3 2.59 0.11 0.1 0.1 356 8.00 0.4 2.38 0.08 0.3 0.2 357 7.8 0.3 2.57 0.10 0.1 356	7.78 0.4 2.42 0.11 0.2 0.2 359	6.1/ 0.2 2.04 0.11 0.1 0.1 500 9.52 1.4 2.65 0.23 0.6 0.6 361 6.85 0.1 2.40 0.10 0.2 0.3 262	9.47 0.6 2.54 0.16 0.3 0.3 363	7.47 0.5 2.40 0.15 0.3 0.2 364	8.65 0.3 2.83 0.11 0.2 0.2 366	8.89 0.4 2.37 0.10 0.2 0.2 367	12.08 0.5 2.52 0.17 0.6 0.4 368	8.05 0.3 2.37 0.13 0.2 0.2 370	9.69 0.9 2.46 0.17 0.4 0.3 371	8.78 0.3 2.42 0.08 0.2 0.1 372	8.57 0.5 2.20 0.04 0.2 0.2 373	7.92 0.9 0.00 0.12 0.4 0.5 375	7.50 0.5 0.00 0.08 0.2 0.2 376	8.38 0.3 2.32 0.09 0.2 0.2 377	9.13 0.5 2.14 0.09 0.3 0.4 378 7 24 04 000 008 03 0.2 370	7.24 0.4 0.00 0.00 0.2 379 7.58 0.5 2.52 0.11 0.3 0.2 380	12.44 0.9 2.20 0.05 0.3 0.6 381	7.40 0.4 2.69 0.12 0.2 0.2 382	9.57 0.3 2.69 0.09 0.1 0.1 383 8 12 0.3 2.65 0.10 0.2 0.2 384	8.47 0.3 2.57 0.08 0.1 0.1 385	6.13 0.5 2.35 0.10 0.6 0.5 386	7.77 0.5 2.39 0.15 0.4 0.3 387 9.08 0.6 2.57 0.17 0.3 0.2 388	11.64 0.7 2.22 0.14 0.9 0.5 389	8.13 0.3 2.20 0.06 0.2 0.2 390	6.82 0.4 0.00 0.04 0.2 0.1 391	6.79 0.7 2.20 0.09 0.3 0.2 392	0.40 U.3 2.20 U.08 U.2 U.3 393 6.78 0.2 2.60 0.13 0.3 0.2 394	6.44 0.4 2.31 0.12 0.3 0.3 395	6.22 0.4 2.28 0.11 0.3 0.3 396	10.90 0.7 2.50 0.12 0.4 0.9 397	9.56 0.3 2.37 0.08 0.2 0.2 398	7.45 0.5 2.34 0.12 0.3 0.3 399	<b>6.</b> 89 <b>0.3 2.29 0.09 0.3 0.3 400</b>	17.28 0.4 2.11 0.05 0.5 1.1 401	5.91 0.7 2.57 0.11 0.2 0.4 402	8.50 0.4 2.84 0.14 0.2 0.1 403 8.00 0.7 2.44 0.14 0.3 0.4 404	7.46 0.6 0.00 0.08 0.2 0.3 405	6.88 0.2 2.38 0.09 0.3 0.3 406
Depth ERZ Mag. RMS ERX ERY n.evt 3 7.56 0.4 2.44 0.10 0.2 0.2 355 7 8.55 0.3 2.59 0.11 0.1 0.1 356 8.00 0.4 2.38 0.08 0.3 0.2 357 7 8.00 3 3.57 0.10 0.1 356	7.78 0.4 2.42 0.11 0.1 0.1 550 7 7.78 0.4 2.42 0.11 0.2 0.2 359 8 9 7 0 7 2.44 0.11 0.1 2.55	9.11 0.2 2.04 0.11 0.1 0.1 500 9.52 1.4 2.65 0.23 0.6 0.6 361 5 5 5 5 0.4 2.00 0.10 0.7 375	9.47 0.6 2.54 0.16 0.3 0.3 363	4 7.47 0.5 2.40 0.15 0.3 0.2 364	5 8.65 0.3 2.83 0.11 0.2 0.2 366	1 8.89 0.4 2.37 0.10 0.2 0.2 367	5 12.08 0.5 2.52 0.17 0.6 0.4 368 5 8.21 0.8 2.39 0.14 0.4 0.5 360	2 8.05 0.3 2.37 0.13 0.2 0.2 370	9.69 0.9 2.46 0.17 0.4 0.3 371	8.78 0.3 2.42 0.08 0.2 0.1 372	1 8.57 0.5 2.20 0.04 0.2 0.2 373	7.92 0.9 0.00 0.12 0.4 0.5 375	0 7.50 0.5 0.00 0.08 0.2 0.2 376	8.38 0.3 2.32 0.09 0.2 0.2 377	5 9.13 0.5 2.14 0.09 0.3 0.4 378 5 7.24 0.4 0.00 0.6 0.3 0.2 370	7.24 0.4 0.00 0.00 0.0 0.2 379 7.58 0.5 2.52 0.11 0.3 0.2 380	12.44 0.9 2.20 0.05 0.3 0.6 381	7.40 0.4 2.69 0.12 0.2 0.2 382	0.57 0.3 2.69 0.09 0.1 0.1 383	0.12 0.13 2.57 0.08 0.1 0.1 385	3 6.13 0.5 2.35 0.10 0.6 0.5 386	7.77 0.5 2.39 0.15 0.4 0.3 387 0.08 0.6 2.57 0.17 0.3 0.2 200	11.64 0.7 2.22 0.14 0.9 0.5 389	3 8.13 0.3 2.20 0.06 0.2 0.2 390	l 6.82 0.4 0.00 0.04 0.2 0.1 391	3 6.79 0.7 2.20 0.09 0.3 0.2 392	6.40 0.3 2.20 0.08 0.2 0.3 393 6.78 0.2 2.60 0.13 0.3 0.2 394	6.44 0.4 2.31 0.12 0.3 0.3 395	6.22 0.4 2.28 0.11 0.3 0.3 396	10.90 0.7 2.50 0.12 0.4 0.9 397	l 9.56 0.3 2.37 0.08 0.2 0.2 398	2 7.45 0.5 2.34 0.12 0.3 0.3 399	6.89 0.3 2.29 0.09 0.3 0.3 400	8 17.28 0.4 2.11 0.05 0.5 1.1 401	3 5.91 0.7 2.57 0.11 0.2 0.4 402	8.50 0.4 2.84 0.14 0.2 0.1 403 8.00 0.7 2.44 0.14 0.3 0.4 404	1 7.46 0.6 0.00 0.08 0.2 0.3 405	6.88 0.2 2.38 0.09 0.3 0.3 406
Aong Depth ERZ Mag. RMS ERX ERY n.evt   159.78 7.56 0.4 2.44 0.10 0.2 0.2 355   159.77 8.55 0.3 2.59 0.11 0.1 0.1 356   159.77 8.55 0.3 2.59 0.11 0.1 0.1 356   2 5.66 8.00 0.4 2.38 0.08 0.3 0.2 357   15 5.57 0.10 0.1 0.1 0.1 356	1.39.75 7.78 0.5 2.57 0.10 0.1 0.2 0.2 359 1.59.75 7.78 0.4 2.42 0.11 0.2 0.2 359	1. 37.67 6.17 0.2 2.64 0.11 0.1 0.1 0.0 2. 0.05 9.52 1.4 2.65 0.23 0.6 0.6 361 1. 50.7 5.85 0.4 3.07 0.10 0.7 351	<b>2</b> 3.40 9.47 0.6 2.54 0.16 0.3 0.3 363	1 59.74 7.47 0.5 2.40 0.15 0.3 0.2 364	2 2.04 8.05 0.3 2.83 0.11 0.2 0.2 366 11 46.15 8.65 0.3 2.83 0.11 0.2 0.2 366	.1 57.21 8.89 0.4 2.37 0.10 0.2 0.2 367	2 15.95 12.08 0.5 2.52 0.17 0.6 0.4 368 3 50 55 8 21 0 5 23 0.14 0.4 0 5 350	1 59.72 8.05 0.3 2.37 0.13 0.2 0.2 370	2 4.40 9.69 0.9 2.46 0.17 0.4 0.3 371	2 1.58 8.78 0.3 2.42 0.08 0.2 0.1 372	1 59.64 8.57 0.5 2.20 0.04 0.2 0.2 373	2 0.18 7.92 0.9 0.00 0.12 0.4 0.5 375	1 59.80 7.50 0.5 0.00 0.08 0.2 0.2 376	2 1.46 8.38 0.3 2.32 0.09 0.2 0.2 377	149.06 9.13 0.5 2.14 0.09 0.3 0.4 378 140.75 7.24 0.4 0.00 0.6 0.3 0.2 379	1.39.13 1.24 0.4 0.00 0.00 0.2 0.2 319 2.7.25 7.58 0.5 2.52 0.11 0.3 0.2 380	2 8.68 12.44 0.9 2.20 0.05 0.3 0.6 381	2 6.22 7.40 0.4 2.69 0.12 0.2 0.2 382	2 0.60 9.57 0.3 2.69 0.09 0.1 0.1 383 148.24 8.12 0.3 2.65 0.10 0.7 0.7 384	159.79 8.47 0.3 2.57 0.08 0.1 0.1 385		2 1.15 7.77 0.5 2.39 0.15 0.4 0.3 387 3 5 85 0 06 0 5 3 0 17 0 3 0 3 208	<b>2</b> 13.03 11.64 0.7 <b>2.22</b> 0.14 0.9 0.5 389	1 59.63 8.13 0.3 2.20 0.06 0.2 0.2 390	1 59.31 6.82 0.4 0.00 0.04 0.2 0.1 391	1 59.48 6.79 0.7 2.20 0.09 0.3 0.2 392	2 9.42 0.40 0.3 2.20 0.08 0.2 0.3 393 2 9.58 6.78 0.2 2.60 0.13 0.3 0.2 394	2 9.42 6.44 0.4 2.31 0.12 0.3 0.3 395	2 9.30 6.22 0.4 2.28 0.11 0.3 0.3 396	2 1.42 10.90 0.7 2.50 0.12 0.4 0.9 397	1 54.91 9.56 0.3 2.37 0.08 0.2 0.2 398	1 59.82 7.45 0.5 2.34 0.12 0.3 0.3 399	2 9.57 6.89 0.3 2.29 0.09 0.3 0.3 400	1 52.88 17.28 0.4 2.11 0.05 0.5 1.1 401	157.58 5.91 0.7 2.57 0.11 0.2 0.4 402	1 39.87 8.50 0.4 2.84 0.14 0.2 0.1 403 2 0.06 8 00 0.7 2.44 0 14 0.3 0.4 404	<b>1</b> 59.73 7.46 0.6 0.00 0.08 0.2 0.3 405	2 9.56 6.88 0.2 2.38 0.09 0.3 0.3 406
Long Deptil ERZ Mag. RMS ERX ERY n.evt   21 5978 7.56 0.4 2.44 0.10 0.2 0.2 355   21 5977 8.55 0.3 2.59 0.11 0.1 31 356   21 5977 8.55 0.3 2.59 0.11 0.1 356   22 5.66 8.00 0.4 2.38 0.08 0.3 0.2 357   21 5917 8.50 3.69 0.3 0.2 357   22 5.66 8.00 0.4 2.38 0.08 0.3 0.2 357   21 5017 7.57 0.10 0.1 2.55 0.11 0.1 2.55	2193/31 / 20 22 23 24 24 24 25 25 25 21 25 25 25 25 25 25 25 25 25 25 25 25 25	22 0.05 6.17 0.2 2.04 0.11 0.1 0.1 500 22 0.05 9.52 1.4 2.65 0.23 0.6 0.6 361 21 6.6 0.6 1.4 0.10 0.7 2.5	22 3.40 9.47 0.6 2.54 0.16 0.3 0.3 363	21 59.74 7.47 0.5 2.40 0.15 0.3 0.2 364	22 2.04 8.65 0.3 2.83 0.11 0.2 0.2 366	21 57.21 8.89 0.4 2.37 0.10 0.2 0.2 367	22 15.95 12.08 0.5 2.52 0.17 0.6 0.4 368 21 50 55 8 21 0.8 238 0.14 0.4 0.5 350	21 59.72 8.05 0.3 2.37 0.13 0.2 0.2 370	22 4.40 9.69 0.9 2.46 0.17 0.4 0.3 371	22 1.58 8.78 0.3 2.42 0.08 0.2 0.1 372	21 59.64 8.57 0.5 2.20 0.04 0.2 0.2 373	22 0.18 7.92 0.9 0.00 0.12 0.4 0.5 374	21 59.80 7.50 0.5 0.00 0.08 0.2 0.2 376	22 1.46 8.38 0.3 2.32 0.09 0.2 0.2 377	21 49.06 9.13 0.5 2.14 0.09 0.3 0.4 378 21 60 75 7 24 0.4 0.00 0.8 03 0.2 370	22 7.25 7.58 0.5 2.52 0.11 0.3 0.2 379	22 8.68 12.44 0.9 2.20 0.05 0.3 0.6 381	22 6.22 7.40 0.4 2.69 0.12 0.2 0.2 382	22 0.60 9.57 0.3 2.69 0.09 0.1 0.1 383 21 48 24 8 12 0 3 2 65 0 10 0 2 0 2 384	21 59.79 8.47 0.3 2.57 0.08 0.1 0.1 385	22 10.03 6.13 0.5 2.35 0.10 0.6 0.5 386	22 1.15 7.77 0.5 2.39 0.15 0.4 0.3 387 22 56 0.08 0.6 2.57 0.17 0.3 0.2 388	<b>22</b> 13.03 11.64 0.7 2.22 0.14 0.9 0.5 389	21 59.63 8.13 0.3 2.20 0.06 0.2 0.2 390	21 59.31 6.82 0.4 0.00 0.04 0.2 0.1 391	21 59.48 6.79 0.7 2.20 0.09 0.3 0.2 392	22 9.42 0.40 0.3 2.20 0.08 0.2 0.3 393 22 9.58 6.78 0.2 2.60 0.13 0.3 0.2 394	22 9.42 6.44 0.4 2.31 0.12 0.3 0.3 395	22 9.30 6.22 0.4 2.28 0.11 0.3 0.3 396	22 1.42 10.90 0.7 2.50 0.12 0.4 0.9 397	21 54.91 9.56 0.3 2.37 0.08 0.2 0.2 398	21 59.82 7.45 0.5 2.34 0.12 0.3 0.3 399	22 9.57 6.89 0.3 2.29 0.09 0.3 0.3 400	21 52.88 17.28 0.4 2.11 0.05 0.5 1.1 401	21 57.58 5.91 0.7 2.57 0.11 0.2 0.4 402	21 29:87 8:20 0.4 2:84 0.14 0.2 0.1 403 22 0.06 8:00 0.7 2:44 0.14 0.3 0.4 404	21 59.73 7.46 0.6 0.00 0.08 0.2 0.3 405	22 9.56 6.88 0.2 2.38 0.09 0.3 0.3 406
at Long Depth ERZ Mag. RMS ERX ERY nevt 322.38 2159.78 7.56 0.4 2.44 0.10 0.2 0.2 355 322.38 2159.77 8.55 0.3 2.59 0.11 0.1 0.1 356 315.65 22 5.66 8.00 0.4 2.38 0.08 0.3 0.2 357 22 30 21 28 0.3 356 0.01 0.1 356	22.2.3 21.37.61 7.80 0.2 2.0 0.1 0.1 0.1 5.0 22.3.1 21.59.75 7.78 0.4 2.42 0.11 0.1 0.2 359 23.7.51 21.69.7 2.7.51 0.11 0.1 2.50	8 22 22 21 27 20 8.17 0.2 2.04 0.11 0.1 0.1 500 8 23 22 22 0.05 9.52 1.4 2.65 0.23 0.6 0.6 361 3 2 3 4 0 0.0 0.0 2 361	313.15 22 3.40 9.47 0.6 2.54 0.16 0.3 0.3 363	8 22.16 21 59.74 7.47 0.5 2.40 0.15 0.3 0.2 364	8 21:1/ 22 2:04 8:05 0.3 2.83 0.11 0.2 0.2 366 3 22.67 21 46.15 8:65 0.3 2.83 0.11 0.2 0.2 366	3 24.80 21 57.21 8.89 0.4 2.37 0.10 0.2 0.2 367	321.78 2215.95 12.08 0.5 2.52 0.17 0.6 0.4 368 273 53 2150 55 821 0.8 238 0.14 0.4 0.5 350	8 22.44 21 59.72 8.05 0.3 2.37 0.13 0.2 0.2 370	317.23 22 4.40 9.69 0.9 2.46 0.17 0.4 0.3 371	3 22.16 22 1.58 8.78 0.3 2.42 0.08 0.2 0.1 372	3 22.38 21 59.64 8.57 0.5 2.20 0.04 0.2 0.2 373	14.24 22 0.18 7.92 0.9 0.00 0.12 0.4 0.5 374 122.47 22 0.18 7.92 0.9 0.00 0.12 0.4 0.5 375	3 22.49 21 59.80 7.50 0.5 0.00 0.08 0.2 0.2 376	321.98 22 1.46 8.38 0.3 2.32 0.09 0.2 0.2 377	8 25.79 21 49.06 9.13 0.5 2.14 0.09 0.3 0.4 378 117 66 21 60 75 7.24 0.4 0.00 0.6 0.3 0.7 370	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	135.75 22 8.68 12.44 0.9 2.20 0.05 0.3 0.6 381	1 14.73 22 6.22 7.40 0.4 2.69 0.12 0.2 0.2 382	823.34 22 0.60 9.57 0.3 2.69 0.09 0.1 0.1 383 03.01 21.48.24 8.12 0.3 2.65 0.10 0.2 0.2 384	122.40 21 59.79 8.47 0.3 2.57 0.08 0.1 0.1 385	118.26 22 10.03 6.13 0.5 2.35 0.10 0.6 0.5 386	8 16.70 22 1.15 7.77 0.5 2.39 0.15 0.4 0.3 387 0.00 1 23 5.85 0.08 0.5 2.57 0.17 0.3 0.3 388	122.24 22 13.03 11.64 0.7 2.22 0.14 0.9 0.5 389	122.49 21 59.63 8.13 0.3 2.20 0.06 0.2 0.2 390	122.34 21 59.31 6.82 0.4 0.00 0.04 0.2 0.1 391	1 22.38 21 59.48 6.79 0.7 2.20 0.09 0.3 0.2 392	2.20.34 22.9.42 0.40 0.3 2.22 0.08 0.2 0.3 393 1.20.92 22.9.58 6.78 0.2 2.60 0.13 0.3 0.2 394	120.55 22 9.42 6.44 0.4 2.31 0.12 0.3 0.3 395	120.65 22 9.30 6.22 0.4 2.28 0.11 0.3 0.3 396	17.63 22 1.42 10.90 0.7 2.50 0.12 0.4 0.9 397	126.67 21 54.91 9.56 0.3 2.37 0.08 0.2 0.2 398	122.65 21 59.82 7.45 0.5 2.34 0.12 0.3 0.3 399	120.28 22 9.57 6.89 0.3 2.29 0.09 0.3 0.3 400	133.03 21 52.88 17.28 0.4 2.11 0.05 0.5 1.1 401	123.67 21 57.58 5.91 0.7 2.57 0.11 0.2 0.4 402	22.46 21 29.87 8.50 0.4 2.84 0.14 0.2 0.1 403 22.29 22 0.06 8.00 0.7 2.44 0.14 0.3 0.4 404	<b>22.52</b> 21 59.73 7.46 0.5 0.00 0.08 0.2 0.3 405	20.55 22 9.56 6.88 0.2 2.38 0.09 0.3 0.3 406
Lat Long Depth ERZ Mag. RMS ERX ERY n.evt   38 22.38 21 59.78 7.56 0.4 2.44 0.10 0.2 0.2 355   13 8 22.38 21 59.77 8.55 0.3 2.59 0.11 0.1 355   13 8 22.38 21 59.77 8.55 0.3 2.59 0.11 0.1 356   13 8 22.38 21 59.77 8.55 0.3 2.59 0.01 0.1 356   38 22.38 22 5.66 8.00 0.4 2.38 0.08 0.3 0.2 357   38 77 30 7 57 0.1 0.1 0.1 256	0.0 22.31 21.59.76 7.80 0.5 2.50 0.10 0.1 0.1 0.50 2.159.75 7.78 0.4 2.42 0.11 0.1 0.2 359 2.357.75 1.50.77 0.1 2.50	0 30.22.20 21.37.07 8.17 0.2 2.04 0.11 0.1 0.1 300 1 323.25 22.0.05 9.52 1.4 2.65 0.23 0.6 0.6 361 3 3 3 3 4 0 1 0 0 0 0 3 361	<b>38 13.15 22 3.40 9.47</b> 0.6 <b>2.54</b> 0.16 0.3 0.3 363	38 22.16 21 59.74 7.47 0.5 2.40 0.15 0.3 0.2 364	38 21:17 22 2.04 8.55 0.3 2.83 0.11 0.2 0.2 366 38 22.67 21 46.15 8.65 0.3 2.83 0.11 0.2 0.2 366	38 24.80 21 57.21 8.89 0.4 2.37 0.10 0.2 0.2 367	) 38 21.78 22 15.95 12.08 0.5 2.52 0.17 0.6 0.4 368 28 27 63 21 60 66 8 21 0 8 2 38 0 14 0 4 0 5 360	38 22.44 21 59.72 8.05 0.3 2.37 0.13 0.2 0.2 370	i 38 17.23 22 4.40 9.69 0.9 2.46 0.17 0.4 0.3 371	38 22.16 22 1.58 8.78 0.3 2.42 0.08 0.2 0.1 372	38 22.38 21 59.64 8.57 0.5 2.20 0.04 0.2 0.2 373	38 22.47 22 0.18 7.92 0.9 0.00 0.12 0.4 0.5 375	0 38 22.49 21 59.80 7.50 0.5 0.00 0.08 0.2 0.2 376	38 21.98 22 1.46 8.38 0.3 2.32 0.09 0.2 0.2 377	2 38 25.79 21 49.06 9.13 0.5 2.14 0.09 0.3 0.4 378 2 38 27 56 21 50 75 7.7 0.4 0.00 0.3 0.3 270	3 38 14.45 22 7.25 7.58 0.5 2.52 0.11 0.3 0.2 380	1 38 35.75 22 8.68 12.44 0.9 2.20 0.05 0.3 0.6 381	5 38 14.73 22 6.22 7.40 0.4 2.69 0.12 0.2 0.2 382	9 38 23 34 22 0.60 9.57 0.3 2.69 0.09 0.1 0.1 383 3 38 23 01 21 48 24 8 12 03 3 55 0.10 02 02 384	7 38 22.40 21 59.79 8.47 0.3 2.57 0.08 0.1 0.1 385	9 38 18.26 22 10.03 6.13 0.5 2.35 0.10 0.6 0.5 386	↓ 3816.70 221.15 7.77 0.5 2.39 0.15 0.4 0.3 387 ○ 38.20.01 27.5.85 0.08 0.5 2.57 0.17 0.3 0.3 288	3 38 22.24 22 13.03 11.64 0.7 2.22 0.14 0.9 0.5 389	2 38 22 49 21 59 63 8.13 0.3 2.20 0.06 0.2 0.2 390	9 38 22.34 21 59.31 6.82 0.4 0.00 0.04 0.2 0.1 391	3 38 22.38 21 59.48 6.79 0.7 2.20 0.09 0.3 0.2 392	1 38 20:34 22 9.42 0.40 0.3 2.20 0.08 0.2 0.3 393 0 38 20 92 22 9.58 6.78 0.2 2.60 0.13 0.3 0.2 304	4 38 20.55 22 9.42 6.44 0.4 2.31 0.12 0.3 0.3 395	1 38 20.65 22 9.30 6.22 0.4 2.28 0.11 0.3 0.3 396	7 38 7.63 22 1.42 10.90 0.7 2.50 0.12 0.4 0.9 397	5 38 26.67 21 54.91 9.56 0.3 2.37 0.08 0.2 0.2 398	2 38 22.65 21 59.82 7.45 0.5 2.34 0.12 0.3 0.3 399	5 38 20.28 22 9.57 6.89 0.3 2.29 0.09 0.3 0.3 400	4 38 33.03 21 52.88 17.28 0.4 2.11 0.05 0.5 1.1 401	4 38 23.67 21 57.58 5.91 0.7 2.57 0.11 0.2 0.4 402	1 38 22 40 21 39 87 8.50 0.4 2.84 0.14 0.2 0.1 403 0 38 22 29 22 0.06 8.00 0.7 2.44 0.14 0.3 0.4 404	38 22.52 21 59.73 7.46 0.6 0.00 0.08 0.2 0.3 405	38 20.55 22 9.56 6.88 0.2 2.38 0.09 0.3 0.3 406
Inc Lat Long Depth ERZ Mag. RMS ERX ERY n.evt   151.66 38.22.38 2159.78 7.56 0.4 2.44 0.10 0.2 0.2 355   1745.08 38.22.38 2159.77 8.55 0.3 2.59 0.11 0.1 0.1 356   544556 38.22.38 2159.77 8.55 0.3 2.59 0.11 0.1 356   54556 38.15.65 2.2 5.66 8.00 0.4 2.38 0.08 0.3 2.35   50 38.7 9.03 7.37 0.01 0.1 356	22.2.2. 30.2.2.3 21.5.2.1 7.00 7.2 2.5 0.10 0.1 0.1 5.5 10.44.15 32.31 21.59.75 7.78 0.4 2.42 0.11 0.1 0.2 359 10.45 38.3.25 21.59.75 7.7 0.3 5.4 0.11 0.1 0.1 2.50	0441.30 38 12.20 21 37.67 8.17 0.1 2.04 0.11 0.1 0.1 300 859.34 38 23.25 22 0.05 9.52 1.4 2.65 0.23 0.6 0.6 361 031.03 38 37 34 71 67 37 26 0.4 7.10 0.10 0.7 267	345.19 38 13.15 22 3.40 9.47 0.6 2.54 0.16 0.3 0.3 363	16.3.51 38.22.16 21 59.74 7.47 0.5 2.40 0.15 0.3 0.2 364	2/8.24 38 21.1/ 22 2.04 8.53 0.3 2.83 0.11 0.2 0.2 366 738.19 38 22.67 21 46.15 8.65 0.3 2.83 0.11 0.2 0.2 366	3 7.68 38 24.80 21 57.21 8.89 0.4 2.37 0.10 0.2 0.2 367	927.39 38.21.78 22.15.95 12.08 0.5 2.52 0.17 0.6 0.4 368 200.35 28.27.53 21.50.05 8.21 0.8 2.32 0.14 0.5 2.50	351.81 38 22.44 21 59.72 8.05 0.3 2.37 0.13 0.2 0.2 370	748.54 38 17.23 22 4.40 9.69 0.9 2.46 0.17 0.4 0.3 371	5 4.12 38 22.16 22 1.58 8.78 0.3 2.42 0.08 0.2 0.1 372	15 7.39 38 22.38 21 59.64 8.57 0.5 2.20 0.04 0.2 0.2 373	717 36 14.24 22 3.30 7.42 0.3 2.40 0.13 0.4 0.5 374 V43.44 38 22.47 22 0.18 7.92 0.9 0.00 0.12 0.4 0.5 375	942.10 38 22.49 21 59.80 7.50 0.5 0.00 0.08 0.2 0.2 376	045.48 38.21.98 22 1.46 8.38 0.3 2.32 0.09 0.2 0.2 377	226.67 38 25.79 21 49.06 9.13 0.5 2.14 0.09 0.3 0.4 378 457 58 38 77 66 71 50 75 7.74 0.4 0.00 0.08 0.3 0.7 370	4.2.2.0 30 2.2.00 21 39.1 24 0.4 0.4 0.00 0.00 0.2 0.2 319 355.73 38 14.45 22 7.25 7.58 0.5 2.52 0.11 0.3 0.2 380	3650.81 38 35.75 22 8.68 12.44 0.9 2.20 0.05 0.3 0.6 381	3244.75 38 14.73 22 6.22 7.40 0.4 2.69 0.12 0.2 0.2 382	3315.19 38 23.34 22 0.60 9.57 0.3 2.69 0.09 0.1 0.1 383 545703 38 23.61 21 48 24 8 12 0.3 2.65 0.10 0.7 0.7 384	4436.87 38 22.40 21 59.79 8.47 0.3 2.57 0.08 0.1 0.1 385	5828.49 38 18.26 22 10.03 6.13 0.5 2.35 0.10 0.6 0.5 386	335.74 3816.70 221.15 7.77 0.5 2.39 0.15 0.4 0.3 387 813.00 38.00.01 2258 0.08 0.6 2.67 0.7 0.3 0.2 388	1637.93 38 22.24 22 13.03 11.64 0.7 2.22 0.14 0.9 0.5 389	4130.22 38 22.49 21 59.63 8.13 0.3 2.20 0.06 0.2 0.2 390	2245.59 38 22.34 21 59.31 6.82 0.4 0.00 0.04 0.2 0.1 391	270.18 38 22.38 21 59.48 6.79 0.7 2.20 0.09 0.3 0.2 392	2829./1 38 20.34 22 9.42 0.40 0.3 2.22 0.08 0.2 0.3 393 051.69 38 20.92 22 9.58 6.78 0.2 2.60 0.13 0.3 0.2 394	1750.04 38 20.55 22 9.42 6.44 0.4 2.31 0.12 0.3 0.3 395	3945.11 38 20.65 22 9.30 6.22 0.4 2.28 0.11 0.3 0.3 396	5513.37 38 7.63 22 1.42 10.90 0.7 2.50 0.12 0.4 0.9 397	3925.45 38 26.67 21 54.91 9.56 0.3 2.37 0.08 0.2 0.2 398	035.12 38 22.65 21 59.82 7.45 0.5 2.34 0.12 0.3 0.3 399	1025.05 38 20.28 22 9.57 6.89 0.3 2.29 0.09 0.3 0.3 400	2320.24 38 33.03 21 52.88 17.28 0.4 2.11 0.05 0.5 1.1 401	2819.44 38 23.67 21 57.58 5.91 0.7 2.57 0.11 0.2 0.4 402	252.2.1 38 22.40 21 39.87 8.50 0.4 2.84 0.14 0.2 0.1 403 42 2.80 38 22.29 22 0.06 8.00 0.7 2.44 0.14 0.3 0.4 404	25.03 38.22.52 21.59.73 7.46 0.5 0.00 0.08 0.2 0.3 405	9 2.50 38 20.55 22 9.56 6.88 0.2 2.38 0.09 0.3 0.3 406
Time Lat Long Depth ERZ Mag. RMS ERX ERY n.evt   0451.66 38.22.38 2159.78 7.56 0.4 2.44 0.10 0.2 0.2 355   04745.08 38.22.38 2159.77 8.55 0.3 2.59 0.11 0.1 0.1 356   04745.08 38.22.38 2159.77 8.55 0.3 2.59 0.11 0.1 356   0556.56 3815.65 22.5.66 8.00 0.4 2.38 0.08 0.3 2.57   0750.55 3815.65 22.5.66 8.00 0.4 2.38 0.08 0.2 357   0720.55 3877.30 7.57 0.4 7.0 0.1 255	122 7.1 50 22.21 21.50 7.1 7.0 51 51 51 51 51 51 51 51 51 51 51 51 51	1404/.20 36.22.20 21.37.57 0.17 0.2 2.04 0.11 0.1 0.1 300 3.83034 38.23.25 22.0.05 9.52 1.4 2.65 0.23 0.5 0.6 361 3.3703103 38.37.45 71 67.57 5.68 0.4 7.40 0.10 0.3 357	35345.19 38 13.15 22 3.40 9.47 0.6 2.54 0.16 0.3 0.3 363	4 26 3.51 38 22.16 21 59.74 7.47 0.5 2.40 0.15 0.3 0.2 364	4 2/ 8.24 38 21.17 22 2.04 8.25 0.3 2.31 0.1/ 0.1 0.1 305 5 738.19 38 22.67 21 46.15 8.65 0.3 2.83 0.11 0.2 0.2 366	5 13 7.68 38 24.80 21 57.21 8.89 0.4 2.37 0.10 0.2 0.2 367	5 2927.39 38 21.78 22 15.95 12.08 0.5 2.52 0.17 0.6 0.4 368 6 000 35 38 37 63 31 60 06 9 31 0 8 3 38 0 14 0 4 0 5 360	6 [351.8] 38 22.44 21 59.72 8.05 0.3 2.37 0.13 0.2 0.2 370	6 4748.54 38 17.23 22 4.40 9.69 0.9 2.46 0.17 0.4 0.3 371	7 25 4.12 38 22.16 22 1.58 8.78 0.3 2.42 0.08 0.2 0.1 372	7 55 7.39 38 22.38 21 59.64 8.57 0.5 2.20 0.04 0.2 0.2 373	9 343.44 38 22.47 22 0.18 7.92 0.9 0.00 0.12 0.4 0.5 375	9 1942.10 38 22.49 21 59.80 7.50 0.5 0.00 0.08 0.2 0.2 376	9 5045 48 38 21.98 22 1.46 8.38 0.3 2.32 0.09 0.2 0.2 377	9525667 382579 2149.06 9.13 0.5 2.14 0.09 0.3 0.4 378 11 45758 382756 215075 724 0.4 0.00 0.8 0.3 0.2 270	11 4-2.2.0 56 22.00 21 37.12 1.24 0.4 0.00 0.06 0.5 2.7 57 13 3555.73 38 14.45 22 7.25 7.58 0.5 2.52 0.11 0.3 0.2 380	13 3650.81 38 35.75 22 8.68 12.44 0.9 2.20 0.05 0.3 0.6 381	14 3244.75 38 14.73 22 6.22 7.40 0.4 2.69 0.12 0.2 0.2 382	15 3315.19 38 23.34 22 0.60 9.57 0.3 2.69 0.09 0.1 0.1 383 15 6467 03 38 23.01 21.48 24 8 17 03 2.66 0.10 0.7 0.7 284	15 3436.87 38 22.40 21 59.79 8.47 0.3 2.57 0.08 0.1 0.1 385	16 5828.49 38 18.26 22 10.03 6.13 0.5 2.35 0.10 0.6 0.5 386	17 335.74 38 16.70 22 1.15 7.77 0.5 2.39 0.15 0.4 0.3 387 17 813.00 38.00 1 25 85 0.08 0.6 2.57 0.17 0.3 0.2 388	17 1637.93 38 22.24 22 13.03 11.64 0.7 2.22 0.14 0.9 0.5 389	17 4130.22 38 22.49 21 59.63 8.13 0.3 2.20 0.06 0.2 0.2 390	18 2245.59 38 22.34 21 59.31 6.82 0.4 0.00 0.04 0.2 0.1 391	18 27 0.18 38 22.38 21 59.48 6.79 0.7 2.20 0.09 0.3 0.2 392	18 2829./1 38 20.34 22 9.42 0.40 0.3 2.22 0.08 0.2 0.3 393 19 051.69 38 20.92 22 9.58 6.78 0.3 2.60 0.13 0.3 0.2 394	20 1750.04 38 20.55 22 9.42 6.44 0.4 2.31 0.12 0.3 0.3 395	20 3945.11 38 20.65 22 9.30 6.22 0.4 2.28 0.11 0.3 0.3 396	20 5513.37 38 7.63 22 1.42 10.90 0.7 2.50 0.12 0.4 0.9 397	21 3925.45 38 26.67 21 54.91 9.56 0.3 2.37 0.08 0.2 0.2 398	22 035.12 38 22.65 21 59.82 7.45 0.5 2.34 0.12 0.3 0.3 399	22 1025.05 38 20.28 22 9.57 6.89 0.3 2.29 0.09 0.3 0.3 400	23 2320.24 38 33.03 21 52.88 17.28 0.4 2.11 0.05 0.5 1.1 401	23 2819.44 38 23.67 21 57.58 5.91 0.7 2.57 0.11 0.2 0.4 402	23 3532,51 38 22,46 21 59,87 8,50 0,4 2,84 0,14 0,2 0,1 403 23 42 2,80 38 22,29 22 0,06 8,00 0,7 2,44 0,14 0,3 0,4 404	0 525.03 38 22.52 21 59.73 7.46 0.6 0.00 0.08 0.2 0.3 405	0 29 2.50 38 20.55 22 9.56 6.88 0.2 2.38 0.09 0.3 0.3 406
te Time Lat Long Depth ERZ Mag. RMS ERX ERY n.evt   3812 0.451.66 38.22.38 2159.78 7.56 0.4 2.44 0.10 0.2 0.2 355   3812 0.4745.08 38.22.38 2159.77 8.55 0.3 2.59 0.11 0.1 0.1 356   3812 0.4745.08 38.22.38 2159.77 8.55 0.3 2.59 0.11 0.1 356   3812 0.756.56 38.15.65 22.5.66 8.00 0.4 2.38 0.08 0.3 0.2 357   3817 1.70.95 38.73 22.5.66 8.00 0.4 2.38 0.08 0.2 357	1012 12272 302223 2137.01 7.00 0.5 2.5 0.10 0.1 0.1 300 1012 1394415 382231 215975 7.78 0.4 2.42 0.11 0.1 0.2 359 1013 1487735 382237 31597 31504 311 0.1 0.1 250	012 1404/-0 36.22.20 21.37.50 0.1/ 0.2 204 0.11 0.1 0.1 0.1 300 1812 38.02.34 38.23.25 22.0.05 9.52 1.4 2.65 0.23 0.5 0.6 361 1813 3.3771 0.3 38.37.45 7.4 71.67.07 0.3 361	812 35345.19 38 13.15 22 3.40 9.47 0.6 2.54 0.16 0.3 0.3 363	812 4263.51 3822.16 2159.74 7.47 0.5 2.40 0.15 0.3 0.2 364	812 4 2/ 8.24 38 21:1/ 22 2.04 8.25 0.3 2.83 0.11 0.1 0.1 305 812 5 738.19 38 22.67 21 46.15 8.65 0.3 2.83 0.11 0.2 0.2 366	812 5 13 7.68 38 24.80 21 57.21 8.89 0.4 2.37 0.10 0.2 0.2 367	1812 5 2927.39 38 21.78 22 15.95 12.08 0.5 2.52 0.17 0.6 0.4 368 813 6 000 36 38 37 63 31 60 06 8 31 0 8 3 38 0 14 0 4 0 5 360	812 6 1351.81 38 22.44 21 55.72 8.05 0.3 2.37 0.13 0.2 0.2 370	812 64748.54 3817.23 22.4.40 9.69 0.9 2.46 0.17 0.4 0.3 371	812 7254.12 3822.16 22 1.58 8.78 0.3 2.42 0.08 0.2 0.1 372	812 7557.39 38 22.38 21 59.64 8.57 0.5 2.20 0.04 0.2 0.2 373	012 / JJ1/JJ J014.24 22 3.90 / 42 0.3 2.40 0.13 0.4 0.5 3/4 812 9 343.44 38 22.47 22 0.18 7.92 0.9 0.00 0.12 0.4 0.5 375	812 91942.10 38 22.49 21 59.80 7.50 0.5 0.00 0.08 0.2 0.2 376	812 9 5045.48 38 21.98 22 1.46 8.38 0.3 2.32 0.09 0.2 0.2 377	812 95256.67 3825.79 2149.06 9.13 0.5 2.14 0.09 0.3 0.4 378 813 11 457 58 3827 56 71 5675 724 0.4 0.00 0.8 0.3 0.7 370	812 13 355573 38 14.45 22 7.25 7.58 0.5 2.52 0.11 0.3 0.2 380	812 13 3650.81 38 35.75 22 8.68 12.44 0.9 2.20 0.05 0.3 0.6 381	812 14 3244.75 38 14.73 22 6.22 7.40 0.4 2.69 0.12 0.2 0.2 382	812 15 3315.19 38 23.34 22 0.60 9.57 0.3 2.69 0.09 0.1 0.1 383 213 15 5457 03 38 33 01 21 48 34 8 12 03 3 55 0.10 02 02 324	812 164436.87 3822.40 2159.79 8.47 0.3 2.57 0.08 0.1 0.1 385	812 16 5828.49 38 18.26 22 10.03 6.13 0.5 2.35 0.10 0.6 0.5 386	812 17 335.74 38 16.70 22 1.15 7.77 0.5 2.39 0.15 0.4 0.3 387 213 17 212.00 22 20.01 22 5 2 6 08 06 2 57 0.17 0.3 0.2 388	812 17 1637.93 38 22.24 22 13.03 11.64 0.7 2.22 0.14 0.9 0.5 389	812 17 4130.22 38 22.49 21 59.63 8.13 0.3 2.20 0.06 0.2 0.2 390	812 18 2245.59 38 22.34 21 59.31 6.82 0.4 0.00 0.04 0.2 0.1 391	812 18 27 0.18 38 22.38 21 59.48 6.79 0.7 2.20 0.09 0.3 0.2 392	812 18 2824/1 38 20.34 22 9.44 0.40 0.5 22 0.00 0.2 0.5 393 812 19 051.69 38 20.92 22 9.58 6.78 0.2 2.60 0.13 0.3 0.2 394	812 20 1750.04 38 20.55 22 9.42 6.44 0.4 2.31 0.12 0.3 0.3 395	312 20 3945.11 38 20.65 22 9.30 6.22 0.4 2.28 0.11 0.3 0.3 396	812 20 5513.37 38 7.63 22 1.42 10.90 0.7 2.50 0.12 0.4 0.9 397	812 21 3925.45 38 26.67 21 54.91 9.56 0.3 2.37 0.08 0.2 0.2 398	812 22 035.12 38 22.65 21 59.82 7.45 0.5 2.34 0.12 0.3 0.3 399	812 22 1025.05 38 20.28 22 9.57 6.89 0.3 2.29 0.09 0.3 0.3 400	812 23 2320.24 38 33.03 21 52.88 17.28 0.4 2.11 0.05 0.5 1.1 401	812 23 2819.44 38 23.67 21 57.58 5.91 0.7 2.57 0.11 0.2 0.4 402	812 23 3352.51 38 22.46 21 39.87 8.50 0.4 2.84 0.14 0.2 0.1 403 312 23 42 2.80 38 22.29 22 0.06 8.00 0.7 2.44 0.14 0.3 0.4 404	313 0 525.03 38 22.52 21 59.73 7.46 0.6 0.00 0.08 0.2 0.3 405	313 0 29 2.50 38 20.55 22 9.56 6.88 0.2 2.38 0.09 0.3 0.3 406

n.ev 519	22 22	222	523	22	526	528	529	530	5	233	534	535	537	538	£ 5	541	542	<b>5</b> 43	¥ 3	£ 5	55	548	550	221	223	554	556	557	558	60 G	20 20	562	563	<u>5</u>	565	267	568	§	22	1.6	575	576
ERY 0.2	22	6.6	0.5	3.5	1.9	10	0.2	0.3	0.1	0.3	0.4	0.1	0.2	0.6	6.0	0.2	0.2	0.4	0.3	0.2	0.1	0.3	0.2	0.2	0.3	0.2	0.3	0.2	0.5	0.5	0.2	0.2	0.2	0.3	0.4	0.3	0.4	0.2	0.7	6	9 7 7	0.5
ERX 0.3	50	0.4	8.0	20	1.4 4.0	3 8	0.2	0.3	5 2	04	0.4	0.1	0.3	0.0	6.0	0.3	0.2	0.3	0.3	070	0 4	0.3	0.2	6. 4. c	0.2	0.1	0.3	0.3	0.4	5 C	0 4	0.2	0.1	0.2	03	0.3	0.4 4 0	0.7	0.0	0.0	0.5	0.6
RMS 0.15	60 O	0.16	0.16	0.16	0.21	0.11	0.13	0.16	0.10	0.13	0.10	0.09	0.10	0.12	0.16	0.10	0.08	0.0	800	800	0.0	0.10	0.0	1.5	0.0	0.05	0.12	0.05	0.11	0.08	0.08	0.07	0.11	0.0	0.06	600	0.13	600	0.12	0.14	0.16	0.19
Mag. 2.39	8.8	0.0	2.50	231	2.35	2.43	2.47	2; 5 4 8	2 42 2 42	2.39	2.23	2.79	2.29	2.58	212	2.28	2.49	2.42	2.29	2.47	2.71	2.52	2;40 2;40	507	2.46	2.24	2.35	2.00	2.10	717	2.38	2.20	2.63	8.0	2.22	5; 5; 6; 7;	2.92	242	2.61	247	2.46 14	2.19
ERZ 0.4	0.6 0.6	0.8	9 9 0 0	6.0	2.2	0.0	0.3	0.6	3.5	4.0	0.6	0.2	0.6	80 0	0.7	0.7	0.2	0.4	0.0 4 v	50	0.6	0.5	0.4		50	0.2	0.4	0.3	0.7	0.4 0.6	0.3	0.2	0.4	0.5	0.4	0.8 0.8	0.4	0.3	0.0	4.0 4	0.7	0.8
Depth 7.34	6.47	5.84	6.36 e oe	8.9 9.9	6.66 6.97	6.46	8.10	7.43	049 049	14.32	4.87	7.53	6.58	2.02 2.02	6.25	10.82	9.08	9.10	8 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	8.27	8.25	10.89	7.63		12.33	8.20	7.87	9.49	8.32	18.30	11.26	10.29	9.51	8.35	17.29	6.76	22.04	4.70	7.28	775	7.54	6.43
0	5 G	41	5	13	76	3	28	е К	28	3 6	37	24	23	£ 5	: 22	3	5	ពុ	ci X	8 18	43	14	8,5	8 =	: ព	8	86	<b>7</b>	ត្ត៖	<u></u>	8	54	<b>S</b>	F. I	<u>.</u>	<b>.</b> 5	<del>4</del>	8 5	£. 4	<u></u> 19.03	38	56
Long 22 5.	21 48	21 48	21 49.	23.2	21 48	21 50	22 5.	22 4	21 54	22 11.	22 5.	22 5.	2	2 2	2 8	22 3.	22	22 12	21 12	21 51.	21 45.	22 16	21 52	1 5 5 5	21 52	22 3.	21 59.	22 9.	21 59	22 17	22 16	2144	21 59	21 55	21 51	21 59	21 45	22 3.	21 48	21.50	22 4	22 3.
56	76.	<del>9</del>	4 8	8	80 Q	5	.18	ភ្លូ ទ	2.6	18	8	8	<u>s</u> , ;	ನ ಕ	22	53	8	8, 8	2.3	ភ្	12	56	4	2 5	34	52	.67	8	<u>8</u> .8	2 8	5	<b>6</b> 3	5	<b>7</b> , 7	¥ 1	50	3	<u>-</u>	F, F	e 6	4	8
Lat 38 14		38 21.	38 14	38 16	38 18	38 20	38 14	38 14	38 26	38 24	38 22	38 17	38 13	38 13	38 18	38 19	38 20	38 21	38 20	38.25	38 18	38 20	38 22	38 20	38 29	38 21	38 22	38 22	38 21	38 19	38 22	38 23	38 24	38 25	38 33	38 22	38 0.	38 15	38 18	38 23	38 14	38 13
4.49	CE.V 0.81	6.60	5.55 0 0 0 0	9.66 9.66	1.45 0.86	4.56	90.1	7.22	47 II	12.04	48.82	44.56	0.10	20.10	36.17	7.72	9.85	15.30	57.48	27.15	7.69	0.98	0.57	16.1	9.54	9.12	2.89	17.22	29.55	16.02	5.45	113.25	15.99	141.53	15.12	58.54	6.27	5 08	5 5 5	9.78	1.46	8.65
Time 0 324	1 403 1 403	1 403	1431	3 491	3 50 4	4 475	7 13/	9 531	13.42	14 33	14 49	1626	1741	19 22	2010	21 35	21 39	21 56	22 33	1 R 2 R	1 121	1 361	3 522	4 4 4 7 4 4 4	6 424	9 32	9 16	10 26	10 5	21 21	13 33	14 24	1631	18 23	20 22	23 29	16 0	0 141	0 284		. 2 2	3 365
8	18	18	8 8	3 22	<u>81</u> 8	. 22	18	81 0	o 8	18	18	18	8	18	18	18	18	81 :	18	o 81	61	61	61	2 5	6	19	19	61	61 :	2 2	6	61	61	<u>6</u> :	61 9	61	នន	នុន	នុន	2 2	ເລ	50
Date 9108	8016 8016	9108	9108	9108	9108	9108	9108	9108	010	9108	9108	9108	9108	8019	9108	9108	9108	9108	8016	8016	9108	9108	9108	8016	6108	9108	9108	9108	9108	8016 8016	9108	9108	9108	9108	9108	9108 8016	8016	8016	9108	8016 8016	9108	9108
5	+ v		<b>~</b> a				5	<b>V</b> 0 F	- a			_	2	~ ~		9	~	~	<u>م</u> د		. 9	3	<b>.</b>	n v	0 F	~	6	0	_	~ ~	. 4	ŝ	Ś	~	•	0	_	2	<b>~</b> .		~ ~	
Y n.evt 463	4 8 8	466	467	8 69	471	473	475	476	478	479	480	481	482	483	485	486	487	488	489	64 164	492	493	494	495	464	498	499	200	201		5 S	505	206	20	203	510	511	512	513	514	516	517
X ERY n.evt 0.3 463	0.5 465	0.1 466	0.6 467 0.3 468	0.3 469	0.4 471 0.5 477	0.2 473	1 0.3 475	0.6 476	0.2 478	0.7 479	0.1 480	i 0.3 481	0.2 482	0.3 483	0.2 485	0.5 486	5 0.5 487	9 0.2 488	2 0.3 489	0.2 491	0.3 492	5 0.3 493	1 0.2 494	1 0.3 495	0.3 497	3 0.2 498	1 0.3 499	2 0.4 500	0.2 501	0.5 502 0.1 502	5 0.6 504	0.8 505	2 0.2 506	0.4 507	0.4 509	1 0.3 510	0.5 511	0.5 512	0.1 513	0.4 514	0.1 516	0.3 517
4S ERX ERY n.evt 3 0.2 0.3 463	2 0.6 0.5 465	3 0.1 0.1 466	5 0.6 0.6 467 0 03 03 468	6 0.3 0.3 469	0 0.6 0.4 471	9 0.3 0.2 473	4 0.4 0.3 475	0 0.3 0.6 476	0 0 0 0 0 478 0 478	4 0.5 0.7 479	2 0.1 0.1 480	6 0.5 0.3 481	5 0.2 0.2 482	(7 0.3 0.3 483 4 0.4 0.3 483	2 0.4 0.2 485	5 0.9 0.5 486	5 0.6 0.5 487	4 0.3 0.2 488	0.2 0.3 489 0 0.3 0.3 489	16 0.4 0.2 491	1 0.2 0.3 492	9 0.5 0.3 493	11 0.4 0.2 494	15 0.4 0.3 495 10 0.5 0.3 405	11 0.2 0.3 497	9 0.3 0.2 498	9 0.4 0.3 499	<b>)5 0.2 0.4 500</b>	<b>36 0.1 0.2 501</b>	11 0.3 0.5 502 10 0.7 0.1 503	14 0.5 0.6 504	18 1.0 0.8 505	11 0.2 0.2 506	7 0.3 0.4 507	4 0.4 0.4 509	1 0.4 0.3 510	8 0.5 0.5 511	6 0.7 0.5 512	6 0.2 0.1 513	0 0.5 0.4 514	7 0.1 0.1 516	9 0.2 0.3 517
RMS ERX ERY n.evt 2 0.13 0.2 0.3 463	9 0.12 0.6 0.4 404 2 0.15 0.6 0.5 465	3 0.03 0.1 0.1 466	12 0.15 0.6 0.6 467	0 0.06 0.3 0.3 469	5 0.10 0.6 0.4 471 0 0.73 0.4 0.5 477	3 0.19 0.3 0.2 473	19 0.14 0.4 0.3 475	77 0.10 0.3 0.6 476	2 0.13 0.3 0.3 4// 0 0 13 0 3 0 3 478	1 0.14 0.5 0.7 479	2 0.12 0.1 0.1 480	4 0.16 0.5 0.3 481	1 0.15 0.2 0.2 482	13 0.17 0.3 0.3 483	57 0.12 0.4 0.2 485	1 0.15 0.9 0.5 486	13 0.15 0.6 0.5 487	55 0.14 0.3 0.2 488	00 0.06 0.2 0.3 489	14 0.10 0.5 0.2 490	8 0.11 0.2 0.3 492	27 0.09 0.5 0.3 493	14 0.11 0.4 0.2 494	4 0.15 0.4 0.3 495 6 0.10 0.5 0.3 405	28 0.11 0.2 0.3 497	22 0.09 0.3 0.2 498	37 0.09 0.4 0.3 499	00 0.05 0.2 0.4 500	25 0.06 0.1 0.2 501	24 0.11 0.3 0.5 502	22 0.14 0.5 0.6 504	51 0.18 1.0 0.8 505	<b>15 0.11 0.2 0.2 506</b>	0 0.07 0.3 0.4 507	22 0.14 0.4 0.4 509	<b>7 0.11 0.4 0.3 510</b>	2 0.18 0.5 0.5 511	0 0.16 0.7 0.5 512		11 0.10 0.5 0.4 514 15 0.09 0.7 0.1 515	1 0.07 0.1 0.1 516	8 0.09 0.2 0.3 517
Z Mag. RMS ERX ERY n.evt 4 2.62 0.13 0.2 0.3 463	) 2.19 0.12 0.0 0.4 464 5 2.52 0.15 0.6 0.5 465	2 1.93 0.03 0.1 0.1 466	5 2.52 0.15 0.6 0.6 467	5 0.00 0.06 0.3 0.3 469	7 2.15 0.10 0.6 0.4 471 5 2.80 0.23 0.4 0.5 472	2 2.83 0.19 0.3 0.2 473	3 2.49 0.14 0.4 0.3 475	2.07 0.10 0.3 0.6 476	2 2.12 0.13 0.3 0.3 4// 7 3 47 0 13 0 3 0 0 478	8 2.21 0.14 0.5 0.7 479	4 2.92 0.12 0.1 0.1 480	5 2.74 0.16 0.5 0.3 481	3 2.81 0.15 0.2 0.2 482	5 2.33 0.17 0.3 0.3 483	5 2.57 0.12 0.4 0.2 485	5 2.11 0.15 0.9 0.5 486	9 2.43 0.15 0.6 0.5 487	4 2.55 0.14 0.3 0.2 488	3 0.00 0.06 0.2 0.3 489	2 2.44 0.10 0.5 0.2 450 1 2.86 0.16 0.4 0.2 491	5 2.08 0.11 0.2 0.3 492	3 2.27 0.09 0.5 0.3 493	5 2.34 0.11 0.4 0.2 494	7 2.44 0.15 0.4 0.3 495	4 2.28 0.11 0.2 0.3 497	4 2.22 0.09 0.3 0.2 498	4 2.37 0.09 0.4 0.3 499	3 0.00 0.05 0.2 0.4 500	2 2.25 0.06 0.1 0.2 501	8 2.24 0.11 0.3 0.5 502 5 2 7 010 0 2 0 1 503	0 2.22 0.14 0.5 0.6 504	2 2.51 0.18 1.0 0.8 505	5 2.35 0.11 0.2 0.2 506	4 2.30 0.07 0.3 0.4 507	5 2.22 0.14 0.4 0.4 509	5 2.07 0.11 0.4 0.3 510	2.32 0.18 0.5 0.5 511	0.00 0.16 0.7 0.5 512	2.80 0.06 0.2 0.1 513	0 2221 0.10 0.5 0.4 514 7 245 0.00 0.7 0.1 515	1 2.51 0.07 0.1 0.1 516	1 2.18 0.09 0.2 0.3 517
pth ERZ Mag. RMS ERY new 24 0.4 2.62 0.13 0.2 0.3 463	00 1.0 2.19 0.12 0.0 0.4 464 14 0.6 2.52 0.15 0.6 0.5 465	0 0.2 1.93 0.03 0.1 0.1 466	.73 0.6 2.52 0.15 0.6 0.6 467 53 0.6 2.21 0.10 0.3 0.3 468		53 0.7 2.15 0.10 0.6 0.4 471 55 0.6 280 0.73 0.4 0.5 472	[3 0.2 2.83 0.19 0.3 0.2 473	<b>99 0.8 2.49 0.14 0.4 0.3 475</b>	33 0.9 2.07 0.10 0.3 0.6 476	52 2.0 2.12 0.13 0.9 0.9 4// 78 0.7 3.47 0.13 0.7 0.3 478	.92 0.8 2.21 0.14 0.5 0.7 479	52 0.4 2.92 0.12 0.1 0.1 480	38 0.6 2.74 0.16 0.5 0.3 481	<b>32</b> 0.3 2.81 0.15 0.2 0.2 482	34 0.6 2.33 0.17 0.3 0.3 483 56 0.4 2.51 0.14 0.4 0.3 484	78 0.6 2.57 0.12 0.4 0.2 485	29 0.6 2.11 0.15 0.9 0.5 486	42 1.9 2.43 0.15 0.6 0.5 487	50 0.4 2.55 0.14 0.3 0.2 488	55 0.3 0.00 0.06 0.2 0.3 489 32 0.3 244 0.10 0.3 0.3 480	-22 0.3 2.44 0.10 0.3 0.2 490 79 0.4 2.86 0.16 0.4 0.2 491	<b>7</b> 0.6 2.08 0.11 0.2 0.3 492	73 0.8 2.27 0.09 0.5 0.3 493	<b>32 0.5 2.34 0.11 0.4 0.2 494</b>	28 0.7 2.44 0.15 0.4 0.3 495	47 0.4 2.28 0.11 0.2 0.3 497	30 0.4 2.22 0.09 0.3 0.2 498	14 0.4 2.37 0.09 0.4 0.3 499	58 0.3 0.00 0.05 0.2 0.4 500	23 0.2 2.25 0.06 0.1 0.2 501	37 0.8 2.24 0.11 0.3 0.5 502 11 0.3 3.73 0.10 0.3 0.1 503	17 1.0 2.22 0.14 0.5 0.6 504	33 1.2 2.51 0.18 1.0 0.8 505	31 0.6 2.35 0.11 0.2 0.2 506	26 0.4 2.30 0.07 0.3 0.4 507	99 0.6 2.22 0.14 0.4 0.4 509	72 0.5 2.07 0.11 0.4 0.3 510	76 1.2 2.32 0.18 0.5 0.5 511	00 1.3 0.00 0.16 0.7 0.5 512	57 0.1 2.80 0.06 0.2 0.1 513	22 0.5 221 0.10 0.5 0.4 514 0 04 245 008 02 01 515	3 0.3 2.51 0.07 0.1 0.1 516	4 0.4 2.18 0.09 0.2 0.3 517
Depth ERZ Mag RMS ERX ERY n.evt 7.24 0.4 2.62 0.13 0.2 0.3 463	6.00 1.0 2.19 0.12 0.0 0.4 464 9.14 0.6 2.52 0.15 0.6 0.5 465	9.00 0.2 1.93 0.03 0.1 0.1 466	23.73 0.6 2.52 0.15 0.6 0.6 467	8.15 0.5 0.00 0.06 0.3 0.3 469	9.53 0.7 2.15 0.10 0.6 0.4 471 7.5 0.6 780 0.73 0.4 0.5 477	7.13 0.2 2.83 0.19 0.3 0.2 473	6.99 0.8 2.49 0.14 0.4 0.3 475	8.33 0.9 2.07 0.10 0.3 0.6 476	78 0.7 7.40 0.10 0.10 0.2 0.2 0.7 0.7 471 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	10.92 0.8 2.21 0.14 0.5 0.7 479	9.62 0.4 2.92 0.12 0.1 0.1 480	9.38 0.6 2.74 0.16 0.5 0.3 481	8.02 0.3 2.81 0.15 0.2 0.2 482	8.34 0.6 2.33 0.17 0.3 0.3 483 8.05 0.4 2.51 0.14 0.4 0.3 483	7.78 0.6 2.57 0.12 0.4 0.2 485	12.29 0.6 2.11 0.15 0.9 0.5 486	8.42 1.9 2.43 0.15 0.6 0.5 487	7.60 0.4 2.55 0.14 0.3 0.2 488	6.65 0.3 0.00 0.06 0.2 0.3 489 12 22 03 244 010 0.3 02 400	8.79 0.4 2.86 0.16 0.4 0.2 490	9.97 0.6 2.08 0.11 0.2 0.3 492	8.73 0.8 2.27 0.09 0.5 0.3 493	7.92 0.5 2.34 0.11 0.4 0.2 494	8.28 0.7 2.44 0.15 0.4 0.3 495 574 0.5 2.54 0.10 0.5 0.2 405	5.74 0.5 2.04 0.15 0.5 0.5 490 12.47 0.4 2.28 0.11 0.2 0.3 497	7.80 0.4 2.22 0.09 0.3 0.2 498	8.14 0.4 2.37 0.09 0.4 0.3 499	8.68 0.3 0.00 0.05 0.2 0.4 500	12.23 0.2 2.25 0.06 0.1 0.2 501	8.37 0.8 2.24 0.11 0.3 0.5 502 8.11 0.2 2.72 0.10 0.2 0.1 503	5.17 1.0 2.22 0.14 0.5 0.6 504	6.33 1.2 2.51 0.18 1.0 0.8 505	9.31 0.6 2.35 0.11 0.2 0.2 506	6.26 0.4 2.30 0.07 0.3 0.4 507	6.99 0.6 2.22 0.14 0.4 0.4 509	6.72 0.5 2.07 0.11 0.4 0.3 510	8.76 1.2 2.32 0.18 0.5 0.5 511	10.00 1.3 0.00 0.16 0.7 0.5 512	6.67 0.1 2.80 0.06 0.2 0.1 513	14.22 0.5 2.21 0.10 0.5 0.4 514 0.30 0.4 2.45 0.00 0.2 0.1 515	8.63 0.3 2.51 0.07 0.1 0.1 516	8.14 0.4 2.18 0.09 0.2 0.3 517
ng Depth ERZ Mag. RMS ERX ERY n.evt 55.48 7.24 0.4 2.62 0.13 0.2 0.3 463	2.5.12 6.00 1.0 2.19 0.12 0.6 0.4 404 2.11.97 9.14 0.6 2.52 0.15 0.6 0.5 465	54.94 9.00 0.2 1.93 0.03 0.1 0.1 466	46.97 23.73 0.6 2.52 0.15 0.6 0.6 467	49.01 8.15 0.5 0.00 0.06 0.3 0.3 469	19.22 9.53 0.7 2.15 0.10 0.6 0.4 471   \$144 7.75 0.6 7.80 0.73 0.4 0.5 477	5.53 7.13 0.2 2.83 0.19 0.3 0.2 473	. 4.81 6.99 0.8 2.49 0.14 0.4 0.3 475	59.70 8.33 0.9 2.07 0.10 0.3 0.6 476	114 C.D 2.D CI.D 21.2 D.Z C2.1 14.8 C 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	51.75 10.92 0.8 2.21 0.14 0.5 0.7 479	59.93 9.62 0.4 2.92 0.12 0.1 0.1 480	45.59 9.38 0.6 2.74 0.16 0.5 0.3 481	5.80 8.02 0.3 2.81 0.15 0.2 0.2 482	5.90 8.34 0.6 2.33 0.17 0.3 0.3 483	5.27 7.78 0.6 2.57 0.12 0.4 0.2 485	13.32 12.29 0.6 2.11 0.15 0.9 0.5 486	2.79 8.42 1.9 2.43 0.15 0.6 0.5 487	7.29 7.60 0.4 2.55 0.14 0.3 0.2 488	51.85 6.65 0.3 0.00 0.06 0.2 0.3 489 14 81 13 23 0.3 244 0.10 0.3 0.3 400	48.90 8.79 0.4 2.86 0.16 0.4 0.2 490	57.40 9.97 0.6 2.08 0.11 0.2 0.3 492	: 6.01 8.73 0.8 2.27 0.09 0.5 0.3 493	6.19 7.92 0.5 2.34 0.11 0.4 0.2 494	5.22 8.28 0.7 2.44 0.15 0.4 0.3 495	2.04 12.47 0.4 2.28 0.11 0.2 0.3 497	. 6.47 7.80 0.4 2.22 0.09 0.3 0.2 498	2. 7.55 8.14 0.4 2.37 0.09 0.4 0.3 499	3.45 8.68 0.3 0.00 0.05 0.2 0.4 500	7.28 12.23 0.2 2.25 0.06 0.1 0.2 501	34.42 8.37 0.8 2.24 0.11 0.3 0.5 502 10.85 8.11 0.3 3.72 0.10 0.3 0.1 503	3.49 5.17 1.0 2.22 0.14 0.5 0.6 504	4.74 6.33 1.2 2.51 0.18 1.0 0.8 505	58.04 9.31 0.6 2.35 0.11 0.2 0.2 506	5.17 6.26 0.4 2.30 0.07 0.3 0.4 507	5.04 6.99 0.6 2.22 0.14 0.4 0.4 509	5.33 6.72 0.5 2.07 0.11 0.4 0.3 510	5.04 8.76 1.2 2.32 0.18 0.5 0.5 511	3.40 10.00 1.3 0.00 0.16 0.7 0.5 512	48.57 6.67 0.1 2.80 0.06 0.2 0.1 513	11.4/ 14.22 0.3 2.21 0.10 0.3 0.4 514 1.68 0.30 0.4 7.45 0.00 0.7 0.1 515	57.55 8.63 0.3 2.51 0.07 0.1 0.1 516	53.56 8.14 0.4 2.18 0.09 0.2 0.3 517
Long Depth ERZ Mag. RMS ERX ERY n.evt 21 55.48 7.24 0.4 2.62 0.13 0.2 0.3 463	22 5.12 6.00 1.0 2.19 0.12 0.6 0.4 404 22 11.97 9.14 0.6 2.52 0.15 0.6 0.5 465	21 54.94 9.00 0.2 1.93 0.03 0.1 0.1 466	21 46.97 23.73 0.6 2.52 0.15 0.6 0.6 467 22 4.7 5 53 05 221 0.10 03 03 458	21 49.01 8.15 0.5 0.00 0.06 0.3 0.3 469	22 9.22 9.53 0.7 2.15 0.10 0.6 0.4 471 21 51 44 7.75 0.5 780 0.73 0.4 0.5 477	22 5.53 7.13 0.2 2.83 0.19 0.3 0.2 473	22 4.81 6.99 0.8 2.49 0.14 0.4 0.3 475	21 59.70 8.33 0.9 2.07 0.10 0.3 0.6 476	717 C.D. C.D. C1.0, C1.2, C.Z. C.D. C.2, C.C.2, C.C	21 51.75 10.92 0.8 2.21 0.14 0.5 0.7 479	21 59.93 9.62 0.4 2.92 0.12 0.1 0.1 480	21 45.59 9.38 0.6 2.74 0.16 0.5 0.3 481	22 5.80 8.02 0.3 2.81 0.15 0.2 0.2 482	22 5.90 8.34 0.6 2.33 0.17 0.3 0.3 483 22 5.00 8.05 0.4 2.51 0.14 0.4 0.3 484	22 5.27 7.78 0.6 2.57 0.12 0.4 0.2 485	22 13.32 12.29 0.6 2.11 0.15 0.9 0.5 486	22 2.79 8.42 1.9 2.43 0.15 0.6 0.5 487	22 7.29 7.60 0.4 2.55 0.14 0.3 0.2 488	21 51.85 6.65 0.3 0.00 0.06 0.2 0.3 489	21 13.61 12.22 0.3 2.44 0.10 0.3 0.4 430 21 48.90 8.79 0.4 2.86 0.16 0.4 0.2 491	21 57.40 9.97 0.6 2.08 0.11 0.2 0.3 492	22 6.01 8.73 0.8 2.27 0.09 0.5 0.3 493	22 6.19 7.92 0.5 2.34 0.11 0.4 0.2 494	22 6.22 8.28 0.7 2.44 0.10 0.4 0.3 495	22 2.64 12.47 0.4 2.28 0.11 0.2 0.3 497	22 6.47 7.80 0.4 2.22 0.09 0.3 0.2 498	22 7.55 8.14 0.4 2.37 0.09 0.4 0.3 499	22 3.45 8.68 0.3 0.00 0.05 0.2 0.4 500	22 7.28 12.23 0.2 2.25 0.06 0.1 0.2 501	21 54.42 8.37 0.8 2.24 0.11 0.3 0.5 502 22 10 85 8 11 0 2 2 72 0 10 0 2 0 1 503	22 3.49 5.17 1.0 2.22 0.14 0.5 0.6 504	22 4.74 6.33 1.2 2.51 0.18 1.0 0.8 505	21 58.04 9.31 0.6 2.35 0.11 0.2 0.2 506	22 5.17 6.26 0.4 2.30 0.07 0.3 0.4 507	22 5.04 6.99 0.6 2.22 0.14 0.4 0.4 509	22 5.33 6.72 0.5 2.07 0.11 0.4 0.3 510	22 5.04 8.76 1.2 2.32 0.18 0.5 0.5 511	22 3.40 10.00 1.3 0.00 0.16 0.7 0.5 512	21 48.57 6.67 0.1 2.80 0.06 0.2 0.1 513	22 11.4/ 14.22 0.3 2.21 0.10 0.5 0.4 514 22 168 030 04 245 0.00 07 01 515	21 7.55 8.63 0.3 2.51 0.07 0.1 0.1 516	21 53.56 8.14 0.4 2.18 0.09 0.2 0.3 517
ut Long Depth ERZ Mag. RMS ERX ERY n.evt 3 13.78 21 55.48 7.24 0.4 2.62 0.13 0.2 0.3 463	8 14.23 22 5.12 6.00 1.0 2.19 0.12 0.0 0.4 404 3 23 06 22 11.97 9.14 0.6 2.52 0.15 0.6 0.5 465	3 26.88 21 54.94 9.00 0.2 1.93 0.03 0.1 0.1 466	3 8.37 21 46.97 23.73 0.6 2.52 0.15 0.6 0.6 467	3 25.69 21 49.01 8.15 0.5 0.00 0.06 0.3 0.3 469	321.82 22.9.22 9.53 0.7 2.15 0.10 0.6 0.4 471	3 17.01 22 5.53 7.13 0.2 2.83 0.19 0.3 0.2 473	3 14.34 22 4.81 6.99 0.8 2.49 0.14 0.4 0.3 475	3 23.22 21 59.70 8.33 0.9 2.07 0.10 0.3 0.6 476	174 C.0 6.0 CI.0 71.7 0.7 C.9. 1.9. 0.2 0.2 4.1 1.1 1.2 0.2 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1	3 29.40 21 51.75 10.92 0.8 2.21 0.14 0.5 0.7 479	323.70 21 59.93 9.62 0.4 2.92 0.12 0.1 0.1 480	3 23.14 21 45.59 9.38 0.6 2.74 0.16 0.5 0.3 481	3 14.25 22 5.80 8.02 0.3 2.81 0.15 0.2 0.2 482	3 14.25 22 5.90 8.34 0.6 2.33 0.17 0.3 0.3 483	3 17.08 22 5.27 7.78 0.6 2.57 0.12 0.4 0.2 485	3 22.65 22 13.32 12.29 0.6 2.11 0.15 0.9 0.5 486	3 17.83 22 2.79 8.42 1.9 2.43 0.15 0.6 0.5 487	3 14.15 22 7.29 7.60 0.4 2.55 0.14 0.3 0.2 488	3 22.88 21 51.85 6.65 0.3 0.00 0.06 0.2 0.3 489	2 21:40	3 24.87 21 57.40 9.97 0.6 2.08 0.11 0.2 0.3 492	8 14.70 22 6.01 8.73 0.8 2.27 0.09 0.5 0.3 493	3 14.85 22 6.19 7.92 0.5 2.34 0.11 0.4 0.2 494	8 14.87 22 6.22 8.28 0.7 2.44 0.15 0.4 0.3 495	3 25.11 22 2.64 12.47 0.4 2.28 0.11 0.2 0.3 490	3 14.68 22 6.47 7.80 0.4 2.22 0.09 0.3 0.2 498	3 14.13 22 7.55 8.14 0.4 2.37 0.09 0.4 0.3 499	3 20.00 22 3.45 8.68 0.3 0.00 0.05 0.2 0.4 500	3 24.66 22 7.28 12.23 0.2 2.25 0.06 0.1 0.2 501	527.16 21 34.42 8.37 0.8 2.24 0.11 0.3 0.5 502 21818 22 10.85 811 0.2 2.72 0.10 0.2 0.1 502	3 12.98 22 3.49 5.17 1.0 2.22 0.14 0.5 0.6 504	3 13.52 22 4.74 6.33 1.2 2.51 0.18 1.0 0.8 505	3 24.36 21 58.04 9.31 0.6 2.35 0.11 0.2 0.2 506	13.56 22 5.17 6.26 0.4 2.30 0.07 0.3 0.4 507	14.24 22 5.04 6.99 0.6 2.22 0.14 0.4 0.4 509	14.15 22 5.33 6.72 0.5 2.07 0.11 0.4 0.3 510	113.77 22 5.04 8.76 1.2 2.32 0.18 0.5 0.5 511	19.77 22 3.40 10.00 1.3 0.00 0.16 0.7 0.5 512	14.08 21 48.57 6.67 0.1 2.80 0.06 0.2 0.1 513	124.42 2211.4/ 14.22 0.3 2.21 0.10 0.3 0.4 514 123.09 22168 030 0.4 2.45 0.09 0.2 0.1 515	123.44 21 57.55 8.63 0.3 2.51 0.07 0.1 0.1 516	24.67 21 53.56 8.14 0.4 2.18 0.09 0.2 0.3 517
Lat Long Depth ERZ Mag. RMS ERX ERY n.evt 8 38 13.78 21 55.48 7.24 0.4 2.62 0.13 0.2 0.3 463	1 38 14.23 22 5.12 6.00 1.0 2.19 0.12 0.0 0.4 404 5 38 23.06 22 11.97 9.14 0.6 2.52 0.15 0.6 0.5 465	9 38 26.88 21 54.94 9.00 0.2 1.93 0.03 0.1 0.1 466	9 38 8.37 21 46.97 23.73 0.6 2.52 0.15 0.6 0.6 467	40 38 13.24 24 4.47 3.03 0.5 24 4.10 0.3 0.3 469 05 38 25.69 21 49.01 8.15 0.5 0.00 0.06 0.3 0.3 469	10 38 21.82 22 9.22 9.53 0.7 2.15 0.10 0.6 0.4 471	81 38 17.01 22 5.53 7.13 0.2 2.83 0.19 0.3 0.2 473	57 38 14.34 22 4.81 6.99 0.8 2.49 0.14 0.4 0.3 475	05 38 23.22 21 59.70 8.33 0.9 2.07 0.10 0.3 0.6 476	() 38 (3.84 22 8.41 / .85 2.0 2.12 0.10 1.9 0.9 47 47 47 12 0.2 47 47 47 12 12 12 12 12 12 12 12 12 12 12 12 12	75 38 29.40 21 51.75 10.92 0.8 2.21 0.14 0.5 0.7 479	14 38 23.70 21 59.93 9.62 0.4 2.92 0.12 0.1 0.1 480	30 38 23.14 21 45.59 9.38 0.6 2.74 0.16 0.5 0.3 481	7 38 14.25 22 5.80 8.02 0.3 2.81 0.15 0.2 0.2 482	9 38 14.25 22 5.90 8.34 0.6 2.33 0.17 0.3 0.3 483	<b>1</b> 38 17.08 22 5.27 7.78 0.6 2.57 0.12 0.4 0.2 485	0 38 22.65 22 13.32 12.29 0.6 2.11 0.15 0.9 0.5 486	1 38 17.83 22 2.79 8.42 1.9 2.43 0.15 0.6 0.5 487	7 38 14.15 22 7.29 7.60 0.4 2.55 0.14 0.3 0.2 488	2 38 22.88 21 51.85 6.65 0.3 0.00 0.06 0.2 0.3 489	80 36 21:40 24 13:61 12:22 0.3 2:44 0.10 0.3 0.2 430 38 38 24 54 21 48:90 8.79 0.4 2.86 0.16 0.4 0.2 491	57 38 24.87 21 57.40 9.97 0.6 2.08 0.11 0.2 0.3 492	3 38 14.70 22 6.01 8.73 0.8 2.27 0.09 0.5 0.3 493	8 38 14.85 22 6.19 7.92 0.5 2.34 0.11 0.4 0.2 494	9 38 14.87 22 6.22 8.28 0.7 2.44 0.15 0.4 0.3 495	7 38 25.11 22 2.64 12.47 0.4 2.28 0.11 0.2 0.3 490	9 38 14.68 22 6.47 7.80 0.4 2.22 0.09 0.3 0.2 498	5 38 14.13 22 7.55 8.14 0.4 2.37 0.09 0.4 0.3 499	3 38 20.00 22 3.45 8.68 0.3 0.00 0.05 0.2 0.4 500	38 24 66 22 7.28 12.23 0.2 2.25 0.06 0.1 0.2 501	8 38 27.16 21 34.42 8.37 0.8 2.24 0.11 0.3 0.5 502 1 38 18 18 27 10 85 8 11 0.2 272 0 10 0.2 0 1 602	6 3812.98 22 3.49 5.17 1.0 2.22 0.14 0.5 0.6 504	35 38 13.52 22 4.74 6.33 1.2 2.51 0.18 1.0 0.8 505	7 38 24.36 21 58.04 9.31 0.6 2.35 0.11 0.2 0.2 506	3 38 13.56 22 5.17 6.26 0.4 2.30 0.07 0.3 0.4 507	34 38 14:24 22 5.04 6.99 0.6 2.22 0.14 0.4 0.4 509	43 38 14.15 22 5.33 6.72 0.5 2.07 0.11 0.4 0.3 510	35 38 13.77 22 5.04 8.76 1.2 2.32 0.18 0.5 0.5 511	5 38 19.77 22 3.40 10.00 1.3 0.00 0.16 0.7 0.5 512	0 38 14.08 21 48.57 6.67 0.1 2.80 0.06 0.2 0.1 513	0/ 38 24:42 22 11:4/ 14:22 0.5 2.21 0.10 0.5 0.4 514 0 38 27 09 22 168 030 04 245 009 02 01 515	20 20 20 22 4 21 57.55 8.63 0.3 2.51 0.07 0.1 0.1 516	37 38 24.67 21 53.56 8.14 0.4 2.18 0.09 0.2 0.3 517
ine Lat Long Depth ERZ Mag. RMS ERX ERY n.evt 4952.98 38 13.78 21 55.48 7.24 0.4 2.62 0.13 0.2 0.3 463	:5934.01 38 14.23 22 5.12 6.00 1.0 2.19 0.12 0.0 0.4 404 5112 25 38 23.06 22 11.97 9.14 0.6 2.52 0.15 0.6 0.5 465	1951.39 38 26.88 21 54.94 9.00 0.2 1.93 0.03 0.1 0.1 466	01245.19 38 8.37 21 46.97 23.73 0.6 2.52 0.15 0.6 0.6 467	05/20/40 38 15/32 22 4/47 5/03 0.3 2/41 0/10 0.3 0.3 469 05141.05 38 25:69 21 49.01 8.15 0.5 0.00 0.06 0.3 0.3 469	3 447.40 38 21.82 22 9.22 9.53 0.7 2.15 0.10 0.6 0.4 471	5 3935,81 38 17.01 22 5.53 7.13 0.2 2.83 0.19 0.3 0.2 473	5 55 1.57 38 14.34 22 4.81 6.99 0.8 2.49 0.14 0.4 0.3 475	7 11 0.05 38 23.22 21 59.70 8.33 0.9 2.07 0.10 0.3 0.6 476	844.2.19 58.12.84 22 8.41 7.85 2.0 2.12 0.13 0.9 0.9 417 417 7 47 0.7 0.7 1.7 0.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1	2 1218.75 38 29.40 21 51.75 10.92 0.8 2.21 0.14 0.5 0.7 479	3 042 44 38 23.70 21 59.93 9.62 0.4 2.92 0.12 0.1 480	3 5317.30 38 23.14 21 45.59 9.38 0.6 2.74 0.16 0.5 0.3 481	4340.27 38 14.25 22 5.80 8.02 0.3 2.81 0.15 0.2 0.2 482	5611.99 38 14.25 22 5.90 8.34 0.6 2.33 0.17 0.3 0.3 483 5051 20 38 14.18 22 5.00 8.54 0.6 2.33 0.17 0.3 0.3 483	736.44 38.17.08 22.5.27 7.78 0.6 2.57 0.12 0.4 0.2 485	564.10 38 22.65 22 13.32 12.29 0.6 2.11 0.15 0.9 0.5 486	191.54 3817.83 22 2.79 8.42 1.9 2.43 0.15 0.6 0.5 487	4325.37 38 14.15 22 7.29 7.60 0.4 2.55 0.14 0.3 0.2 488	5026.32 38 22.88 21 51.85 6.65 0.3 0.00 0.06 0.2 0.3 489 8 10 8 44 28 21 44 21 15 81 12 22 0.3 2 44 0 10 0.3 0.3 400	8 1 8 8 40 38 21 40 22 13.81 12.22 0.3 2.44 0.10 0.3 0.2 4 90 9 5 4 5 3 3 8 2 4 5 4 2 1 4 8 90 8 7 9 0 4 2 8 6 0 1 6 0 4 0 2 4 9 1	3 737.57 38 24.87 21 57.40 9.97 0.6 2.08 0.11 0.2 0.3 492	3025.43 38 14.70 22 6.01 8.73 0.8 2.27 0.09 0.5 0.3 493	(3733.18 38 14.85 22 6.19 7.92 0.5 2.34 0.11 0.4 0.2 494	14710.39 3814.87 22 6.22 8.28 0.7 2.44 0.15 0.4 0.3 495 5315 31 3818 58 2310 53 5 74 5 5 7 54 510 5 5 5 3 405	0210.04 00 16.06 22 10.00 0.14 0.0 2.04 0.17 0.0 0.0 490 5250.67 38 25.11 22 2.64 12.47 0.4 2.28 0.11 0.2 0.3 497	<i>5747.59</i> 38 14.68 22 6.47 7.80 0.4 2.22 0.09 0.3 0.2 498	2146.75 38 14.13 22 7.55 8.14 0.4 2.37 0.09 0.4 0.3 499	4844.93 38 20.00 22 3.45 8.68 0.3 0.00 0.05 0.2 0.4 500	543.01 38 24.66 22 7.28 12.23 0.2 2.25 0.06 0.1 0.2 501	1339,38 38 27.16 21 34.42 8.37 0.8 2.24 0.11 0.3 0.5 502 2010 71 38 18 18 27 10 85 8 11 0.7 272 0.10 0.7 0.1 603	1 925.36 38 12.98 22 3.49 5.17 1.0 2.22 0.14 0.5 0.6 504	4 4327.35 38 13.52 22 4.74 6.33 1.2 2.51 0.18 1.0 0.8 505	4 57 7.17 38 24.36 21 58.04 9.31 0.6 2.35 0.11 0.2 0.2 506	5 20 5.23 38 13.56 22 5.17 6.26 0.4 2.30 0.07 0.3 0.4 507	7 3618.34 38 14.24 22 5.04 6.99 0.6 2.22 0.14 0.4 0.4 509	7 3631.43 38 14.15 22 5.33 6.72 0.5 2.07 0.11 0.4 0.3 510	7 3840.35 38 13.77 22 5.04 8.76 1.2 2.32 0.18 0.5 0.5 511	9 1 2.95 38 19.77 22 3.40 10.00 1.3 0.00 0.16 0.7 0.5 512	0 925.00 38 14.08 21 48.57 6.67 0.1 2.80 0.06 0.2 0.1 513	01112.5/ 38.24.42 22.11.4/ 14.22.0.3 22.1 0.10 0.5 0.4 514 1840.20 38.27.00 22 168 0.30 0.4 2.45 0.00 0.7 0.1 515	1 3718.01 38 23.44 21 57.55 8.63 0.3 2.51 0.07 0.1 0.1 516	3 2429.87 38 24.67 21 53.56 8.14 0.4 2.18 0.09 0.2 0.3 517
Time Lat Long Depth ERZ Mag. RMS ERX ERY n.evt   5 4952.98 38 13.78 21 55.48 7.24 0.4 2.62 0.13 0.3 463	5 5934,01 38 14.23 22 5.12 6.00 1.0 2.19 0.12 0.6 0.4 404 6 5112 25 38 23.06 22 11.97 9.14 0.6 2.52 0.15 0.6 0.5 465	7 1951.39 38 26.88 21 54.94 9.00 0.2 1.93 0.03 0.1 0.1 466	8 1245.19 38 8.37 21 46.97 23.73 0.6 2.52 0.15 0.6 0.6 467	10 3/20.40 38 13.26 21 49.01 8.15 0.5 0.00 0.06 0.3 0.3 469	13 447.40 38 21.82 22 9.22 9.53 0.7 2.15 0.10 0.6 0.4 471	15 3935,81 38 17.01 22 5.53 7.13 0.2 2.83 0.19 0.3 0.2 473	15 55 1.57 38 14.34 22 4.81 6.99 0.8 2.49 0.14 0.4 0.3 475	17110.05 3823.22 2159.70 8.33 0.9 2.07 0.10 0.3 0.6 476	18 44 5.19 58 15.84 24 8.41 7.55 2.0 2.12 0.12 0.9 49 41 41 12 12 12 12 12 12 12 12 12 12 12 12 12	22 1218.75 38 29.40 21 51.75 10.92 0.8 2.21 0.14 0.5 0.7 479	23 042.44 38 23.70 21 59.93 9.62 0.4 2.92 0.12 0.1 0.1 480	23 5317.30 38 23.14 21 45.59 9.38 0.6 2.74 0.16 0.5 0.3 481	1 4340.27 38 14.25 22 5.80 8.02 0.3 2.81 0.15 0.2 0.2 482	1 5611.99 38 14.25 22 5.90 8.34 0.6 2.33 0.17 0.3 0.3 483	2 736 44 38 17.08 22 5.27 7.78 0.6 2.57 0.12 0.4 0.2 485	3564.10 38 22.65 22 13.32 12.29 0.6 2.11 0.15 0.9 0.5 486	6 19 1.54 38 17.83 22 2.79 8.42 1.9 2.43 0.15 0.6 0.5 487	6 4325.37 38 14.15 22 7.29 7.60 0.4 2.55 0.14 0.3 0.2 488	7 5026.32 38 22.88 21 51.85 6.65 0.3 0.00 0.06 0.2 0.3 489	16 19 6.40 36 21.40 24 13.61 12.22 0.3 2.44 0.10 0.3 0.2 430 19 5453 38 38 24 54 21 48.90 8.79 0.4 2.86 0.16 0.4 0.2 491	23 737.57 38 24.87 21 57.40 9.97 0.6 2.08 0.11 0.2 0.3 492	0 3025.43 38 14.70 22 6.01 8.73 0.8 2.27 0.09 0.5 0.3 493	03733.18 3814.85 22 6.19 7.92 0.5 2.34 0.11 0.4 0.2 494	04710.39 3814.87 22 6.22 8.28 0.7 2.44 0.15 0.4 0.3 495 05314 2819 59 22 10 52 574 0 5 2 54 0 50 0 5 0 2 405	0.5250.67 38.25.11 22.2.64 12.47 0.4 2.28 0.11 0.2 0.3 490	0 5747.59 38 14.68 22 6.47 7.80 0.4 2.22 0.09 0.3 0.2 498	1 2146.75 38 14.13 22 7.55 8.14 0.4 2.37 0.09 0.4 0.3 499	i 4844.93 38 20.00 22 3.45 8.68 0.3 0.00 0.05 0.2 0.4 500	3 543.01 38 24.66 22 7.28 12.23 0.2 2.25 0.06 0.1 0.2 501	5 1359.58 38 27.16 21 34.42 8.37 0.8 2.24 0.11 0.3 0.5 502 0 2010 71 38 18 18 22 10 85 8 11 0 2 2 72 0 10 0 2 0 1 603	11 925.36 38 12.98 22 3.49 5.17 1.0 2.22 0.14 0.5 0.6 504	14 4327.35 38 13.52 22 4.74 6.33 1.2 2.51 0.18 1.0 0.8 505	14 57 7.17 38 24.36 21 58.04 9.31 0.6 2.35 0.11 0.2 0.2 506	15 20 5.23 38 13.56 22 5.17 6.26 0.4 2.30 0.07 0.3 0.4 507	17 3618.34 38 14.24 22 5.04 6.99 0.6 2.22 0.14 0.4 0.4 509	17 3631.43 38 14.15 22 5.33 6.72 0.5 2.07 0.11 0.4 0.3 510	17 3840.35 38 13.77 22 5.04 8.76 1.2 2.32 0.18 0.5 0.5 511	19 12.95 38 19.77 22 3.40 10.00 1.3 0.00 0.16 0.7 0.5 512	20 925.00 38 14.08 21 48.57 6.67 0.1 2.80 0.06 0.2 0.1 513	20 1112.2/ 38 24.42 22 11.4/ 14.22 0.3 2.21 0.10 0.3 0.4 514 21 849.20 38.27.09 22 1.68 0.30 0.4 2.45 0.06 0.2 0.3 515	21 3718.01 38 23.44 21 57.55 8.63 0.3 2.51 0.07 0.1 0.1 516	23 2429.87 38 24.67 21 53.56 8.14 0.4 2.18 0.09 0.2 0.3 517
Date Time Lat Long Depth ERZ Mag. RMS ERX ERY n.evt   910815 5 4952.98 38 13.78 21 55 48 7.24 0.4 2.62 0.13 0.2 0.3 463	910815 55934.01 38 14.23 22 5.12 6.00 1.0 2.19 0.12 0.6 0.4 404 310815 6511225 38 23.06 22 11.97 9.14 0.6 2.52 0.15 0.6 0.5 465	910815 7 1951.39 38 26.88 21 54.94 9.00 0.2 1.93 0.03 0.1 0.1 466	910815 8 1245.19 38 8.37 21 46.97 23.73 0.6 2.52 0.15 0.6 0.6 467	910815 10.5140105 38.25.69 21.49.01 8.15 0.5 0.00 0.06 0.3 0.3 469	910815 13 447.40 38 21.82 22 9.22 9.53 0.7 2.15 0.10 0.6 0.4 471		910815 15 55 1.57 38 14.34 22 4.81 6.99 0.8 2.49 0.14 0.4 0.3 475	910815 17110.05 38 23.22 21 59.70 8.33 0.9 2.07 0.10 0.3 0.6 476	910815 18 44 5.19 58 15.84 22 8.41 1.55 2.0 2.12 0.12 0.9 4.7 4/1 11/01/4 70 7/1 38 74 77 71 67 4/7 0 78 0/7 7 4/2 0/17 0/7 0/7 4/78	910815 22 1218.75 38 29.40 21 51.75 10.92 0.8 2.21 0.14 0.5 0.7 479	910815 23 042.44 38 23.70 21 59.93 9.62 0.4 2.92 0.12 0.1 0.1 480	910815 23 5317.30 38 23.14 21 45.59 9.38 0.6 2.74 0.16 0.5 0.3 481	910816 1 4340.27 38 14.25 22 5.80 8.02 0.3 2.81 0.15 0.2 0.2 482	910816 15611.99 38 14.25 22 5.90 8.34 0.6 2.33 0.17 0.3 0.3 483	210610 1.2221.24 38.17.08 22.5.27 7.78 0.6 2.57 0.12 0.4 0.2 485	010816 3 56 4.10 38 22.65 22 13.32 12.29 0.6 2.11 0.15 0.9 0.5 486	910816 6191.54 3817.83 22.2.79 8.42 1.9 2.43 0.15 0.6 0.5 487	910816 6 4325.37 38 14.15 22 7.29 7.60 0.4 2.55 0.14 0.3 0.2 488	910816 7 5026.32 38 22.88 21 51.85 6.65 0.3 0.00 0.06 0.2 0.3 489	910810 18 19 8:40 38 21:40 22 13:61 12:22 0.3 2:44 0.10 0.3 0.2 430 110816 19 5453 38 38 24 54 21 48,90 8.79 0.4 2.86 0.16 0.4 0.2 491	010816 23 737.57 38 24.87 21 57.40 9.97 0.6 2.08 0.11 0.2 0.3 492	10817 03025.43 38 14.70 22 6.01 8.73 0.8 2.27 0.09 0.5 0.3 493	10817 03733.18 38 14.85 22 6.19 7.92 0.5 2.34 0.11 0.4 0.2 494	010817 04710.39 3814.87 22 6.22 8.28 0.7 2.44 0.15 0.4 0.3 495	1061/ 0.3210.34 36 16.36 22 10.63 3.14 0.5 2.64 0.3 430 10817 0.5250.67 38 25.11 22 2.64 12.47 0.4 2.28 0.11 0.2 0.3 497	0.0817 05747.59 38 14.68 22 6.47 7.80 0.4 2.22 0.09 0.3 0.2 498	10817 1 2146.75 38 14.13 22 7.55 8.14 0.4 2.37 0.09 0.4 0.3 499	10817 I 4844.93 38 20.00 22 3.45 8.68 0.3 0.00 0.05 0.2 0.4 500	10817 3 543.01 38 24.66 22 7.28 12.23 0.2 2.25 0.06 0.1 0.2 501	10817 51359.58 3827.16 2154.42 8.37 0.8 2.24 0.11 0.3 0.5 502 10817 0.01071 381818 221085 811 0.3 272 0.10 0.3 01 503	10817 11 925.36 38 12.98 22 3.49 5.17 1.0 2.22 0.14 0.5 0.6 504	10817 14 4327.35 38 13.52 22 4.74 6.33 1.2 2.51 0.18 1.0 0.8 505	0817 14 57 7.17 38 24.36 21 58.04 9.31 0.6 2.35 0.11 0.2 0.2 506	10817 15 20 5.23 38 13.56 22 5.17 6.26 0.4 2.30 0.07 0.3 0.4 507	010817 17 3618.34 38 14.24 22 5.04 6.99 0.6 2.22 0.14 0.4 0.4 509	010817 17 3631.43 38 14.15 22 5.33 6.72 0.5 2.07 0.11 0.4 0.3 510	10817 17 3840.35 38 13.77 22 5.04 8.76 1.2 2.32 0.18 0.5 0.5 511	010817 19 1 2.95 38 19.77 22 3.40 10.00 1.3 0.00 0.16 0.7 0.5 512	10817 20 925.00 38 14.08 21 48.57 6.67 0.1 2.80 0.06 0.2 0.1 513	1081/ 2011112.2/ 38 24:42 22 11:47 14:22 0.5 2:21 0.10 0.5 0.4 514 10817 21 849.20 38 27:09 22 1:68 0.30 0.4 2.45 0.09 0.5 0.5 1:5	10817 21 3718.01 38 23.44 21 57.55 8.63 0.3 2.51 0.07 0.1 0.1 516	10817 23 2429.87 38 24.67 21 53.56 8.14 0.4 2.18 0.09 0.2 0.3 517

n.evt 630 631 633 633 634 636 636	633 639 640	643 643	89 89 89 89 89	<b>2</b> 2	650	652	62 <del>1</del>	655 656	657 658	629	662 662	88 88 88	665	88	699	0 <u>7</u> 0	672	674 675	676	677	8/0	680	681	682	683 684	685
ERY 0.5 0.3 0.3 0.3 0.3 0.4	0 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	0.3 0.1 0.1	0.2 0.4 0.2	0.2	0.2	0.3	0.5	0.3 0.2	0.3	0.2	0.3	0.3	0.2	c. 0 S: 0	0.3	0.6	0.4	0.1	03	0.1	4.0	3	0.6	0.2	0.2	0.4
ERX 0.6 0.1 0.1 0.3 0.3 0.3	0 7 7 0 7 0 7 0 7	0.3 0.3 0.1	0.3 0.4 0.2	0.2	0.3	0.5		07 07	0.3	0.2	0.2	0.3	0.3	0.0 0.0	0.2	0.3 0.3	0.2	0.3	0.4	0.1	70	0.2	0.3	0.1	0.2	0.2
RMS 0.15 0.08 0.08 0.08 0.14 0.18	0.11 0.07 0.13 0.13	0.09 0.10	0.14 0.13 0.08	0.07	0.06	0.16	ci .0	0.15	0.13	0.13	0.05	0.12	0.13	0.10	0.10	60 0 0 08	0.09	0.13	0.12	0.11	61.0 6	0.13	0.14	0.10	0.09	0.11
Mag. 2.46 2.33 2.72 2.14 2.14 2.14 2.27	2.74 2.74 2.69 2.63	2.17 2.48 2.53	2.85 2.21 2.22	2.21	2.52	2.52	1.99	233 223	2.54 2.46	2.48	507	2.16 2.39	2.79	2.19 2.19	2.25	2.39	2.54	2.42	2.38	3.00	65.2	5.49	2.43	2.7	252	2.23
ERZ 0.9 0.2 0.4 0.5 0.5	0.4 0.4	0.3	0.3 1.1 0.3	0.5	4.0	50	0.7	0.5	0.4	0.5	0.3	0.9	0.4	3 1	0.6	0.5	0.6	0.4	0.7	0.4	× ×	0.6	1.0	0.4	0.5	0.9
Depth 5.49 5.90 5.90 10.02 7.02 6.50	10.52 9.70 8.26 7.54	9.69 9.97 9.55	7.77 9.67 8.45	5.91	1.71	8	c1./	9.09 8.07	6.99 5.40	7.74	07.7 97.7	9.04 8.61	8.88	8.40	9.59	19.72	9.44	8.04 7.01	6.19	66.6	8'.8 0 10	9.27	10.25	9.22	9.08 9.38	9.00
4 ° ° ° ° 4 ° ° °	8 E <b>3</b> 8	2 % 4	65-		22	105	55	8 ∞	92	∞ ⊆	2 22	8 8	23	20	=	2 5	8	4 (1	9	<u>s</u> :	2 2	12		= >	<b>e</b> 9	6
Long 22 8.3 22 8.1 22 8.1 21 49.0 21 57.6 21 55.5 22 3.6 22 8.0	21 48.5 21 48.5 21 50.5 21 50.5 21 47.5	21 59.6 22 12.6 22 0.1	21 48. 21 59.6 22 1.0	22 8.3 22 6.4	21 47.0 22 10.0	22 9.8	21 4/.2	21 60.( 22 0.3	22 8.1 22 16.3	22 6.5	21 48.(	21 59.5	21 47.5	22 6.3	21 57.3	21 20. 21 56.3	21 56.0	27 7 8 27 6 0	22 6.4	21 57.8	27C 17	21 57.9	21 57.6	21 57.8	21 57.5	21 57.4
8869883	****	\$ % <del>-</del>	8 G G	8 5	8 2	5	8 8	8 X	ន្តត	22 2	2 œ	8 12	81	2 2	<u> </u>	2 2	=	e ک ک	8	8	= S	1 2	2	5 9	2 22	5
Lat 38 14.0 38 14.0 38 17.5 38 24.0 38 24.0 38 24.0 38 24.0	38 26.0 38 25.9 38 22 38 22 38 17.	38 21. 38 20. 38 24.	38 21. 38 22.0 38 22.0	38 21.3 38 14 6	38 17.38	38 18.	38 17.3 38 23.0	38 23. 38 22.	38 14. 38 25.	38 14.	38 23.	38 22. 38 24.	38 23.	38 15.	38 24.1	38 36.	38 24.	38 18.0 38 14.0	38 13.9	38 24.	38 24 0	38 25.0	38 25.4	38 24.	38 24.	38 24.3
4.61 4.61 4.7 4.7 4.1 6.5 6.5 99	8 1 8 8	48 8.95 4.41	5.97 5.97	2.02	3.24	5.71	0.10	3.98	8.00 5.87	8.37	o 61.	6 E	.14	8. 8.	8	<del>5</del> 5	()	5 <del>1</del> 2	9.51	5.88	60. F	ÌŢ	9.13	<b>.</b> 82	.97 1.87	2.27
Time 23 591 0 1610 0 2355 1 3112 3 3732 3 4751 3 5756	4 2819 4 2820 8 3418 9 1218	9 32 7. 12 162 12 194	12 22 14 52 14 21	15 543 16 41	16 192 17 161	17 252	21 204	21 405 21 492	22 504 23 55	23 334	0 5025	1 101 1	1 3645	4 3614 7 3713	7 3858	7 4722	8 2830	10471	11 191	16 472	10 483	17 24	17 24	17 439	17 221	17 223
							2 0	~ ~			~ ~	~ ~	~ ~		~		~		-	-			-	-		-
Date 910821 910822 910822 910822 910822 910822 910822	91082 91082 91082 91082	91082 91082 91082	910822 910822 910822	91082	91082	91082	91082	91082 91082	91082	91082	91082	91082	91082	91082	91082	91082	91082	91082	91082	910823	910825	910823	910823	910823	910823	910823
n.evt 577 578 578 580 581 583 583	584 585 587 587	588 589 590	593 593	595 595	596 597	865	66 69	8 8 8	<u>ş</u> §	<b>8</b>	808	609 910	611	613	614	616 616	617	618 619	620	621	770	55	625	626	021 628	629
ERY 1evt 0.2 577 0.4 578 0.1 579 0.1 579 0.1 581 0.1 581 0.1 583	0.3 584 0.2 585 0.4 586 0.1 587	0.2 588 0.2 589 0.2 590	0.3 591 0.2 592 1.1 593	0.6 594 0.3 595	0.2 596	0.4 598	0.3 600	0.2 602 0.3 603	0.2 604 0.3 605	0.2 606	0.4 608	0.2 609 0.3 610	0.3 611	0.6 613	0.2 614	0.2 616 0.2 616	0.1 617	0.1 618 0.3 619	0.4 620	0.2 621	779 7.0	0.3 624	0.1 625	0.3 626	0.3 628	0.3 629
ERX ERY n.evt 0.2 0.2 577 0.4 0.4 578 0.1 0.1 579 0.2 0.5 580 0.2 0.1 581 0.4 0.7 582 0.2 0.1 583	0.4 0.3 584 0.2 0.2 585 0.3 0.4 586 0.2 0.1 587	0.2 0.2 588 0.3 0.2 589 0.3 0.2 590	0.3 0.3 591 0.2 0.2 592 0.8 1.1 593	0.7 0.6 594 0.6 0.3 595	0.2 0.2 596	0.4 0.4 598	0.3 0.3 600	0.2 0.2 602 0.4 0.3 603	0.2 0.2 604 0.3 0.3 605	0.2 0.2 606	0.3 0.4 608	0.1 0.2 609 0.4 0.3 610	0.2 0.3 611	0.5 0.6 613	0.1 0.2 614	0.3 0.4 015 0.2 0.2 616	0.1 0.1 617	0.1 0.1 618 0.3 0.3 619	0.3 0.4 620	0.4 0.2 621	779 7.0 670 10 10 10	0.3 0.3 624	0.1 0.1 625	0.3 0.3 626	0.2 0.3 628	0.3 0.3 629
RMS ERX ERY n.evt   0.04 0.2 0.2 577   0.15 0.4 0.4 578   0.11 0.1 0.1 579   0.12 0.2 0.5 580   0.12 0.2 0.5 580   0.07 0.2 0.1 581   0.09 0.4 0.7 581   0.09 0.4 0.7 581   0.09 0.4 0.7 581	0.10 0.4 0.3 584 0.19 0.2 0.2 585 0.07 0.3 0.4 586 0.06 0.2 0.1 587	0.05 0.2 0.2 588   0.16 0.3 0.2 589   0.11 0.3 0.2 589	0.07 0.3 0.3 591 0.10 0.2 0.2 592 0.14 0.8 1.1 593	0.23 0.7 0.6 594 0.13 0.6 0.3 595	0.11 0.2 0.2 596 0.18 0.2 0.3 597	0.13 0.4 0.4 598	0.10 0.3 0.3 600	0.10 0.2 0.2 602 0.11 0.4 0.3 603	0.11 0.2 0.2 604 0.11 0.3 0.3 605	0.13 0.2 0.2 606	0.08 0.3 0.4 608	0.11 0.1 0.2 609 0.14 0.4 0.3 610	0.14 0.2 0.3 611	0.09 0.5 0.6 613	0.04 0.1 0.2 614	0.13 0.3 0.4 015 0.13 0.2 0.2 616	0.07 0.1 0.1 617	0.06 0.1 0.1 618 0.08 0.3 0.3 619	0.16 0.3 0.4 620	0.15 0.4 0.2 621	0.11 0.5 0.2 022	0.15 0.3 0.3 624	0.09 0.1 0.1 625	0.07 0.3 0.3 626	0.12 0.2 0.3 628	0.08 0.3 0.3 629
Mag. RMS ERX ERY Levt   2.47 0.04 0.2 0.2 577   2.30 0.15 0.4 0.4 578   2.34 0.11 0.1 0.1 579   2.37 0.15 0.4 0.4 578   2.37 0.10 0.1 0.1 579   2.37 0.10 0.1 0.1 579   2.37 0.10 0.1 0.1 579   2.37 0.07 0.2 0.5 580   2.53 0.07 0.2 0.1 581   2.11 0.09 0.4 0.7 582   2.53 0.07 0.2 0.1 581   2.53 0.07 0.2 0.1 582   2.53 0.09 0.2 0.1 583	2.27 0.10 0.4 0.3 584 2.75 0.19 0.2 0.2 585 2.43 0.07 0.3 0.4 586 2.63 0.06 0.2 0.1 587	2.40 0.05 0.2 0.2 588   2.61 0.16 0.3 0.2 589   2.27 0.11 0.3 0.2 590	0.00 0.07 0.3 0.3 591 2.13 0.10 0.2 0.2 592 0.00 0.14 0.8 1.1 593	2.36 0.23 0.7 0.6 594 2.33 0.13 0.6 0.3 595	2.47 0.11 0.2 0.2 596 2.45 0.18 0.2 0.3 597	2.21 0.13 0.4 0.4 598	1.8/ 0.02 0.2 0.2 0.2 999 2.30 0.10 0.3 0.3 600	2.39 0.10 0.2 0.2 602 2.45 0.11 0.4 0.3 603	2.36 0.11 0.2 0.2 604 2.19 0.11 0.3 0.3 605	2.53 0.13 0.2 0.2 606 0.00 0.07 0.2 0.2 606	2.23 0.08 0.3 0.4 608	2.58 0.11 0.1 0.2 609 2.43 0.14 0.4 0.3 610	2.45 0.14 0.2 0.3 611	2.47 0.09 0.5 0.6 613	2.11 0.04 0.1 0.2 614	2.34 0.13 0.3 0.4 015 2.35 0.13 0.2 0.2 616	2.49 0.07 0.1 0.1 617	2.28 0.06 0.1 0.1 618 2.25 0.08 0.3 0.3 619	2.48 0.16 0.3 0.4 620	2.65 0.15 0.4 0.2 621	2.24 0.11 0.3 0.2 0.22 2.64 0.10 0.1 0.1 6.23	2.23 0.15 0.3 0.3 624	2.63 0.09 0.1 0.1 625	2.18 0.07 0.3 0.3 626	2.31 0.12 0.2 0.3 628	2.35 0.08 0.3 0.3 629
ERZ Mag. RMS ERX ERY n.evt   0.2 2.47 0.04 0.2 0.2 577   0.6 2.30 0.15 0.4 0.4 578   0.6 2.30 0.15 0.4 0.4 578   0.2 2.34 0.11 0.1 0.1 579   0.2 2.34 0.11 0.1 0.1 579   0.2 2.34 0.11 0.1 0.1 579   0.5 2.37 0.12 0.2 0.5 580   0.2 2.53 0.07 0.2 0.1 581   0.2 2.53 0.07 0.2 0.1 581   0.1 2.11 0.09 0.4 0.7 582   0.3 2.52 0.09 0.2 0.1 583	0.5 2.27 0.10 0.4 0.3 584 0.3 2.75 0.19 0.2 0.2 585 0.4 2.43 0.07 0.3 0.4 586 0.2 2.63 0.06 0.2 0.1 587	0.2 2.40 0.05 0.2 588   0.5 2.61 0.16 0.3 0.2 589   0.5 2.27 0.11 0.3 0.2 589	0.5 0.00 0.07 0.3 0.3 591 0.5 2.13 0.10 0.2 0.2 592 1.9 0.00 0.14 0.8 1.1 593	1.3 2.36 0.23 0.7 0.6 594 0.7 2.33 0.13 0.6 0.3 595	0.4 2.47 0.11 0.2 0.2 596 0.5 2.45 0.18 0.2 0.3 597	0.6 2.21 0.13 0.4 0.4 598	0.2 1.8/ 0.02 0.2 0.2 599 0.3 2.30 0.10 0.3 0.3 600	0.3 2.39 0.10 0.2 0.2 602 0.7 2.45 0.11 0.4 0.3 603	0.5 2.36 0.11 0.2 0.2 604 0.6 2.19 0.11 0.3 0.3 605	0.4 2.53 0.13 0.2 0.2 606	0.4 2.23 0.08 0.3 0.4 608	0.4 2.58 0.11 0.1 0.2 609 0.7 2.43 0.14 0.4 0.3 610	0.5 2.45 0.14 0.2 0.3 611	0.7 2.47 0.09 0.5 0.6 613	0.4 2.11 0.04 0.1 0.2 614	0.6 2.34 0.13 0.3 0.4 015 0.4 2.35 0.13 0.2 0.2 616	0.2 2.49 0.07 0.1 0.1 617	0.3 2.28 0.06 0.1 0.1 618 0.4 2.25 0.08 0.3 0.3 619	0.5 2.48 0.16 0.3 0.4 620	0.5 2.65 0.15 0.4 0.2 621	0.8 2.24 0.11 0.3 0.2 0.22 0.3 2.64 0.10 0.1 0.1 623	0.5 2.23 0.15 0.3 0.3 624	0.3 2.63 0.09 0.1 0.1 625	0.4 2.18 0.07 0.3 0.3 626	0.3 2.31 0.12 0.2 0.3 628	0.4 2.35 0.08 0.3 0.3 629
Depth ERZ Mag. RMS ERY Levt   11.12 0.2 2.47 0.04 0.2 0.2 577   7.20 0.6 2.30 0.15 0.4 0.4 578   7.20 0.6 2.30 0.15 0.4 0.4 578   7.00 0.2 2.84 0.11 0.1 0.1 579   7.00 0.2 2.84 0.11 0.1 0.1 579   7.16 0.2 2.53 0.07 0.2 0.5 580   7.16 0.2 2.53 0.07 0.2 0.1 581   8.01 0.3 2.52 0.07 0.2 0.1 581	9.02 0.5 2.27 0.10 0.4 0.3 584 8.04 0.3 2.75 0.19 0.2 0.2 585 6.33 0.4 2.43 0.07 0.3 0.4 586 7.04 0.2 2.63 0.06 0.2 0.1 587	10.31 0.2 2.40 0.05 0.2 588   8.43 0.5 2.61 0.16 0.3 0.2 589   7.49 0.5 2.27 0.11 0.3 0.2 590	9.08 0.5 0.00 0.07 0.3 0.3 591 9.20 0.5 2.13 0.10 0.2 0.2 592 13.95 1.9 0.00 0.14 0.8 1.1 593	4.36 1.3 2.36 0.23 0.7 0.6 594 7.57 0.7 2.33 0.13 0.6 0.3 595	8.21 0.4 2.47 0.11 0.2 0.2 596 9.77 0.5 2.45 0.18 0.2 0.3 597	<b>6.64</b> 0.6 2.21 0.13 0.4 0.4 598	0.93 0.2 1.87 0.02 0.2 0.2 0.2 599 7.16 0.3 2.30 0.10 0.3 0.3 600	7.46 0.3 2.39 0.10 0.2 0.2 602 5.55 0.7 2.45 0.11 0.4 0.3 603	9.24 0.5 2.36 0.11 0.2 0.2 604 8.98 0.6 2.19 0.11 0.3 0.3 605	9.22 0.4 2.53 0.13 0.2 0.2 606	8.67 0.4 2.23 0.08 0.3 0.4 608	9.04 0.4 2.58 0.11 0.1 0.2 609 8.26 0.7 2.43 0.14 0.4 0.3 610	7.69 0.5 2.45 0.14 0.2 0.3 611	9.33 0.7 2.47 0.09 0.5 0.6 613	7.46 0.4 2.11 0.04 0.1 0.2 614	8.42 0.6 2.34 0.13 0.3 0.4 015 9.22 0.4 2.35 0.13 0.2 0.2 616	8.54 0.2 2.49 0.07 0.1 0.1 617	9.01 0.3 2.28 0.06 0.1 0.1 618 11.13 0.4 2.25 0.08 0.3 0.3 619	8.85 0.5 2.48 0.16 0.3 0.4 620	9.28 0.5 2.65 0.15 0.4 0.2 621	0.33 U.8 2.24 U.II U.3 U.2 022 033 D.3 264 D1D D1 D1 623	7.71 0.5 2.23 0.15 0.3 0.3 624	8.26 0.3 2.63 0.09 0.1 0.1 625	7.98 0.4 2.18 0.07 0.3 0.3 626	3.98 0.3 2.31 0.12 0.2 0.3 628	12.36 0.4 2.35 0.08 0.3 0.3 629
Depth ERZ Mag. RMS ERY newt   97 11.12 0.2 2.47 0.04 0.2 0.2 577   13 7.20 0.6 2.30 0.15 0.4 0.4 578   37 7.00 0.5 2.34 0.01 0.1 0.1 579   37 7.00 0.2 2.84 0.11 0.1 0.1 579   11 13.19 0.5 2.37 0.12 0.2 0.5 580   11 7.16 0.2 2.53 0.07 0.2 0.1 581   11 7.16 0.2 2.53 0.07 0.2 0.1 581   11 7.16 0.2 2.53 0.07 0.2 0.1 581   11 7.16 0.2 2.53 0.07 0.2 0.1 581   8.01 0.3 2.52 0.09 0.2 0.1 583	40 9.02 0.5 2.27 0.10 0.4 0.3 584   15 8.04 0.3 2.75 0.19 0.2 0.2 585   05 6.33 0.4 2.43 0.07 0.3 0.4 586   05 6.33 0.4 2.43 0.07 0.3 0.4 586   05 7.04 0.2 2.63 0.06 0.2 0.1 587	88 10.31 0.2 2.40 0.05 0.2 0.2 588 77 8.43 0.5 2.61 0.16 0.3 0.2 589 98 7.49 0.5 2.27 0.11 0.3 0.2 590	00 9.08 0.5 0.00 0.07 0.3 0.3 591 66 9.20 0.5 2.13 0.10 0.2 0.2 592 59 13.95 1.9 0.00 0.14 0.8 1.1 593	17 4.36 1.3 2.36 0.23 0.7 0.6 594 44 7.57 0.7 2.33 0.13 0.6 0.3 595	20 8.21 0.4 2.47 0.11 0.2 0.2 596 50 9.77 0.5 245 0.18 0.2 0.3 597	54 6.64 0.6 2.21 0.13 0.4 0.4 598	01 6.95 0.2 1.87 0.02 0.2 0.2 599 92 7.16 0.3 2.30 0.10 0.3 0.3 600	39 7.46 0.3 2.39 0.10 0.2 0.2 602 50 5.55 0.7 2.45 0.11 0.4 0.3 603	81 9.24 0.5 2.36 0.11 0.2 0.2 604 65 8.98 0.6 2.19 0.11 0.3 0.3 605	90 9.22 0.4 2.53 0.13 0.2 0.2 606	95 8.67 0.4 2.23 0.08 0.3 0.4 608	92 9.04 0.4 2.58 0.11 0.1 0.2 609 18 8.26 0.7 2.43 0.14 0.4 0.3 610	63 7.69 0.5 2.45 0.14 0.2 0.3 611	240 C.O. C.O. 0.16 U.J. C.O. 0.2 U.Z. 74 9.33 0.7 2.47 0.09 0.5 0.6 613	76 7.46 0.4 2.11 0.04 0.1 0.2 614	27 8.42 0.6 2.34 0.13 0.3 0.4 615 75 9.22 0.4 2.35 0.13 0.2 0.2 616	04 8.54 0.2 2.49 0.07 0.1 0.1 617	21 9.01 0.3 2.28 0.06 0.1 0.1 618 14 11.13 0.4 2.25 0.08 0.3 0.3 619	14 8.85 0.5 2.48 0.16 0.3 0.4 620	46 9.28 0.5 2.65 0.15 0.4 0.2 621	10 0.33 0.8 2.24 0.11 0.3 0.2 0.22 83 0.33 0.3 7.64 0.10 0.1 0.1 673	77 7.71 0.5 2.23 0.15 0.3 0.3 624	9 8.26 0.3 2.63 0.09 0.1 0.1 625	43 7.98 0.4 2.18 0.07 0.3 0.3 626	00 1.04 0.4 1.90 0.10 0.2 0.3 0.2/ 09 3.98 0.3 2.31 0.12 0.2 0.3 628	i5 12.36 0.4 2.35 0.08 0.3 0.3 629
Long Depth ERZ Mag. RMS ERY newt   221137 11.12 0.2 2.47 0.04 0.2 0.2 577   22 4.13 7.20 0.6 2.30 0.15 0.4 0.4 578   22 3.37 7.00 0.2 2.84 0.11 0.1 0.1 579   22 3.37 7.00 0.2 2.84 0.11 0.1 0.1 579   22 3.51 13.19 0.5 2.37 0.12 0.2 0.5 580   22 3.71 7.16 0.2 2.53 0.07 0.2 0.5 580   22 3.71 7.16 0.2 2.53 0.07 0.2 0.1 581   22 3.85 10.3 2.52 0.09 0.2 0.1 583   22 3.85 8.01 0.3 2.52 0.09 0.2 0.1 583   22	21 58.40 9.02 0.5 2.27 0.10 0.4 0.3 584 22 3.15 8.04 0.3 2.75 0.19 0.2 0.2 585 22 4.05 6.33 0.4 2.43 0.07 0.3 0.4 586 22 3.35 7.04 0.2 2.63 0.06 0.2 0.1 587	21 44.88 10.31 0.2 2.40 0.05 0.2 0.2 588   22 4.97 8.43 0.5 2.61 0.16 0.3 0.2 589   22 5.98 7.49 0.5 2.27 0.11 0.3 0.2 589	22 0.30 9.08 0.5 0.00 0.07 0.3 0.3 591 21 57.66 9.20 0.5 2.13 0.10 0.2 0.2 592 22 5.69 13.95 1.9 0.00 0.14 0.8 1.1 593	22 6.17 4.36 1.3 2.36 0.23 0.7 0.6 594 22 3.54 7.57 0.7 2.33 0.13 0.6 0.3 595	215920 8.21 0.4 2.47 0.11 0.2 0.2 596 215950 9.77 0.5 245 0.18 0.2 0.3 597	22 4.64 6.64 0.6 2.21 0.13 0.4 0.4 598	21 50.01 6.95 0.2 1.87 0.02 0.2 0.2 599 21 59.92 7.16 0.3 2.30 0.10 0.3 0.3 600	21 53.39 7.46 0.3 2.39 0.10 0.2 0.2 602 22 5.50 5.55 0.7 2.45 0.11 0.4 0.3 603	21 57.81 9.24 0.5 2.36 0.11 0.2 0.2 604 21 57.65 8.98 0.6 2.19 0.11 0.3 0.3 605	21 57.90 9.22 0.4 2.53 0.13 0.2 0.2 606 22 0.45 0.7 0.00 0.7 0.2 0.7 00	22 12.95 8.67 0.4 2.23 0.08 0.3 0.4 608	21 55.92 9.04 0.4 2.58 0.11 0.1 0.2 609 22 0.48 8.26 0.7 2.43 0.14 0.4 0.3 610	21 59.63 7.69 0.5 2.45 0.14 0.2 0.3 611	21 30.30 10.34 0.3 2.46 0.16 0.3 0.5 0.6 613 22 9.74 9.33 0.7 2.47 0.09 0.5 0.6 613	21 51.76 7.46 0.4 2.11 0.04 0.1 0.2 614	21 59.57 8.42 0.6 2.34 0.13 0.3 0.4 015 21 59.75 9.22 0.4 2.35 0.13 0.2 0.2 616	22 4.04 8.54 0.2 2.49 0.07 0.1 0.1 617	22 4.21 9.01 0.3 2.28 0.06 0.1 0.1 618 22 10.14 11.13 0.4 2.25 0.08 0.3 0.3 619	22 0.14 8.85 0.5 2.48 0.16 0.3 0.4 620	21 44.46 9.28 0.5 2.65 0.15 0.4 0.2 621	21 39.10 0.35 0.8 2.24 0.11 0.5 0.20 22 21 40 83 0 33 0 3 2 44 0 10 0 1 0 1 673	22 4.97 7.71 0.5 2.23 0.15 0.3 0.3 624	22 2.09 8.26 0.3 2.63 0.09 0.1 0.1 625	21 49.43 7.98 0.4 2.18 0.07 0.3 0.3 626	22 5.59 3.98 0.3 2.31 0.12 0.2 0.3 628	22 4.45 12.36 0.4 2.35 0.08 0.3 0.3 629
Long Depth ERZ Mag. RMS ERY newt   79 2211297 11.12 0.2 2.47 0.04 0.2 0.2 577   54 22 4.13 7.20 0.6 2.30 0.15 0.4 0.2 577   55 22 3.37 7.00 0.2 2.84 0.11 0.1 0.1 579   46 22 3.11 13.19 0.5 2.37 0.12 0.2 0.5 580   91 22 3.71 7.16 0.2 2.53 0.07 0.2 0.5 580   91 22 3.37 7.16 0.2 2.53 0.07 0.2 0.5 580   31 22 4.45 11.54 10 2.11 0.09 0.4 07 582   331 22 3.85 0.07 0.2 0.0 583 582	74 21 58.40 9.02 0.5 2.27 0.10 0.4 0.3 584   75 22 3.15 8.04 0.3 2.75 0.19 0.2 0.2 585   05 22 4.05 6.33 0.4 2.43 0.07 0.3 0.4 586   94 22 3.35 7.04 0.2 263 0.06 0.2 0.1 587	53 21 44.88 10.31 0.2 2.40 0.05 0.2 0.2 588   21 22 4.97 8.43 0.5 2.61 0.16 0.3 0.2 589   02 22 5.98 7.49 0.5 2.27 0.11 0.3 0.2 589	87 22 0.30 9.08 0.5 0.00 0.07 0.3 0.3 591 86 21 57,66 9.20 0.5 2.13 0.10 0.2 0.2 592 64 22 5,69 13.95 1.9 0.00 0.14 0.8 1.1 593	74 22 6.17 4.36 1.3 2.36 0.23 0.7 0.6 594 81 22 3.54 7.57 0.7 2.33 0.13 0.6 0.3 595	00 2159.20 8.21 0.4 2.47 0.11 0.2 596   95 2156.50 8.27 0.5 2.45 0.18 0.2 596	<b>34 22 4.64 6.64 0.6 2.21 0.13 0.4 0.4 598</b>	// 21 20.01 6.93 0.2 1.8/ 0.02 0.2 0.2 599 58 21 59.92 7.16 0.3 2.30 0.10 0.3 0.3 600	19 21 53.39 7.46 0.3 2.39 0.10 0.2 0.2 602 26 22 5.50 5.55 0.7 2.45 0.11 0.4 0.3 603	53 21 57.81 9.24 0.5 2.36 0.11 0.2 0.2 604 53 21 57.65 8.98 0.6 2.19 0.11 0.3 0.3 605	46 21 57,90 9.22 0.4 2.53 0.13 0.2 0.2 606 24 21 0.2 0.4 0.7 0.00 0.7 0.2 0.2 606	74 22 12.95 8.67 0.4 2.23 0.08 0.3 0.4 608	12 21 55.92 9.04 0.4 2.58 0.11 0.1 0.2 609 74 22 0.48 8.26 0.7 2.43 0.14 0.4 0.3 610	08 21 59.63 7.69 0.5 2.45 0.14 0.2 0.3 611	21 22 9.74 9.33 0.7 2.47 0.09 0.5 0.6 613	<b>32</b> 21 51.76 7.46 0.4 2.11 0.04 0.1 0.2 614	18 21 39.57 8.42 0.6 2.34 0.13 0.3 0.4 015 66 21 59.75 9.22 0.4 2.35 0.13 0.2 0.2 616	94 22 4.04 8.54 0.2 2.49 0.07 0.1 0.1 617	03 22 4.21 9.01 0.3 2.28 0.06 0.1 0.1 618 43 22 10.14 11.13 0.4 2.25 0.08 0.3 0.3 619	06 22 0.14 8.85 0.5 2.48 0.16 0.3 0.4 620	86 21 44.46 9.28 0.5 2.65 0.15 0.4 0.2 621	00 21 29.10 0.35 0.8 2.24 0.11 0.5 0.2 022 77 21 50 83 0 33 0 3 2 64 0 10 0 1 0 1 623	39 22 4.97 7.71 0.5 2.23 0.15 0.3 0.3 624	12 22 2.09 8.26 0.3 2.63 0.09 0.1 0.1 625	58 21 49.43 7.98 0.4 2.18 0.07 0.3 0.3 626	5 21 46.65 7.54 0.4 1.90 0.00 0.5 0.5 627 50 22 5.59 3.98 0.3 2.31 0.12 0.2 0.3 628	51 22 4.45 12.36 0.4 2.35 0.08 0.3 0.3 629
Lat Long Depth ERZ Mag. RMS ERY newt   38 21.79 22 11.297 11.12 0.2 2.47 0.04 0.2 577   38 21.79 22 11.37 11.12 0.2 2.47 0.04 0.2 577   38 14.54 22 3.13 7.20 0.6 2.30 0.15 0.4 0.4 578   38 16.05 22 3.37 7.00 0.2 2.84 0.11 0.1 0.1 579   38 31.66 22 3.37 7.00 0.2 2.84 0.11 0.1 0.1 579   38 33.46 22 3.71 13.19 0.5 2.37 0.12 0.5 580   38 34.31 22 4.45 11.54 10 2.11 0.09 0.4 07 581   38 1586 22 3.85 801 0.3 2.52 0.09 0.1 583   38 1586 22 3.85 801 0.3 2.52 0.09 0.1 583	38 24.74 21 58.40 9.02 0.5 2.27 0.10 0.4 0.3 584 38 15.75 22 3.15 8.04 0.3 2.75 0.19 0.2 0.2 585 38 14.05 22 4.05 6.33 0.4 2.43 0.07 0.3 0.4 586 38 15.94 22 3.35 7.04 0.2 2.63 0.06 0.2 0.1 587	38 23.53 21 44.88 10.31 0.2 2.40 0.05 0.2 0.2 588   38 14.21 22 4.97 8.43 0.5 2.61 0.16 0.3 0.2 589   38 14.02 22 5.98 7.49 0.5 2.27 0.11 0.3 0.2 589	38 23.87 22 0.30 9.08 0.5 0.00 0.07 0.3 0.3 591 38 24.86 21 57.66 9.20 0.5 2.13 0.10 0.2 0.2 592 38 34.64 22 5.69 13.95 1.9 0.00 0.14 0.8 1.1 593	3813.74 22 6.17 4.36 1.3 2.36 0.23 0.7 0.6 594 3815.81 22 3.54 7.57 0.7 2.33 0.13 0.6 0.3 595	382200 215920 8.21 0.4 2.47 0.11 0.2 0.2 596 38240 215956 8.21 0.4 2.47 0.11 0.2 0.2 596 38245 215550 977 0.5 2.45 0.18 0.2 0.3 597	38 14.34 22 4.64 6.64 0.6 2.21 0.13 0.4 0.4 598	38 22.// 21 30.01 6.93 0.2 1.8/ 0.02 0.2 0.2 599 38 21:58 21 59.92 7.16 0.3 2.30 0.10 0.3 0.3 600	38 22.19 21 53.39 7.46 0.3 2.39 0.10 0.2 0.2 602 38 13.26 22 5.50 5.55 0.7 2.45 0.11 0.4 0.3 603	38 24.53 21 57.81 9.24 0.5 2.36 0.11 0.2 0.2 604 38 24.53 21 57.65 8.98 0.6 2.19 0.11 0.3 0.3 605	38 24:46 21 57:90 9.22 0.4 2.53 0.13 0.2 0.2 606 38 37 4 30 62 0.45 0.4 0.00 0.07 0.2 605	38 22.09 22 12.95 8.67 0.4 2.23 0.08 0.3 0.4 608	38 25:12 21 55:92 9.04 0.4 2.58 0.11 0.1 0.2 609 38 18.74 22 0.48 8.26 0.7 2.43 0.14 0.4 0.3 610	38 22.08 21 59.63 7.69 0.5 2.45 0.14 0.2 0.3 611	38 25.31 22 9.74 9.33 0.7 2.47 0.09 0.5 0.6 613	38 24.32 21 51.76 7.46 0.4 2.11 0.04 0.1 0.2 614	38 23.18 21 39.57 8.42 0.6 2.34 0.13 0.3 0.4 013 38 23.66 21 59.75 9.22 0.4 2.35 0.13 0.2 0.2 616	38 20.94 22 4.04 8.54 0.2 2.49 0.07 0.1 0.1 617	38 22.03 22 4.21 9.01 0.3 2.28 0.06 0.1 0.1 618 38 25 43 22 10.14 11.13 0.4 2.25 0.08 0.3 0.3 619	38 24.06 22 0.14 8.85 0.5 2.48 0.16 0.3 0.4 620	38 20.86 21 44.46 9.28 0.5 2.65 0.15 0.4 0.2 621	36 22.0 21 20.0 10 02.0 2.0 0.50 0.50 01 0.0 02 38 23 77 21 01 01 01 02 23 03 24 010 01 01 01 62	38 14.39 22 4.97 7.71 0.5 2.23 0.15 0.3 0.3 624	38 21.12 22 2.09 8.26 0.3 2.63 0.09 0.1 0.1 625	38 20.58 21 49.43 7.98 0.4 2.18 0.07 0.3 0.3 626	38.22.60 22.5.59 3.98 0.3 2.31 0.12 0.2 0.3 628	38 10.61 22 4.45 12.36 0.4 2.35 0.08 0.3 0.3 629
Lat Long Depth ERZ Mag. RMS ERY newt   6.45 38.21.79 22.12.97 11.12 0.2 2.47 0.04 0.2 0.3 577   8.47 38.14.54 22 2.13.97 11.12 0.2 2.47 0.04 0.2 0.3 577   1.42 38.14.54 22 2.3.37 7.20 0.6 2.30 0.15 0.4 0.4 578   1.42 38.16.05 22 3.3.7 7.00 0.2 2.84 0.11 0.1 0.1 579   8.92 38.15.01 22 2.5.11 13.19 0.5 2.37 0.12 0.2 0.5 580   1.55 38.15.91 22 3.71 7.16 0.2 2.53 0.07 0.2 0.1 581   1.55 38.15.86 22 3.85 10.1 0.3 2.52 0.07 0.0 0.5 580   1.65 38.10.1	3.13 38.24.74 21.58.40 9.02 0.5 2.27 0.10 0.4 0.3 584 1.81 38.15.75 22.3.15 8.04 0.3 2.75 0.19 0.2 0.2 585 1.89 38.14.05 22.4.05 6.33 0.4 2.43 0.07 0.3 0.4 586 3.63 38.15.94 22 3.35 7.04 0.2 2.63 0.06 0.2 0.1 587	3.45 3823.53 2144.88 10.31 0.2 2.40 0.05 0.2 588   0.20 3814.21 22 4.97 8.43 0.5 2.61 0.16 0.3 0.2 589   0.20 3814.21 22 4.97 8.43 0.5 2.61 0.16 0.3 0.2 589   5.85 3814.02 22 5.98 7.49 0.5 2.27 0.11 0.3 0.2 590	1.70 38 23.87 22 0.30 9.08 0.5 0.00 0.07 0.3 0.3 591 1.32 38 24.86 21 57.66 9.20 0.5 2.13 0.10 0.2 0.2 592 3.19 38 34.64 22 5.69 13.95 1.9 0.00 0.14 0.8 1.1 593	38.14 38.13.74 22.6.17 4.36 1.3 2.36 0.23 0.7 0.6 594 18.19 38.15.81 22.3.54 7.57 0.7 2.33 0.13 0.6 0.3 595	8.05 38.22.00 21.59.20 8.21 0.4 2.47 0.11 0.2 596   4.05 38.24.55 9.77 0.5 2.45 0.11 0.2 596   4.05 38.24.55 9.77 0.5 2.45 0.18 0.2 596	23.76 38 14.34 22 4.64 6.64 0.6 2.21 0.13 0.4 0.4 598	1893 38 22.77 21 30.01 6.93 0.2 1.87 0.02 0.2 0.2 0.2 85 38 21.58 21 59.92 7.16 0.3 2.30 0.10 0.3 0.3 600	2.81 38.22.19 21.53.39 7.46 0.3 2.39 0.10 0.2 0.2 602 9.79 38.13.26 22.5.50 5.55 0.7 2.45 0.11 0.4 0.3 603	.82 38 24.53 21 57.81 9.24 0.5 2.36 0.11 0.2 0.2 604 65 38 24.53 21 57.65 8.98 0.6 2.19 0.11 0.3 0.3 605	86 38 24.46 21 57.90 9.22 0.4 2.53 0.13 0.2 0.2 606	220 30 22.09 22 12.95 8.67 0.4 2.23 0.08 0.3 0.4 608	5.4 38 25.12 21 55.92 9.04 0.4 2.58 0.11 0.1 0.2 609 1.61 38 18.74 22 0.48 8.26 0.7 2.43 0.14 0.4 0.3 610	5.08 38 22.08 21 59.63 7.69 0.5 2.45 0.14 0.2 0.3 611	0.0 38 25.31 22 9.74 9.33 0.7 2.47 0.09 0.5 0.6 613	.56 38 24.32 21 51.76 7.46 0.4 2.11 0.04 0.1 0.2 614	.23 38 23.18 21 39.57 8.42 0.6 2.34 0.13 0.3 0.4 015 2.79 38 23.66 21 59.75 9.22 0.4 2.35 0.13 0.2 0.2 616	13.89 38 20.94 22 4.04 8.54 0.2 2.49 0.07 0.1 0.1 617	0.03 38 22.03 22 4.21 9.01 0.3 2.28 0.06 0.1 0.1 618 605 38 25.43 22 10.14 11.13 0.4 2.25 0.08 0.3 0.3 619	0.58 38 24.06 22 0.14 8.85 0.5 2.48 0.16 0.3 0.4 620	0.35 38 20.86 21 44.46 9.28 0.5 2.65 0.15 0.4 0.2 621	20 7.0 28 72.70 21 70 72 73 0.3 72 74 0.10 0.5 75 75 75 75 75 75 75 75 75 75 75 75 75	2.57 38 14.39 22 4.97 7.71 0.5 2.23 0.15 0.3 0.3 624	9.88 38 21.12 22 2.09 8.26 0.3 2.63 0.09 0.1 0.1 625	0.87 38 20.58 21 49.43 7.98 0.4 2.18 0.07 0.3 0.3 626	4.61 38 22.60 22 5.59 3.98 0.3 2.31 0.12 0.2 0.3 628	9.96 38 10.61 22 4.45 12.36 0.4 2.35 0.08 0.3 0.3 629
Time Lat Long Depth ERZ Mag. RMS ERX ERY n.evt   3 4036.45 38 21.79 2212.97 11.12 0.2 247 0.04 0.2 27   4 1818.47 38 14.54 22 4.13 7.20 0.6 2.30 0.15 0.4 0.4 578   4 2241.42 38 16.65 22 3.37 7.00 0.2 284 0.11 0.1 0.1 579   4 435892 38 15.91 22 3.11 13.19 0.5 2.37 0.12 0.2 580   4 497252 38 15.91 22 3.71 7.16 0.2 2.53 0.07 0.2 0.5 580   4 497252 38 15.91 22 3.45 11.54 10 2.11 0.09 0.4 07 581   4 3595162 38 34.31 22 4.45 11.54 10 2.11 0.09 0.4 07 583   5 3026253 38 15.86 22 3.85 8.01 0.3 2.	5 4523.13 38 24.74 21 58.40 9.02 0.5 2.27 0.10 0.4 0.3 584   5 50 8.81 38 15.75 22 3.15 8.04 0.3 2.75 0.19 0.2 0.2 585   5 5521.89 38 14.05 22 4.05 6.33 0.4 2.43 0.07 0.3 0.4 586   5 5551.89 38 14.05 22 4.05 6.33 0.4 2.43 0.07 0.3 0.4 586   5 5619.63 38 15.94 22 3.35 7.04 0.2 2.63 0.06 0.2 0.1 587	63513.45 38.23.53 21.44.88 10.31 0.2 2.40 0.05 0.2 0.2 588   65010.20 38.14.21 22 4.97 8.43 0.5 2.61 0.16 0.3 0.2 588   73556.85 38.14.02 22 5.98 7.49 0.5 2.27 0.11 0.3 0.2 589	8 [841.70 38 23.87 22 0.30 9.08 0.5 0.00 0.07 0.3 0.3 59] 8 [9 9.32 38 24.86 21 57.66 9.20 0.5 2.13 0.10 0.2 0.2 592 8 5728.19 38 34.64 22 5.69 13.95 1.9 0.00 0.14 0.8 1.1 593	103938.14 3813.74 22 6.17 4.36 1.3 2.36 0.23 0.7 0.6 594 132048.19 3815.81 22 3.54 7.57 0.7 2.33 0.13 0.6 0.3 595	1334.805 38.22.00 2159.20 8.21 0.4 2.47 0.11 0.2 0.2 596 15 874.09 38 22.00 2156.50 8.21 0.4 7.45 0.18 0.2 0.3 597 15 874.09 38 749 2156.55	18 4423.76 38 14.34 22 4.64 6.64 0.6 2.21 0.13 0.4 0.4 598	19 1318.93 38 22.77 21 30.01 6.93 0.2 1.87 0.02 0.2 0.2 0.2 899 194138.02 38 21.58 21 59.92 7.16 0.3 2.30 0.10 0.3 0.3 600	23 032.81 38 22.19 21 53.39 7.46 0.3 2.39 0.10 0.2 0.2 602 23 719.79 38 13.26 22 5.50 5.55 0.7 2.45 0.11 0.4 0.3 603	0 328.82 38 24.53 21 57.81 9.24 0.5 2.36 0.11 0.2 0.2 604 0 910.65 38 24.53 21 57.65 8.98 0.6 2.19 0.11 0.3 0.3 605	0 948.86 38 24.46 21 57.90 9.22 0.4 2.53 0.13 0.2 0.2 606 1 310.75 30 37.1 37 6.7 0.45 0.7 0.07 0.7 0.7 60	1 4439.22 38 22.09 22 12.95 8.67 0.4 2.23 0.08 0.3 0.4 608	15526.54 38 25.12 21 55.92 9.04 0.4 2.58 0.11 0.1 0.2 609 4 383561 38 18.74 22 0.48 8.26 0.7 2.43 0.14 0.4 0.3 610	4 5736.08 38 22.08 21 59.63 7.69 0.5 2.45 0.14 0.2 0.3 611	6 2327.60 38 25.31 22 9.74 9.33 0.7 2.47 0.09 0.5 0.6 613	8 212.56 38 24.32 21 51.76 7.46 0.4 2.11 0.04 0.1 0.2 614	9 13 2.53 38 23.18 21 39.57 8.42 0.5 2.34 0.13 0.3 0.4 015 10 932.79 38 23.66 21 59.75 9.22 0.4 2.35 0.13 0.2 0.2 616	11 5953.89 38 20.94 22 4.04 8.54 0.2 2.49 0.07 0.1 0.1 617	12 216.03 38 22.03 22 4.21 9.01 0.3 2.28 0.06 0.1 0.1 618 12 56.05 38 25.43 22 10.14 11.13 0.4 2.25 0.08 0.3 0.3 619	15 2650 58 38 24.06 22 0.14 8.85 0.5 2.48 0.16 0.3 0.4 620	19 4340.35 38 20.86 21 44.46 9.28 0.5 2.65 0.15 0.4 0.2 621	2042.0.76 36.22.06 21.39.10 0.35 0.8 2.24 0.11 0.5 0.22 0.2 022 1.7 10 1.7 10 10 0.1 673	21 1552.57 38 14.39 22 4.97 7.71 0.5 2.23 0.15 0.3 0.3 624	21 3349.88 38 21.12 22 2.09 8.26 0.3 2.63 0.09 0.1 0.1 625	22 1040.87 38 20.58 21 49.43 7.98 0.4 2.18 0.07 0.3 0.3 626	23 294461 38 22.60 22 5.59 3.98 0.3 2.31 0.12 0.2 0.3 621	23 4749.96 38 10.61 22 4.45 12.36 0.4 2.35 0.08 0.3 0.3 629
Time Lat Long Depth ERZ Mag. RMS ERX ERY newt   20 34036.45 38 21.79 22 11.97 11.12 0.2 247 0.04 0.2 0.7 0.0 0.2 577   20 4 1818.47 38 14.54 22 4.13 7.20 0.6 2.30 0.15 0.4 0.4 578   20 4 2241.42 38 16.55 22 3.37 7.00 0.2 284 0.11 0.1 0.1 579   20 4 4975.25 38 15.91 22 3.11 13.19 0.5 2.37 0.01 0.2 580   20 4 4975.25 38 15.91 22 3.71 7.16 0.2 2.53 0.07 0.2 0.5 580   20 4 5951.62 38 34.31 22 4.45 11.54 10 2.11 0.09 0.4 0.7 581   20 5302.55 38 15.86 22 3.35 801 0.3 2.52 0.09	20 5 4523.13 38 24.74 21 58.40 9.02 0.5 2.27 0.10 0.4 0.3 584   20 5 50 8.81 38 15.75 22 3.15 8.04 0.3 2.75 0.19 0.2 0.2 585   20 5 5521.89 38 14.05 22 4.05 6.33 0.4 2.43 0.07 0.3 0.4 586   20 5 5551.89 38 14.05 22 4.05 6.33 0.4 2.43 0.07 0.3 0.4 586   20 5 5551.89 38 15.94 22 3.35 7.04 0.2 2.63 0.06 0.2 0.1 587	00 6 3513 45 38 23.53 21 44.88 10.31 0.2 2.40 0.05 0.2 0.2 588   00 6 5010.20 38 14.21 22 4.97 8.43 0.5 2.61 0.16 0.3 0.2 589   00 7 3556.85 38 14.02 22 5.98 7.49 0.5 2.27 0.11 0.3 0.2 589	00 8 1841.70 38 23.87 22 0.30 9.08 0.5 0.00 0.07 0.3 0.3 591 00 8 19 9.32 38 24.86 21 57.66 9.20 0.5 2.13 0.10 0.2 0.2 592 0 8 5728.19 38 34.64 22 5.69 13.95 1.9 0.00 0.14 0.8 1.1 593	0 103938.14 3813.74 22 6.17 4.36 1.3 2.36 0.23 0.7 0.6 594 0 132048.19 3815.81 22 3.54 7.57 0.7 2.33 0.13 0.6 0.3 595	0 1334.805 38.22.00 2159.20 8.21 0.4 2.47 0.11 0.2 0.2 596 0 15.824.09 38.22.09 2159.56 8.21 0.4 7.45 0.18 0.2 0.3 597	0 18 4423.76 38 14.34 22 4.64 6.64 0.6 2.21 0.13 0.4 0.4 598	0 19413802 3822.// 2130.01 6.95 0.2 1.8/ 0.02 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.	0 23 032.81 38 22.19 21 53.39 7.46 0.3 2.39 0.10 0.2 0.2 602 0 23 719.79 38 13.26 22 5.50 5.55 0.7 2.45 0.11 0.4 0.3 603	1 0 328.82 38 24.53 21 57.81 9.24 0.5 2.36 0.11 0.2 0.2 604 1 0 910.65 38 24.53 21 57.65 8.98 0.6 2.19 0.11 0.3 0.3 605	1 0 948.86 38 24.46 21 57.90 9.22 0.4 2.53 0.13 0.2 0.2 606	1 1 1 1 1 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2	1 15226.54 38 25.12 21 55.92 9.04 0.4 2.58 0.11 0.1 0.2 609 1 43835.61 38 18.74 22 0.48 8.26 0.7 2.43 0.14 0.4 0.3 610	1 45736.08 38.22.08 21 59.63 7.69 0.5 2.45 0.14 0.2 0.3 611	1 5 3 2 2 00 5 0 24 04 21 36 36 10 34 0 2 2 4 0 0 10 0 5 0 6 6 1 1 6 2 3 2 7 6 0 38 2 5 3 1 2 2 9 7 4 9 3 3 0 7 2 4 7 0 0 9 0 5 0 6 6 1 3	1 8 212.56 38 24.32 21 51.76 7.46 0.4 2.11 0.04 0.1 0.2 614	1 9 13 2.32 38 23 18 21 59 27 8 42 0.5 2.34 0.13 0.3 0.4 015 1 10 932.79 38 23.66 21 59.75 9.22 0.4 2.35 0.13 0.2 0.2 616	1 11 5953.89 38 20.94 22 4.04 8.54 0.2 2.49 0.07 0.1 0.1 617	1 12 210.03 38 22.03 22 4.21 9.01 0.3 2.28 0.06 0.1 0.1 618 1 12 56.05 38 25.43 22 10.14 11.13 0.4 2.25 0.08 0.3 0.3 619	1 15 2650.58 38 24.06 22 0.14 8.85 0.5 2.48 0.16 0.3 0.4 620		270 770 770 770 770 770 770 770 770 770	1 211552.57 3814.39 22 4.97 7.71 0.5 2.23 0.15 0.3 0.3 624	1 21 3349.88 38 21.12 22 2.09 8.26 0.3 2.63 0.09 0.1 0.1 625	1 22 1040.87 38 20.58 21 49.43 7.98 0.4 2.18 0.07 0.3 0.3 626	1 23 294461 38 22.60 22 5.59 3.98 0.3 2.31 0.12 0.2 0.3 628	l 23 4749.96 38 10.61 22 4.45 12.36 0.4 2.35 0.08 0.3 0.3 629
Date Time Lat Long Depth ERZ Mag. RMS RKX ERY newt   910820 3 4036.45 38 21.79 22 12.97 11.12 0.2 247 0.04 0.2 577   910820 4 1818.47 38 14.54 22 4.13 7.20 0.6 2.30 0.15 0.4 0.4 578   910820 4 1818.47 38 14.54 22 4.13 7.20 0.6 2.30 0.15 0.4 0.4 578   910820 4 2241.42 38 16.05 22 3.37 7.00 0.2 2.84 0.11 0.1 0.1 579   910820 4 497.25 38 33.66 22 3.11 13.19 0.5 2.37 0.07 0.2 0.5 580   910820 4 5951.22 38 3.4.31 22 4.45 11.54 10 2.11 0.01 0.2 0.1 581   910820 5 3026.25 38 34.31 22 4.45 11.54 10 2.11 0.09 0.1<	910820 5 4523.13 38 24.74 21 58.40 9.02 0.5 2.27 0.10 0.4 0.3 584   910820 5 508.81 38 15.75 22 3.15 8.04 0.3 2.75 0.19 0.2 0.2 585   910820 5 5521.89 38 14.05 22 4.05 6.33 0.4 2.43 0.07 0.3 0.4 586   910820 5 5521.89 38 14.05 22 4.05 6.33 0.4 2.43 0.07 0.3 0.4 586   910820 5 5619.63 38 15.94 22 3.35 7.04 0.2 2.63 0.06 0.2 0.1 587	910820 6 3513.45 38 23.53 21 44.88 10.31 0.2 2.40 0.05 0.2 0.2 588   910820 6 5010.20 38 14.21 22 4.97 8.43 0.5 2.61 0.16 0.3 0.2 589   910820 6 5010.20 38 14.02 22 5.98 7.49 0.5 2.77 0.11 0.3 0.2 589   910820 7 3556.85 38 14.02 22 5.98 7.49 0.5 2.77 0.11 0.3 0.2 590	910820 8 1841.70 38 23.87 22 0.30 9.08 0.5 0.00 0.07 0.3 0.3 591 910820 8 19 9.32 38 24.86 21 57.66 9.20 0.5 2.13 0.10 0.2 0.2 592 910820 8 5728.19 38 34.64 22 5.69 13.95 1.9 0.00 0.14 0.8 1.1 593	910820 10.3938.14 38.13.74 22.6.17 4.36 1.3 2.36 0.23 0.7 0.6 594 910820 13.2048.19 38.15.81 22.3.54 7.57 0.7 2.33 0.13 0.6 0.3 595	910820 13 34 8.05 38 22.00 21 59.20 8.21 0.4 2.47 0.11 0.2 0.2 596 910820 15 824 80 38 22.00 21 59.20 8.21 0.4 2.47 0.11 0.2 0.2 596 910820 15 824 80 38 249 21 56 50 977 0.5 2.45 0.18 0.2 0.3 597	910820 18 4423.76 38 14.34 22 4.64 6.64 0.6 2.21 0.13 0.4 0.4 598	910820 191318.93 38 22.77 21 30.01 6.93 0.2 1.87 0.02 0.2 0.2 0.2 899 910820 194138.02 38 21.58 21 59.92 7.16 0.3 2.30 0.10 0.3 0.3 600	910820 23 032.81 38 22.19 21 53.39 7.46 0.3 2.39 0.10 0.2 0.2 602 910820 23 719.79 38 13.26 22 5.50 5.55 0.7 2.45 0.11 0.4 0.3 603	910821 0 328.82 38 24.53 21 57.81 9.24 0.5 2.36 0.11 0.2 0.2 604 910821 0 910.65 38 24.53 21 57.65 8.98 0.6 2.19 0.11 0.3 0.3 605	910821 0 948.86 38 24.46 21 57.90 9.22 0.4 2.53 0.13 0.2 0.2 606 010021 1 310.75 30 27.4 27 6.45 0.7 0.07 0.7 0.2 607	910821 1 4439.22 38 22.09 22 12.95 8.67 0.4 2.23 0.08 0.3 0.4 608	910821 15526.54 38 25.12 21 55.92 9.04 0.4 2.58 0.11 0.1 0.2 609 910821 4 3835.61 38 18.74 22 0.48 8.26 0.7 2.43 0.14 0.4 0.3 610	910821 45736.08 38.22.08 21 59.63 7.69 0.5 2.45 0.14 0.2 0.3 611	910821 6 2327.60 38 25.31 22 9.74 9.33 0.7 2.47 0.09 0.5 0.6 613	910821 8 212.56 38 24.32 21 51.76 7.46 0.4 2.11 0.04 0.1 0.2 614	910821 9 43 232 38 23.18 21 59.77 8.42 0.5 2.34 0.13 0.3 0.4 015 910821 10 932.79 38 23.66 21 59.75 9.22 0.4 2.35 0.13 0.2 0.2 616	910821 11 5953.89 38 20.94 22 4.04 8.54 0.2 2.49 0.07 0.1 0.1 617	910821 12 216.03 38 22.03 22 4.21 9.01 0.3 2.28 0.06 0.1 0.1 618 910821 12 56.05 38 25.43 22 10.14 11.13 0.4 2.25 0.08 0.3 0.3 619	910821 15 2650.58 38 24.06 22 0.14 8.85 0.5 2.48 0.16 0.3 0.4 620	910821 19 4340.35 38 20.86 21 44.46 9.28 0.5 2.65 0.15 0.4 0.2 621	10821 24420.78 25.25.08 21.26 01.25 27 25.25.08 25.25 01.024 25 12 25.25 010871 75 17 01.01 01 01 25.25 023 023 023 023 021 01 01 01 01 15.25	910821 21 1552.57 38 14.39 22 4.97 7.71 0.5 2.23 0.15 0.3 0.3 624	910821 21 3349.88 38 21.12 22 2.09 8.26 0.3 2.63 0.09 0.1 0.1 625	910821 22 1040.87 38 20.58 21 49.43 7.98 0.4 2.18 0.07 0.3 0.3 626	910821 23 2944.61 38 22.60 22 5.59 3.98 0.3 2.31 0.12 0.2 0.3 628	910821 23 4749.96 38 10.61 22 4.45 12.36 0.4 2.35 0.08 0.3 0.3 629

APPENDIX	B (Continued.	•																	
Date	Time	Lat	Long	Depth ]	ERZ	lag. R	WS E	EX .	RY D.e.	vt Date	Time	Lat	Long	Depth ERZ	Mag.	RMS	ERX	ERY	n.evt
910823	17 2346.57	38 24.38	21 57.58	8.91	0.9	0 ( 20 (		0 	80	910824	6 348.74	38 22.01	22 11.47	10.00 0.2	2.34	0.0	0.2	0.1	738
910823	18 5128.72	38 24.68	21 58.02	9.13	0.7	0 0 27 3	2 8		180	910824	6 /35.73	38 22.17	22 11.82	9.81 0.4	2.4	0.08	0.7	07	139
910823	19 12 9.01	38 24.52	21 58.53	8.11	4 0 4 4 7 7	ې د ۲	o ⊂ 8 ≤	j c	2004	910024	15.0511 0	20 21 20	71.11 22	9.88 0.3	2.23	8.0	0.0	0.7	<del>1</del>
910823	19 24 4.24	38 24.12	07/C 17	10.0				• -	7 069 7 1	910824	6 4436.57	38 22 88	22 11.84	9.07 0.4 9.43 0.4	107	6 = C	56		141
910823	10./4/2 01	38 24.17	15 15 16	9.23	0.6	55 0 0	14	0	2 69	910824	7 438.82	38 22.14	22 11.47	9.37 0.3	2 40 7 40	100	32		
910823	11.16/2 61	38 23 55	21 52.37	16.88	0.3	36	8	0	3 692	910824	7 3637.91	38 22.22	22 11.55	9.32 0.3	230	0.08	9 <b>0</b>	40	44
910823	20 4922.72	38 13.26	22 7.06	6.42	0.3 2	30	03	5	2 693	910824	8 642.44	38 22.49	22 11.88	9.57 0.3	2.41	0.0	0.2	0.7	745
910823	21 2248.94	38 24.07	21 57.55	8.39	0.5 2	.43	8	0	2 69	910824	8 751.57	38 22.34	22 11.82	9.34 0.3	2.27	0.08	0.2	0.3	746
910823	21 25 7.24	38 24.00	21 57.45	9.23	0.4	8; ; 0 ;	8 8		2 69	910824	8 8 1.87	38 22.36	22 11.88	8.97 0.3	2.40	0.0	0.2	0.3	747
910823	21 3059.57	38 25.27	21 59.25	8.58	0.5	<del>4</del> .:	0] (		969	910824	8 858.43	38 22.46	22 12.13	9.77 0.3	2.63	0.0	0.2	0.2	748
910823	21 4157.97	38 24.92	21 58.92	8.42	0.8	E 6	ຕຸ :		0 0	910824	8 52 3.96	38 22.46	22 12.00	9.81 0.3	2.56	0.10	0.2	0.2	749
910823	21 5332.51	38 24.42	21 57.96	80.6	8.0	67 1 67 1	= s	5 C	4 0 20 2	910824	8 2454.95	38 Z2 54	22 11.92	9.88 0.4	2.50	0.0	0.2	0.3	750
910823	22 158.91	38 24.05	21 57.25	5	0.0	2 4 2 4	ם א בי א	5 C	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	910824	11.2052.9	38 22.39	22 11.81	9.99 0.4	2.50	0.08	0.3	0.2 V	751
910823	22 9 1.28	38 24.08	50./C 12	7/ 9	5 0 6 0	5 6 6 6	9 : 9 :		ž	479016 f	21.1420 4	00.41.00	00.C 22	0.0 00.1	2.74	0.13	6.0 1	0.3	752
910823	22 2140.63	38 24.09	21 57.46	9.28	4 v 7 v	۶. : ۲. :	= : = :	-, c		910824	99.1 9C 01	38 24.59	21 51.74	8.53 0.6	8 8	0.11	0.4	0.3	753
910823	23 157.32	38 24.07	21 57.61	19.6	<b>0</b> 0	4 0	5 ( 1 (	о с 1 с		910824	11 430.90	38 21.84	17.8 77	0.2	2.37	0.05	0.1	0.2	75
910823	23 233.62	38 23.99	21 57.42	9.65	0.6	83	6[	0 ·	20 20 20	910824	11 4548.86	38 23.70	21 53.85	6.96 1.1	2.36	0.13	0.4	0.4	755
910823	23 1513.05	38 23.84	21 57.77	8.99	0.5	27 0	80.	0	5	910824	12 931.34	38 24.11	21 55.17	8.81 0.4	2.75	0.11	0.2	0.1	756
910823	23 1648.37	38 24.14	21 57.74	8.99	0.5	58	2	0	202	910824	12 36 5.88	38 22.22	22 11.79	10.07 0.2	2.67	0.0	0.2	0.3	757
910823	23 1837.94	38 24.02	21 57.67	9.17	0.4	.43	8	5	.1	910824	12 3657.79	38 22.26	22 11.34	9.78 0.2	2.03	0.03	0.2	0.3	759
910823	23 1851.74	38 23.84	21 57.64	8.87	0.5	<u>4</u>		0 0	20,	7 910824	12 4415.98	38 21.90	22 12.18	9.58 0.5	2.39	0.10	0.4	0.5	760
910824	0 656.55	38 24.17	21 57.27	9.31	0.5 2	53 0	6	10	5 2 2	8 910824	14 5532.25	38 22.55	22 11.86	10.09 0.4	2.82	0.15	0.3	0.2	761
910824	0 918.04	38 24.16	21 57.34	9.13	0.4	56	Ē	2	5	9 910824	15 2957.97	38 21.76	22 15.33	12.36 0.2	2.46	0.03	0.5	0.4	762
910824	0 950.24	38 24.15	21 57.37	8.21	0.3	16	8		11	910824	16 4041.85	38 21.36	22 8.39	7.13 0.3	2.29	0.10	0.3	0.4	763
910824	0 23 2.28	38 22.23	22 11.92	9.50	0.3	37	8	20	11	1 910824	164958.94	38 22.13	22 11.58	9.54 0.4	2.19	0.07	0.4	0.5	764
910824	03126.72	38 13.83	22 5.18	7.93	0.8	ŝ	.15	.4	12 21	2 910824	17 2253.09	38 22.64	22 11.81	10.76 0.4	2.67	0.12	<b>0</b> .4	0.3	765
910824	0 3711.56	38 21.96	22 11.36	9.57	0.3	5 7	ş	2	1 1	3 910824	17 3919.63	38 22.42	22 11.81	9.52 0.3	2.21	0.05	0.3	0.3	766
910824	0 38 5.97	38 22.34	22 12.01	9.56	0.4	78	8.	2	1	4 910824	17 4624.73	38 22.11	22 12.58	9.21 0.4	2.30	0.0	0.4	0.4	767
910824	0 39 7.86	38 22.46	22 12.05	9.35	0.3	2	8	2	1	5 910824	18 2417.30	38 22.29	22 12.04	9.87 0.5	2.35	0.08	0.5	0.5	768
910824	0 5426.01	38 35.76	21 56.38	20.06	0.5	121	8		.6 71	910824	18 3044.95	38 22.33	22 11.95	10.10 0.4	2.39	0.08	0.4	0.5	769
910824	1 725.09	38 24.44	21 58.24	9.11	0.8	31	0.10	4	12 21	7 910824	18 3812.37	38 22.07	22 11.94	9.83 0.3	2.19	0.06	0.2	0.2	70
910824	1 746.83	38 24.29	21 57.94	9.19	0.6	22	8.	2	3 71	910824	18 49 16.92	38 23.96	22 1.05	9.23 0.2	2.4	0.02	0.1	0.2	171
910824	1 3732.72	38 24.29	21 57.25	8.62	0.4	2.41	8	2	12	9 910824	19 4531.78	38 22.20	22 11.91	9.74 0.3	2.21	0.08	0.4	0.4	<b>712</b>
910824	1 55 9.45	38 22.18	22 11.71	9.24	40	57	SO 2	4.0	1 2	0 910824	20 1640.56	38 30.21	21 50.88	14.11 0.3	2.30	2.0	0.2	0.3	113
910824	2 7 4.53	38 22.32	22 11.77	10.03	4.0	49 9 9	8		2 9	1 910824	20 5224.09	38 14.09	761 77	/./0 0/./	60.2	0.15	0.5	<b>4</b> .0	14
910824	2 2140.27	38 22.51	22 11.80	02.6		5.5	8 8		24	010024	00714C 07	10.22.80	C61 77	0.28 0.4	9.5	5.0	7.0	4.0	ÊÌ
910824	2 2143.41	38 22.51	22 11.90	5.5	2.0	4	5 8	7.5	2 6	470016 7	12.1 4 12	20.02 00	5.4.5	C.U 01.6	2.12	01.0	700		2
910824	2 2849.54	38 22.22	22 11.85	10.6	4.0	64.7	5.8	33		470016 4	+1.0C/ 12	01.44 05	24 11 22	10.40 0.3	00.7	8.0	<u> </u>	<u> </u>	Ξ
910824	2 5326.63	38 22.18	22 11.89	10.6	4 v		8	12	2 8	+70016	14.CI11 17	71.77 OC	CF:11 77	C.U CK.4	5.1	55	7.0	5.0	811
910824	2 5353.18	38 22.16	22 11.82	9.52	0.0	617	5 8	22	25	0 910024	21 14 4.70	00.77 0C	7/11 77	9.78 0.2	27	10.0 0	7.0	7.0	6
910824	2 5742.49	38 22 23	22 12.08	5.6	* *		5 5		2 C	010024	10.040C 12	1117 00	70°C1 77		; ; ; ;	8.0		<u>.</u>	
910824	3 1 6.95	38 22.51	22 11.90	10.6	5.6	2:		12	28	470016 Q	1777 01 77	10.12.00	22 4.00	5.0 00.01	2.7	0.10	7.0	0.1	/81
910824	4 5457.96	38 22.23	22 11.49	20.6	200	4 5	5 5	35		470016 0	41-1 7C 77	00 20.00 05 00 02	64-00 17 CC	0.044 0.3	6.7	8.0		7.0	202
910824	5 728.32	38 22.15	22 11.02	R 7	۰ د ۲ د	17.7	5 5	12	1 S 2 E	1 010874	12 1247 80	70 26 26	10-11 77	7.0 00 01	2 00	500	7.0	7 4	6 5
910824	5 740.21	38 22.11	22 11.74	0.6	3	<b>?</b>		12	3 C C E	470016 I	00.190102	05.00.00	+C'0C 17	21 20 20	00.7	0.00		33	8 8
910824	5 825.63	38 22.80	22 11.90	00.7	 	212	8 8			10010 T	73 4755 KD	28 36 10	20.00 12	CT 0000	60.7		200	4 V	C0/
910824	5 221/1/2 5 220025	38 22.15	27 14:00	190	* "	100	9 8	32	5 E	4 910875	0 5841 55	21.UC 0C	PL 11 CC	0.0 0.00	40.7 1 P C	550	32	0.0	107
910624	25.6205 C	28 22.22 85	10.21 22	10.00		3.4	32	3 2	1 C	s 910825	1 3418.75	38 14 46	22 8.00	6.69 0.7	117	500	1 Y O	50	101
910824	14.7000 C	20 22.11	72 11.87	9.85	1 4	200	58	: 2	13 13	6 910825	1 3945.99	38 13.80	22 7.70	7.74 0.6	251	0.13	0.4	03	789
910824	5 5058.35	38 22.47	22 12.84	9.38	. E.O	30	50	5	12 73	7 910825	2 31 9.72	38 34.06	21 55.68	23.24 0.9	2.34	0.03	0.3	1.7	790

	n.evi	818	819	820	821	822	823	824	825	826	827	828	829	830	831	833	834	835	836	837	838	842	843	844	845	846	847	848
	EKI	0.2	0.2	0.8	0.3	0.5	0.2	0.2	0.3	0.2	0.3	0.4	0.3	0.2	0.5	0.1	0.1	0.3	0.4	0.3	0.3	0.2	0.3	0.1	0.7	0.6	0.3	0.2
	ËK	0.2	0.3	0.6	0.2	0.7	0.3	0.2	0.3	0.3	0.3	0.7	0.3	0.2	1.0	0.2	0.3	0.4	0.6	0.3	0.4	0.2	0.4	0.3	0.6	0.9	0.3	0.5
	KMN	0.09	0.16	0.11	0.09	0.14	0.16	0.05	0.11	0.11	0.11	0.11	0.16	0.08	0.12	0.07	0.11	0.04	0.14	0.08	0.12	0.14	0.12	0.08	0.20	0.05	0.09	0.09
;	Mag.	1.94	2.59	2.25	2.25	0.00	2.53	1.86	2.06	2.75	2.49	2.76	2.55	2.14	2.67	2.62	2.59	2.50	2.35	2.44	2.46	2.42	2.68	2.46	2.87	2.81	2.46	2.65
ļ	ERZ	0.4	0.4	0.9	0.6	2.3	0.4	0.4	0.5	0.5	0.4	0.9	0.5	0.3	2.0	0.3	0.2	0.4	0.9	0.4	0.7	0.5	0.8	0.5	0.8	1.7	0.8	0.8
	Depth	7.13	7.89	10.61	6.57	11.97	8.00	7.88	8.62	7.80	12.28	10.46	7.37	8.00	9.32	9.51	7.15	10.18	5.98	8.55	6.79	7.53	8.59	6.10	7.02	9.85	8.40	8.98
1	Long	21 57.77	22 5.91	22 8.27	22 8.31	22 3.73	22 5.46	22 0.01	22 0.35	21 52.98	21 58.59	22 18.99	22 6.05	22 5.95	21 49.69	22 1.03	21 59.21	21 55.12	22 5.52	21 58.94	22 0.40	22 5.10	21 55.82	22 9.02	22 8.53	21 49.22	22 5.89	22 4.72
	Lat	38 24.27	38 13.94	38 25.24	38 22.69	38 16.14	38 14.11	38 22.65	38 23.09	38 18.49	38 28.99	38 18.35	38 13.87	38 20.50	38 23.56	38 21.68	38 19.02	38 24.96	38 14.17	38 24.61	38 22.08	38 14.61	38 24.32	38 18.02	38 22.86	38 23.91	38 14.67	38 18.83
	Time	1 4317.41	1 5632.37	2 743.46	2 33 2.76	3 813.45	4 149.52	4 1423.63	4 1434.31	6 2140.32	8 1826.91	8 3755.60	9 13 2.50	9 2911.82	10 841.93	11 3417.67	16 1259.39	18 5614.29	19 1450.34	20 3311.15	22 3928.52	3 1510.05	3 5411.37	4 828.08	4 5822.36	5 4953.42	8 2640.22	8 5250.32
	Date	910826	910826	910826	910826	910826	910826	910826	910826	910826	910826	910826	910826	910826	910826	910826	910826	910826	910826	910826	910826	910827	910827	910827	910827	910827	910827	910827
	n.evt	161	792	793	794	795	796	<i>161</i>	798	661	800	801	802	803	804	805	806	807	808	<b>608</b>	811	812	813	814	815	816	817	818
	ERY n.evt	0.1 791	0.2 792	0.3 793	0.2 794	0.3 795	0.5 796	0.5 797	0.4 798	0.5 799	0.2 800	0.2 801	0.1 802	0.4 803	0.3 804	0.4 805	0.5 806	0.4 807	0.2 808	0.4 809	0.3 811	0.6 812	0.2 813	0.4 814	0.4 815	0.3 816	0.5 817	0.2 818
	ERX ERY n.evt	0.3 0.1 791	0.2 0.2 792	0.3 0.3 793	0.3 0.2 794	0.1 0.3 795	0.5 0.5 796	0.5 0.5 797	0.4 0.4 798	0.3 0.5 799	0.3 0.2 800	0.5 0.2 801	0.2 0.1 802	0.3 0.4 803	0.3 0.3 804	0.4 0.4 805	0.4 0.5 806	0.2 0.4 807	0.1 0.2 808	0.2 0.4 809	0.2 0.3 811	0.5 0.6 812	0.3 0.2 813	0.5 0.4 814	0.2 0.4 815	0.3 0.3 816	1.7 0.5 817	0.2 0.2 818
	RMS ERX ERY n.evt	0.11 0.3 0.1 791	0.13 0.2 0.2 792	0.08 0.3 0.3 793	0.13 0.3 0.2 794	0.05 0.1 0.3 795	0.16 0.5 0.5 796	0.14 0.5 0.5 797	0.15 0.4 0.4 798	0.07 0.3 0.5 799	0.10 0.3 0.2 800	0.04 0.5 0.2 801	0.08 0.2 0.1 802	0.13 0.3 0.4 803	0.15 0.3 0.3 804	0.19 0.4 0.4 805	0.10 0.4 0.5 806	0.07 0.2 0.4 807	0.10 0.1 0.2 808	0.13 0.2 0.4 809	0.11 0.2 0.3 811	0.10 0.5 0.6 812	0.12 0.3 0.2 813	0.04 0.5 0.4 814	0.10 0.2 0.4 815	0.09 0.3 0.3 816	0.12 1.7 0.5 817	0.09 0.2 0.2 818
	Mag. RMS ERX ERY n.evt	2.82 0.11 0.3 0.1 791	2.46 0.13 0.2 0.2 792	2.41 0.08 0.3 0.3 793	2.84 0.13 0.3 0.2 794	2.36 0.05 0.1 0.3 795	2.44 0.16 0.5 0.5 796	2.21 0.14 0.5 0.5 797	2.14 0.15 0.4 0.4 798	2.36 0.07 0.3 0.5 799	2.39 0.10 0.3 0.2 800	1.96 0.04 0.5 0.2 801	2.46 0.08 0.2 0.1 802	2.44 0.13 0.3 0.4 803	2.49 0.15 0.3 0.3 804	2.50 0.19 0.4 0.4 805	2.31 0.10 0.4 0.5 806	2.16 0.07 0.2 0.4 807	2.64 0.10 0.1 0.2 808	2.48 0.13 0.2 0.4 809	2.34 0.11 0.2 0.3 811	2.35 0.10 0.5 0.6 812	2.41 0.12 0.3 0.2 813	2.39 0.04 0.5 0.4 814	2.35 0.10 0.2 0.4 815	2.24 0.09 0.3 0.3 816	2.27 0.12 1.7 0.5 817	1.94 0.09 0.2 0.2 818
	ERZ Mag. RMS ERX ERY n.evt	0.5 2.82 0.11 0.3 0.1 791	0.5 2.46 0.13 0.2 0.2 792	0.4 2.41 0.08 0.3 0.3 793	0.4 2.84 0.13 0.3 0.2 794	0.2 2.36 0.05 0.1 0.3 795	0.9 2.44 0.16 0.5 0.5 796	0.8 2.21 0.14 0.5 0.5 797	0.8 2.14 0.15 0.4 0.4 798	0.4 2.36 0.07 0.3 0.5 799	0.3 2.39 0.10 0.3 0.2 800	0.4 1.96 0.04 0.5 0.2 801	0.5 2.46 0.08 0.2 0.1 802	0.6 2.44 0.13 0.3 0.4 803	0.5 2.49 0.15 0.3 0.3 804	0.5 2.50 0.19 0.4 0.4 805	0.4 2.31 0.10 0.4 0.5 806	0.3 2.16 0.07 0.2 0.4 807	0.3 2.64 0.10 0.1 0.2 808	0.3 2.48 0.13 0.2 0.4 809	0.2 2.34 0.11 0.2 0.3 811	0.8 2.35 0.10 0.5 0.6 812	0.3 2.41 0.12 0.3 0.2 813	0.5 2.39 0.04 0.5 0.4 814	0.5 2.35 0.10 0.2 0.4 815	0.7 2.24 0.09 0.3 0.3 816	1.9 2.27 0.12 1.7 0.5 817	0.4 1.94 0.09 0.2 0.2 818
	Depth ERZ Mag. RMS ERX ERY n.evt	8.32 0.5 2.82 0.11 0.3 0.1 791	4.50 0.5 2.46 0.13 0.2 0.2 792	9.60 0.4 2.41 0.08 0.3 0.3 793	9.67 0.4 2.84 0.13 0.3 0.2 794	10.96 0.2 2.36 0.05 0.1 0.3 795	9.20 0.9 2.44 0.16 0.5 0.5 796	7.53 0.8 2.21 0.14 0.5 0.5 797	7.86 0.8 2.14 0.15 0.4 0.4 798	6.94 0.4 2.36 0.07 0.3 0.5 799	9.37 0.3 2.39 0.10 0.3 0.2 800	9.86 0.4 1.96 0.04 0.5 0.2 801	9.15 0.5 2.46 0.08 0.2 0.1 802	7.33 0.6 2.44 0.13 0.3 0.4 803	7.54 0.5 2.49 0.15 0.3 0.3 804	7.82 0.5 2.50 0.19 0.4 0.4 805	6.69 0.4 2.31 0.10 0.4 0.5 806	7.67 0.3 2.16 0.07 0.2 0.4 807	9.32 0.3 2.64 0.10 0.1 0.2 808	6.91 0.3 2.48 0.13 0.2 0.4 809	7.19 0.2 2.34 0.11 0.2 0.3 811	6.85 0.8 2.35 0.10 0.5 0.6 812	7.04 0.3 2.41 0.12 0.3 0.2 813	10.99 0.5 2.39 0.04 0.5 0.4 814	14.30 0.5 2.35 0.10 0.2 0.4 815	6.68 0.7 2.24 0.09 0.3 0.3 816	8.79 1.9 2.27 0.12 1.7 0.5 817	7.13 0.4 1.94 0.09 0.2 0.2 818
	Long Depth ERZ Mag. RMS ERX ERY n.evt	21 48.56 8.32 0.5 2.82 0.11 0.3 0.1 791	22 4.89 4.50 0.5 2.46 0.13 0.2 0.2 792	22 11.71 9.60 0.4 2.41 0.08 0.3 0.3 793	22 11.84 9.67 0.4 2.84 0.13 0.3 0.2 794	22 7.96 10.96 0.2 2.36 0.05 0.1 0.3 795	22 7.70 9.20 0.9 2.44 0.16 0.5 0.5 796	22 5.29 7.53 0.8 2.21 0.14 0.5 0.5 797	22 5.74 7.86 0.8 2.14 0.15 0.4 0.4 798	22 4.70 6.94 0.4 2.36 0.07 0.3 0.5 799	22 11.81 9.37 0.3 2.39 0.10 0.3 0.2 800	22 11.68 9.86 0.4 1.96 0.04 0.5 0.2 801	22 3.78 9.15 0.5 2.46 0.08 0.2 0.1 802	22 5.20 7.33 0.6 2.44 0.13 0.3 0.4 803	22 5.80 7.54 0.5 2.49 0.15 0.3 0.3 804	22 5.80 7.82 0.5 2.50 0.19 0.4 0.4 805	22 3.96 6.69 0.4 2.31 0.10 0.4 0.5 806	21 49.81 7.67 0.3 2.16 0.07 0.2 0.4 807	21 54.74 9.32 0.3 2.64 0.10 0.1 0.2 808	22 8.01 6.91 0.3 2.48 0.13 0.2 0.4 809	22 7.98 7.19 0.2 2.34 0.11 0.2 0.3 811	22 4.94 6.85 0.8 2.35 0.10 0.5 0.6 812	22 5.46 7.04 0.3 2.41 0.12 0.3 0.2 813	22 8.13 10.99 0.5 2.39 0.04 0.5 0.4 814	21 54.47 14.30 0.5 2.35 0.10 0.2 0.4 815	21 53.48 6.68 0.7 2.24 0.09 0.3 0.3 816	21 58.40 8.79 1.9 2.27 0.12 1.7 0.5 817	21 57.77 7.13 0.4 1.94 0.09 0.2 0.2 818
	Lat Long Depth ERZ Mag. RMS ERX ERY n.evt	38 20.37 21 48.56 8.32 0.5 2.82 0.11 0.3 0.1 791	38 10.94 22 4.89 4.50 0.5 2.46 0.13 0.2 0.2 792	38 22.06 22 11.71 9.60 0.4 2.41 0.08 0.3 0.3 793	38 22.35 22 11.84 9.67 0.4 2.84 0.13 0.3 0.2 794	38 25.35 22 7.96 10.96 0.2 2.36 0.05 0.1 0.3 795	38 13.69 22 7.70 9.20 0.9 2.44 0.16 0.5 0.5 796	38 14.54 22 5.29 7.53 0.8 2.21 0.14 0.5 0.5 797	38 14.42 22 5.74 7.86 0.8 2.14 0.15 0.4 0.4 798	38 13.86 22 4.70 6.94 0.4 2.36 0.07 0.3 0.5 799	38 22.40 22 11.81 9.37 0.3 2.39 0.10 0.3 0.2 800	38 21.81 22 11.68 9.86 0.4 1.96 0.04 0.5 0.2 801	38 20.76 22 3.78 9.15 0.5 2.46 0.08 0.2 0.1 802	38 14.48 22 5.20 7.33 0.6 2.44 0.13 0.3 0.4 803	38 13.86 22 5.80 7.54 0.5 2.49 0.15 0.3 0.3 804	38 13.62 22 5.80 7.82 0.5 2.50 0.19 0.4 0.4 805	38 13.76 22 3.96 6.69 0.4 2.31 0.10 0.4 0.5 806	38 23.87 21 49.81 7.67 0.3 2.16 0.07 0.2 0.4 807	38 24.63 21 54.74 9.32 0.3 2.64 0.10 0.1 0.2 808	38 23.08 22 8.01 6.91 0.3 2.48 0.13 0.2 0.4 809	38 22.97 22 7.98 7.19 0.2 2.34 0.11 0.2 0.3 811	38 13.60 22 4.94 6.85 0.8 2.35 0.10 0.5 0.6 812	38 14.25 22 5.46 7.04 0.3 2.41 0.12 0.3 0.2 813	38 24.75 22 8.13 10.99 0.5 2.39 0.04 0.5 0.4 814	38 34.48 21 54.47 14.30 0.5 2.35 0.10 0.2 0.4 815	38 22.14 21 53.48 6.68 0.7 2.24 0.09 0.3 0.3 816	38 24.74 21 58.40 8.79 1.9 2.27 0.12 1.7 0.5 817	38 24.27 21 57.77 7.13 0.4 1.94 0.09 0.2 0.2 818
	Time Lat Long Depth ERZ Mag. RMS ERX ERY n.evt	4 556.74 38 20.37 21 48.56 8.32 0.5 2.82 0.11 0.3 0.1 791	4 4616.40 38 10.94 22 4.89 4.50 0.5 2.46 0.13 0.2 0.2 792	5 1319.02 38 22.06 22 11.71 9.60 0.4 2.41 0.08 0.3 0.3 793	5 1621.73 38 22.35 22 11.84 9.67 0.4 2.84 0.13 0.3 0.2 794	5 5951.93 38 25.35 22 7.96 10.96 0.2 2.36 0.05 0.1 0.3 795	6 9 5.20 38 13.69 22 7.70 9.20 0.9 2.44 0.16 0.5 0.5 796	6 3651.11 38 14.54 22 5.29 7.53 0.8 2.21 0.14 0.5 0.5 797	6 4940.60 38 14.42 22 5.74 7.86 0.8 2.14 0.15 0.4 0.4 798	7 2254.70 38 13.86 22 4.70 6.94 0.4 2.36 0.07 0.3 0.5 799	7 4056.40 38 22.40 22 11.81 9.37 0.3 2.39 0.10 0.3 0.2 800	9 3349.37 38 21.81 22 11.68 9.86 0.4 1.96 0.04 0.5 0.2 801	94724.14 38 20.76 22 3.78 9.15 0.5 2.46 0.08 0.2 0.1 802	11 2736.16 38 14.48 22 5.20 7.33 0.6 2.44 0.13 0.3 0.4 803	11 30 2.97 38 13.86 22 5.80 7.54 0.5 2.49 0.15 0.3 0.3 804	13 2029.12 38 13.62 22 5.80 7.82 0.5 2.50 0.19 0.4 0.4 805	14 3555.73 38 13.76 22 3.96 6.69 0.4 2.31 0.10 0.4 0.5 806	18 4 5.00 38 23.87 21 49.81 7.67 0.3 2.16 0.07 0.2 0.4 807	18 2518.62 38 24.63 21 54.74 9.32 0.3 2.64 0.10 0.1 0.2 808	18 4956.44 38 23.08 22 8.01 6.91 0.3 2.48 0.13 0.2 0.4 809	18 5155.10 38 22.97 22 7.98 7.19 0.2 2.34 0.11 0.2 0.3 811	20 1817.29 38 13.60 22 4.94 6.85 0.8 2.35 0.10 0.5 0.6 812	20 3846.25 38 14.25 22 5.46 7.04 0.3 2.41 0.12 0.3 0.2 813	23 10 6.98 38 24.75 22 8.13 10.99 0.5 2.39 0.04 0.5 0.4 814	0 1338.87 38 34.48 21 54.47 14.30 0.5 2.35 0.10 0.2 0.4 815	0 16 7,49 38 22.14 21 53.48 6.68 0.7 2.24 0.09 0.3 0.3 816	1 3214.75 38 24.74 21 58.40 8.79 1.9 2.27 0.12 1.7 0.5 817	1 4317.41 38 24.27 21 57.77 7.13 0.4 1.94 0.09 0.2 0.2 818

### APPENDIX C: FOCAL MECHANISMS



© 1996 RAS, GJI 126, 663-688





© 1996 RAS, GJI 126, 663-688



# APPENDIX D: FOCAL MECHANISM PARAMETERS

Event	Str1	Dip1	Slip1	Str2	Dip2	Slip2
6	0.0	50.0	-139.9	241.6	60.5	-47.6
8	37.0	83.0	124.7	137.0	35.3	12.2
12	320.0	45.0	-112.2	170.0	49.1	-69.3
13	265.0	23.0	-105.7	102.0	67.9	-83.4
14	300.0	43.0	-129.1	168.0	58.0	-59.5
15	290.0	40.0	-70.0	84.6	52.8	-106.0
22	211.0	70.0	-150.4	110.0	62.3	-22.7
23	223.0	70.0	-157.7	125.0	69.1	-21.5
25	220.0	70.0	-168.4	126.0	79.2	-20.4
34	69.0	35.0	-90.0	249.0	55.0	-90.0
35	120.0	50.0	-90.0	300.0	40.0	<b>-9</b> 0.0
37	102.0	45.0	-88.6	280.0	45.0	-91.4
39	120.0	80.0	-19.9	213.6	70.4	-169.4
40	230.0	50.0	- <del>9</del> 9.8	65.0	41.0	-78.6
41	170.0	40.0	-97.9	0.3	50.5	-83.4
45	110.0	50.0	-79.6	274.0	41.1	-102.2
46	324.0	35.0	-45.7	94.0	65.8	-116.1
47	300.0	20.0	-59.6	88.0	72.8	-100.4
50	89.0	60.0	-56.4	216.0	43.8	-133.8
52	51.0	51.0	-93.2	236.0	39.1	-86.1
59	70.0	80.0	-110.0	314.5	22.3	-27.3
64	310.0	48.0	-34.9	65.0	64.9	-132.3
70	290.0	65.0	-94.3	120.0	25.3	-80.9
72	285.0	65.0	-87.9	100.0	25.1	-94.5
73	70.0	70.0	-90.0	250.0	20.0	-90.0
79	120.0	80.0	180.0	210.0	90.0	0.0
86	35.0	70.0	165.7	130.0	76.5	20.6
88	210.0	90.0	0.0	300.0	90.0	180.0
91	75.0	27.0	-90.0	255.0	63.0	-90.0
92	270.0	60.0	-120.0	139.1	41.4	-49.1
97	30.0	40.0	-60.0	173.0	56.2	-112.8
98	110.0	80.0	-90.0	290.0	10.0	-90.0
103	267.0	28.0	-99.7	98.0	62.4	-84.9
106	90.0	80.0	-100.0	315.4	14.1	-45.5
117	210.0	60.0	0.0	300.0	90.0	180.0
121	250.0	44.0	-78.3	54.0	47.1	-101.0
127	290.0	70.0	-100.0	137.3	22.3	-64.5
136	277.0	44.0	-56.1	54.0	54.8	-118.3
140	311.0	45.0	-102.2	148.0	46.3	-78.1
142	96.0	69.0	-85.6	264.0	21.4	-101.2
146	101.0	59.0	-53.7	226.0	46.3	-134.6
154	70.0	70.0	-80.1	223.0	22.2	-115.3
155	84.0	71.0	-96.0	282.0	19.9	-73.0
156	73.0	65.0	-118.4	305.0	37.1	-44.4
1 <b>75</b>	48.0	47.0	-98.2	240.0	43.6	-81.3
176	106.0	71.0	-100.6	316.0	21.7	-61.8

APPENDIX D ((	Continued.)												
Event	Str1	Dip1	Slip1	Str2	Dip2	Slip2	Event	Str1	Dip1	Slip1	Str2	Dip2	Slip2
188	256.0	45.0	-104.4	96.0	46.8	-76.0	478	90.0	60.0	-90.0	270.0	30.0	-90.0
195	130.0	87.0	-66.9	227.0	23.3	-172.4	490	120.0	45.0	-34.6	236.0	66.3	-129.5
197	311.0	11.0	-46.5	87.0	82.0	-97.6	491	100.0	70.0	-90.0	280.0	20.0	-90.0
199	110.0	39.0	49.2	242.0	61.5	-117.9	496	295.0	30.0	-81.3	105.0	60.4	-95.0
223	290.0	50.0	-79.6	94.0	41.1	-102.2	506	312.0	45.0	-95.7	140.0	45.3	-84.4
226	330.0	70.0	-100.0	177.3	22.3	-64.5	531	0.06	75.0	-99.2	302.0	17.5	-59.2
232	220.0	20.0	-150.0	101.5	80.1	-72.5	563	270.0	10.0	-70.0	69.7	80.6	-93.5
235	10.0	50.0	-140.0	251.7	60.5	-47.6	569	286.0	83.0	-62.2	29.0	28.6	-165.3
241	260.0	40.0	-149.8	146.0	71.2	-54.0	579	286.0	61.0	-113.6	148.0	36.7	-54.2
242	260.0	40.0	-150.0	146.1	71.2	-54.0	581	316.0	59.0	-89.0	134.0	31.0	-91.7
249	321.0	36.0	-70.2	117.0	56.4	-103.8	583	275.0	58.0	-136.1	158.0	54.0	40.9
250	30.0	89.0	-149.0	299.4	59.0	-1.2	585	310.0	70.0	-80.1	103.0	22.2	-115.3
254	282.0	23.0	-54.3	64.0	71.5	-103.9	589	250.0	50.0	-169.9	153.5	82.3	40.4
264	112.0	53.0	-90.0	292.0	37.0	-90.0	597	274.0	17.0	9.66-	104.0	73.2	-87.1
267	80.0	60.0	-120.0	309.1	41.4	49.1	604	268.0	25.0	-115.7	116.0	67.6	-78.6
269	276.0	45.0	-92.8	100.0	45.1	-87.2	<b>6</b> 99	300.0	9.0	-60.3	90.0	82.2	-94.5
273	90.0	65.0	-90.0	270.0	25.0	-90.0	612	281.0	13.0	-92.9	104.0	77.0	-89.3
279	140.0	80.0	-59.9	246.7	31.5	-160.6	618	310.0	20.0	-69.2	108.0	71.4	-97.4
294	30.0	65.0	168.3	125.0	79.4	25.5	623	250.0	10.0	-110.0	90.3	80.6	-86.5
297	250.0	70.0	-169.9	156.5	80.5	-20.3	625	97.0	61.0	-76.7	251.0	31.7	-112.5
305	80.0	0.77	-104.0	308.0	0.61	-43.6	631	264.0	41.0	-83.9	76.0	49.3	-95.2
308	317.0	62.0	14.7	220.0	77.1	151.2	636	80.0	53.0	-63.2	220.0	44.5	-120.9
309	296.0	49.0	-100.7	132.0	42.1	-78.0	638	65.0	65.0	-37.6	173.0	56.5	-149.5
312	90.0	70.0	-100.0	297.3	22.3	-64.5	639	86.0	69.0	-101.7	296.0	23.9	-62.2
315	59.0	68.0	-146.4	315.0	59.1	-25.9	643	265.0	43.0	-101.1	100.0	48.0	-79.8
319	108.0	39.0	-75.8	270.0	52.4	-101.2	<b>644</b>	100.0	60.0	-130.0	339.2	48.4	-41.9
322	300.0	20.0	-60.0	88.4	72.8	-100.3	649	285.0	45.0	-121.6	146.0	53.0	-62.4
324	315.0	48.0	-111.9	166.0	46.4	-67.5	655	80.0	0.06	180.0	170.0	90.0	0.0
326	300.0	21.0	-71.2	100.0	70.2	-97.0	677	276.0	0.91	-107.1	114.0	71.9	-84.2
335	256.0	47.0	-73.1	52.0	45.6	-107.3	682	269.0	29.0	-121.5	124.0	65.6	-73.9
337	332.0	69.0	-21.4	70.0	70.1	-157.6	711	112.0	29.0	-68.7	268.0	63.1	-101.4
349	240.0	60.0	-148.6	133.0	63.1	-34.1	715	94.0	17.0	-82.3	266.0	73.2	-92.3
350	90.0	80.0	-90.0	270.0	10.0	-90.0	727	58.0	31.0	-118.2	270.0	63.0	-74.2
356	330.0	66.0	-9.8 	64.0	81.1	-155.7	728	116.0	41.0	-68.1	268.0	52.5	-107.9
358	350.0	45.0	46.8	223.0	0.65	124.4	733	42.0	25.0	-125.3	260.0	69.8	-74.9
360	75.0	73.0	-128.8	325.0	41.8	-26.0	734	24.0	45.0	-145.4	268.0	66.3	-50.5
505 112	36.0	0.08	-158.2	0.406	08.3	4.C-	738	0.0	45.0	-155.3	252.0	72.8	1.14
5/5 TTC	308.U	45.0	77/94	124.0	1.04	9.76-	651	38.0	31.U	-133.0	200.0	1.80	C.79-
395	0.005	0.00	0.01-	790.0 240.0	0.00	0.611-	147	0.08	0.00	5.50- C 00-	0.622	6.00	-1003
200	115.0	0.00		0.540	246	-135.3	LSL	76.0	0.02	0.00	0.750	0.10	0.06
02C	0.01	0.57	-1457	340.0	571	0.001-	161	85.0	0.10	0.06- - 74 3	0.002	0.00	0.06-
400	950	20.05	73.3	250.0	42.8	-108.9	011	72.0	250	-1157	280.0	67.6	2.00-
411	81.0	59.0	-98.9	278.0	32.1	-75.5	794	28.0	0.6	-85.1	203.0	81.0	-90.8
422	80.0	25.0	-90.0	260.0	65.0	-90.0	802	276.0	37.0	-83.6	88.0	53.3	-94.8
423	55.0	45.0	-67.8	205.0	49.1	-110.7	608	47.0	47.0	-98.9	240.0	43.7	-80.5
431	310.0	30.0	-60.0	96.3	64.3	-106.1	811	110.0	37.0	-58.0	252.0	59.3	-111.7
437	84.0	65.0	-75.2	232.0	28.8	-118.7	819	308.0	65.0	-90.0	128.0	25.0	-90.0
447	350.0	30.0	-40.0	116.0	71.3	-113.9	843	80.0	80.0	-80.1	215.0	14.0	-134.1
463	45.0	68.0	-2.7	136.0	87.5	-158.0							
473	124.0	40.0	-93.8	309.0	50.1	-86.8							
475	180.0	55.0	-69.6	327.0	<b>39.9</b>	-116.5							